## Fluid Mechanics (CT-213)

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# Energy Consideration + Orifices 

Lecture - 7

## Incompressible Fluid:

$\square$ For an incompressible fluid ( $\gamma=$ constant $)$,

$$
\frac{p_{2}}{\gamma}-\frac{p_{1}}{\gamma}+z_{2}-z_{1}+\frac{V_{2}^{2}}{2 g}-\frac{V_{1}^{2}}{2 g}=-\frac{\tau P L}{\gamma A}
$$

$\square$ Or Energy per unit weight:

$$
\begin{equation*}
\left(\frac{p_{1}}{\gamma}+z_{1}+\frac{V_{1}^{2}}{2 g}\right)-\frac{\tau P L}{\gamma A}=\left(\frac{p_{2}}{\gamma}+z_{2}+\frac{V_{2}^{2}}{2 g}\right) \tag{5.12}
\end{equation*}
$$

## Assumptions:

1. Steady flow
2. Incompressible fluid
3. Along a streamline
4. No energy added or removed

## Head:

$\square$ If we compare Eq. (5.12) with Bernoulli Eq. (5.7) for ideal flow we see again the only difference is the additional term $-\tau P L /(\gamma A)$, which represents the loss of energy per unit weight due to fluid friction between points 1 and 2 .
$\square$ The dimensions of this energy loss term are length only, which agrees with all the other terms in Eq. (5.12), and so this term is a form of head.

## Wall friction head loss:

$\square$ The friction causing this loss of energy occurs over the boundary or surface of the element, of area PL. When, as occurs often, we consider the stream tube to fill the conduit, pipe, or duct conveying the fluid, $P L$ becomes the inside surface area of the conduit wall, and $\tau$ becomes the shear stress at the wall, $\tau_{0}$. Then we can call this energy loss term the
$\square$ Wall friction head loss:

$$
\begin{equation*}
h_{f}=\frac{\tau_{0} P L}{\gamma A} \tag{5.13}
\end{equation*}
$$

$\square$ Energy per unit weight:

$$
\begin{equation*}
\left(\frac{p_{1}}{\gamma}+z_{1}+\frac{V_{1}^{2}}{2 g}\right)-h_{f}=\left(\frac{p_{2}}{\gamma}+z_{2}+\frac{V_{2}^{2}}{2 g}\right) \tag{5.14}
\end{equation*}
$$

## Pipe friction head loss:

$\square$ If, as is most common, the conduit is a circular pipe of diameter $D$, then $\quad P / A=\pi D /\left(\pi D^{2} / 4\right)=4 / D \quad$,and Eq. (5.13) becomes the
$\square$ Pipe friction head loss:

$$
\begin{equation*}
h_{f}=\frac{4 \tau_{0} L}{\gamma D} \tag{5.1.}
\end{equation*}
$$

$\square$ Fluid friction loss from any such cause, including wall or pipe friction, we commonly refer to as head loss, denoted by $h_{L}$. So wall friction head loss is usually a part of, but it may be all of, the total head loss. In a given conduit, then $h_{L \geq} h_{f}$.

## Problem

$\square$ Water flows through a 150 -ft-long, 9 -in-diameter pipe at 3.8 cfs . At the entry point, the pressure is 30 psi ; at the exit point, 15 ft higher than the entry point, the pressure is 20 psi . Between these two points, find (a) the pipe friction head loss, (b) the wall shear stress, and (c) the friction force on the pipe.


## Solution:

(a) From Eq. (5.14): $\quad h_{f}=\left(\frac{30(144)}{62.4}+0+\frac{V^{2}}{2 g}\right)-\left(\frac{20(144)}{62.4}+15+\frac{V^{2}}{2 g}\right)$
$V_{1}=V_{2}$ so terms in $V$ cancel, and

$$
h_{f}=8.08 \mathrm{ft}
$$

(b) From Eq. (5.15):

$$
r_{0}=\frac{h_{f} \gamma D}{4 L}=\frac{8.08(62.4) 0.75}{4(150)}=0.630 \mathrm{lb} / \mathrm{ft}^{2}
$$

(c) Friction Force $=r_{0} P L=r_{0}(\pi D) L=0.630 \pi(0.75) 150=223 l b$

## HEAD

$$
\begin{equation*}
\left(\frac{p_{1}}{\gamma}+z_{1}+\frac{V_{1}^{2}}{2 g}\right)-h_{L}=\left(\frac{p_{2}}{\gamma}+z_{2}+\frac{V_{2}^{2}}{2 g}\right) \tag{5.28}
\end{equation*}
$$

$\square$ In above equation each term has the dimensions of length. Thus $\mathrm{p} / \gamma$, called the pressure head, represents the energy per unit weight stored in the fluid by virtue of the pressure under which the fluid exists.
$\square \mathrm{Z}$ called the elevation head or potential head, represents the potential energy per pound of fluid;
$\square \mathrm{V}^{2 / 2} \mathrm{~g}$, called the velocity head, represents the kinetic energy per pound of fluid.
$\square$ We call the sum of these three terms the total head, usually denoted by H, so that

$$
\begin{equation*}
H=\frac{p}{\gamma}+z+\frac{V^{2}}{2 g} \tag{5.35}
\end{equation*}
$$

## Practical Applications of Bernoulli's Theorem

$\square$ The Bernoulli equation can be applied to a great many situations not just the pipe flow we have been considering up to now.
$\square$ In the following sections we will see some examples of its application to flow measurement from tanks, within pipes as well as in open channels.

1. Venturimeter
2. Orificemeter
3. Pitot tube

## 1. Venturimeter:

$\square$ The Venturimeter is a device for measuring discharge in a pipe.
$\square$ It consists of three parts.
a. Convergent Cone
b. Throat
c. Divergent Cone


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## a. Convergent Cone:

$\square$ It is a short pipe which converges from a diameter $d_{1}$ (diameter of a pipe in which a venturimeter is fitted) to a smaller diameter $\mathrm{d}_{2}$.
$\square$ The convergent cone is also known as inlet of the venturimeter.
$\square$ The slope of the converging sides is between 1in 4 or 1in 5.

## b. Throat:

$\square$ It is a small portion of circular pipe in which the


## c. Divergent Cone:

$\square$ It is a pipe, which diverges from a diameter $\mathrm{d}_{2}$ to a large diameter $\mathrm{d}_{1}$.
$\square$ The divergent cone is also known as outlet of venturimeter.
$\square$ The length of the divergent cone is about 3 to 4 times than that of convergent cone.


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## How it operates?

$\square$ It consists of a rapidly converging section, which increases the velocity of flow and hence reduces the pressure (acceleration $\mathrm{b} / \mathrm{w}$ section 1-2).
$\square$ It then returns to the original dimensions of the pipe by a gently diverging 'diffuser' section (deceleration b/w section 2-3).
$\square$ By measuring the pressure differences the discharge can be calculated.
$\square$ This is a particularly accurate method of flow measurement as energy losses are very small.

## Why the divergent cone is made longer?

$\square$ As a result of retardation (section 2-3), the velocity decreases and pressure increases.
$\square$ If the pressure is rapidly recovered, then there is every possibility for the stream of liquid to break away from the walls of meter.
$\square$ In order to avoid the tendency of breaking away the stream of liquid, the divergent cone is made sufficiently longer.
$\square$ Another reason is to minimize friction losses.
$\square$ Divergent cone is 3 to 4 times longer than convergent cone.

## Measurement of Discharge:

$\square$ Consider a venturimeter through which some liquid is flowing.

Let

$\square \mathrm{p}_{1}=$ Pressure at section 1
$\square \mathrm{V}_{1}=$ Velocity of water at section 1
$\square \mathrm{Z}_{1}=$ Datum head at section 1
$\square \mathrm{a}_{1}=$ Area of venturimeter at section 1$\mathrm{p}_{2}, \mathrm{~V}_{2}, \mathrm{z}_{2}, \mathrm{a}_{2}=$ Corresponding values at section 2

Applying Bernoulli' s equation at sections 1 and 2 i.e,
$\frac{p_{1}}{\gamma}+z_{1}+\frac{V_{1}{ }^{2}}{2 g}=\frac{p_{2}}{\gamma}+z_{2}+\frac{V_{2}{ }^{2}}{2 g}$
Let datum line be the axis of venturime ter,
Now $\mathrm{z}_{1}=0$ and $\mathrm{z}_{2}=0$
$\therefore \frac{p_{1}}{\gamma}+\frac{V_{1}^{2}}{2 g}=\frac{p_{2}}{\gamma}+\frac{V_{2}^{2}}{2 g}$
or $\frac{p_{1}}{\gamma}-\frac{p_{2}}{\gamma}=\frac{V_{2}{ }^{2}}{2 g}-\frac{V_{1}{ }^{2}}{2 g}$
Since the discharge at Section $1 \& 2$ is continuous, therefore
$\mathrm{V}_{1}=\frac{a_{2} V_{2}}{a_{1}}$
$\left(\because \mathrm{a}_{1} V_{1}=\mathrm{a}_{2} V_{2}\right)$
$\therefore \mathrm{V}_{1}^{2}=\frac{a_{2}^{2} V_{2}^{2}}{a_{1}^{2}}$

Substituti ng value in equation 2 .

$$
\begin{aligned}
\frac{p_{1}}{\gamma}-\frac{p_{2}}{\gamma} & =\frac{V_{2}^{2}}{2 g}-\frac{a_{2}^{2} V_{2}^{2}}{a_{1}^{2} \cdot 2 \mathrm{~g}} \\
& =\frac{V_{2}^{2}}{2 g}\left(\frac{a_{1}^{2}-a_{2}^{2}}{a_{1}^{2}}\right)
\end{aligned}
$$

We know that $\frac{p_{1}}{\gamma}-\frac{p_{2}}{\gamma}$ is the difference between the pressure heads
at section $1 \& 2$. When the pipe is horizontal , this difference represents the venturi head and is denoded by h .
or $\mathrm{h}=\frac{V_{2}^{2}}{2 g}\left(\frac{a_{1}^{2}-a_{2}^{2}}{a_{1}^{2}}\right)$

$$
\mathrm{V}_{2}^{2}=2 g h\left(\frac{a_{1}^{2}}{a_{1}^{2}-a_{2}^{2}}\right)
$$

$$
\mathrm{V}_{2}=\sqrt{2 g h}\left(\frac{a_{1}}{\sqrt{a_{1}^{2}-a_{2}^{2}}}\right)
$$

We know that discharge through a venturimt er,
$\mathrm{Q}=$ Coefficent of Venturimte $\mathrm{r} . \mathrm{a}_{2} . V_{2}$
$\mathrm{Q}=\mathrm{C} . \mathrm{a}_{2} \cdot V_{2}$
$\mathrm{Q}=\left(\frac{C a_{1} a_{2}}{\sqrt{a_{1}^{2}-a_{2}^{2}}}\right) \sqrt{2 g h}$

## Note:

The venturi head (h), in above equation is taken in terms of liquid head. But, in actual practice, this head is given as mercury head. In such a case the mercury head should be converted into the liquid head.

$$
h=(13.6-s) / s \quad x \quad \text { Head of mercury }
$$

Where, 13.6 is Sp. gravity of mercury and 's' is Sp. gravity of Oil.

## Inclined Venturimeter:



## Problems:

A venturimeter with a 150 mm diameter at inlet and 100 mm at throat is laid with its axis horizontal and is used for measuring the flow of oil ( Sp . Gravity $=0.9$ ). The oil-mercury differential manometer shows a gauge difference of 200 mm . Assume coefficient of meter as 0.98 . Calculate discharge in liters per minute. (Ans, $\mathrm{Q}=3834 \mathrm{lit} / \mathrm{min}$ ).
2. A venturimeter has an area ratio of 9 to 1 , the larger diameter being 300 mm . During the flow, the recorded pressure head in the large section in 6.5 m and that at the throat 4.25 m . If the meter coefficient, $\mathrm{C}=0.99$, compute discharge through the meter. (Ans, $52 \mathrm{lit} / \mathrm{s}$ ).
3. A horizontal venturimeter $160 \mathrm{~mm} \times 80 \mathrm{~mm}$ is used to measure the flow of an oil of Sp . Gracity 0.8 . Determine the deflection of the oil-mercury gauge, if the discharge of the oil is 50lit/s. Take coefficient of venturimeter as 1 . (Ans, 296mm).

## Problems:

4. A venturimeter is to be filled to a 250 mm diameter pipe, in which the maximum flow is $7200 \mathrm{lit} / \mathrm{min}$ and the pressure head is 6 m of water. What is the minimum diameter of throat, so that there is no negative head in it? (Ans, 117 mm )
5. A $300 \mathrm{~mm} \times 150 \mathrm{~mm}$ venturimeter is provided in a vertical pipeline carrying oil of Sp . Gravity 0.9 , the flow being upwards. The difference in elevations of the throat section and entrance section of the venturimeter is 300 mm . The differential $U$ tube mercury manometer shows a gauge deflection of 250 mm . Calculate
i) discharge of the oil
ii) pressure difference $\mathrm{b} / \mathrm{w}$ the entrance and throat section.


## 2. Orifice Meter:

$\square$ An orifice meter is used to measure the discharge in a pipe. It consists of a plate having a sharp edged circular hole known as an orifice. This plate is fixed inside a pipe.


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## Measurement of Discharge:

$\square$ A mercury manometer is inserted to know the difference of pressure between the pipe and the throat. (i.e., orifice)

Let
$\square \mathrm{h}=$ Reading of mercury manometer
$\square \mathrm{p}_{1}=$ Pressure at the inlet
$\square \mathrm{V}_{1}=$ Velocity of liquid at inlet
$\square \mathrm{a}_{1}=$ Area of pipe at inlet
$\square \mathrm{p}_{2}, \mathrm{~V}_{2}, \mathrm{a}_{2}=$ Corresponding values at throat

Applying Bernoulli' s equation for inlet of pipe and the throat,
$\frac{p_{1}}{\gamma}+z_{1}+\frac{V_{1}{ }^{2}}{2 g}=\frac{p_{2}}{\gamma}+z_{2}+\frac{V_{2}{ }^{2}}{2 g}$
$\frac{p_{1}}{\gamma}-\frac{p_{2}}{\gamma}=\frac{V_{2}{ }^{2}}{2 g}-\frac{V_{1}^{2}}{2 g} \quad\left(\because \mathrm{z}_{1}=z_{2}\right)$
or $\quad \mathrm{h}=\frac{V_{2}^{2}}{2 g}-\frac{V_{1}^{2}}{2 g}=\frac{1}{2 g}\left(V_{2}^{2}-V_{1}^{2}\right)$
Since the discharge is continuous, therefore
$\mathrm{V}_{1}=\frac{a_{2} V_{2}}{a_{1}}$
$\left(\because \mathrm{a}_{1} V_{1}=\mathrm{a}_{2} V_{2}\right)$
$\therefore \mathrm{V}_{1}{ }^{2}=\frac{a_{2}^{2} V_{2}{ }^{2}}{a_{1}{ }^{2}}$

Substituti ng value in equation 2 .
$h=\frac{1}{2 g}\left(V_{2}^{2}-\frac{a_{2}^{2} V_{2}^{2}}{a_{1}^{2}}\right)=\frac{V_{2}^{2}}{2 g}\left(\frac{a_{1}^{2}-a_{2}^{2}}{a_{1}^{2}}\right)$
$\mathrm{V}_{2}^{2}=2 g h\left(\frac{a_{1}^{2}}{a_{1}^{2}-a_{2}^{2}}\right)$
$\mathrm{V}_{2}=\sqrt{2 g h}\left(\frac{a_{1}}{\sqrt{a_{1}^{2}-a_{2}^{2}}}\right)$
We know that discharge,
$\mathrm{Q}=$ Coefficent of Orifice Meter. $\mathrm{a}_{2} . V_{2}$
$\mathrm{Q}=\mathrm{C} . \mathrm{a}_{2} . V_{2}$
$\mathrm{Q}=\left(\frac{C a_{1} a_{2}}{\sqrt{a_{1}^{2}-a_{2}^{2}}}\right) \sqrt{2 g h}$
(Same as venturime ter)

## Problem:

$\square$ An orifice meter consisting of 100 mm diameter orifice in a 250 mm diameter pipe has coefficient equal to 0.65 . The pipe delivers oil (Sp. Gravity 0.8). The pressure difference on the two sides of the orifice plate is measured by a mercury oil differential manometer. If the differential gauge reads 80 mm of mercury, calculate the rate of flow in lit/s. (Ans, $82 \mathrm{lit} / \mathrm{s}$ )

## 3. Pitot Tube:

$\square$ A Pitot tube is an instrument to determine the velocity of flow at the required point in a pipe or a stream.
$\square$ It consists of glass tube bent a through $90^{\circ}$
$\square$ The lower end of the tube faces the direction of the flow.
$\square$ The liquid rises up in the tube due to the pressure exerted by the flowing liquid.
$\square$ By measuring the rise of liquid in the tube, we can find out the velocity of the liquid flow.



## Finding Velocity:

$\square$ Let
$\square \mathrm{h}=$ Height of liquid in the pitot tube above the surface.
$\square \mathrm{H}=$ Depth of tube in the liquid
$\square \mathrm{V}=$ velocity of the liquid
$\square$ Applying Bernoulli's equation for the section $1 \& 2$.

$$
\begin{aligned}
& H+\frac{V^{2}}{2 g}=\mathrm{H}+\mathrm{h} \\
& \mathrm{~h}=\frac{\mathrm{V}^{2}}{2 \mathrm{~g}} \\
& V=\sqrt{2 g h}
\end{aligned}
$$



## Problem:

$\square$ A pitot tube was inserted in a pipe to measure the velocity of water in it. If the water rises in the tube is 200 mm . Find velocity of water. (Ans, $1.98 \mathrm{~m} / \mathrm{s}$ )

## FLOW THROUGH ORIFICES

## Introduction:

$\square$ "Orifice is an opening in a vessel through which the liquid flows out."
$\square$ This hole or opening is called an orifice, so long as the level of the liquid on the upstream side is above the top of the orifice.
$\square$ The usual purpose of an orifice is the measurement of discharge.
$\square$ It can be provided in the vertical side of the vessel on in the base. But the former is more common.

# Types of Orifices According to: 



## Important Terms:

$\square$ Jet of Water:
"The continuous stream of liquid, that comes out or flows out of an orifice, is known as Jet of water."
$\square$ Vena Contracta:
$\square$ Vena contracta is the point in a fluid stream where the diameter of the stream is the least, and fluid velocity is at its maximum.


## Vena Contracta:

$\square$ Consider a tank, fitted with an orifice. The liquid particle, in order to flow out through the orifice, move towards the orifice from all directions.
$\square$ A few of the particles first move downward, then take a turn to enter into the orifice and then finally flow through it.
$\square$ It may be noted, that the liquid particles lose some energy, while taking the turn to enter into the orifice.
$\square$ It has been thus observed that the jet, after leaving the orifice, gets contracted.
$\square$ The maximum contraction takes place at a section slightly on the downstream side of the orifice, where the jet is more or less horizontal. Such a section is known as vena contracta as shown by section C (1-2),ing.cingurne

## Vena Contracta:



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## Hydraulic Coefficients:

Following four coefficients are known as hydraulic coefficients or orifice Coefficient.

1) Coefficient of contraction
2) Coefficient of velocity
3) Coefficient of discharge
4) Coefficient of resistance

## 1. Coefficient of Contraction:

$\square$ "The ratio of area of jet, at vena contracta, to the area of orifice is known as coefficient of contraction."
$\square$ Mathematically,

$$
C_{c}=\frac{\text { Area of jet at vena Contracta }}{\text { Area of Orifice }}
$$

$\square$ The value varies slightly with the available head of the liquid, size and the shape of the orifice.
$\square$ An average value of $C_{c}$ is about 0.64.

## 2. Coefficient of Velocity:

- "The ratio of actual velocity of the jet, at vena contracta, to the theoretical velocity is known as coefficient of velocity."
$\square$ Mathematically,

$$
C_{v}=\frac{\text { Actual velocity of jet at vena Contracta }}{\text { Theoretical velocity of jet }}
$$

$\square$ The difference between the velocities is due to friction of the orifice.
$\square$ The value of coefficient of velocity varies slightly with the different shapes of the edges of the orifices.
$\square$ For a sharp edged orifice, the value of $\mathrm{C}_{\mathrm{v}}$ increases with the head of water.

## 2. Coefficient of Velocity:

$\square$ The following table gives the values of $\mathrm{C}_{\mathrm{v}}$ for an orifice of 10 mm diameter with the corresponding head (given by Weisback).

| $\mathbf{H}$ | $\mathbf{2 0 m m}$ | $\mathbf{5 0 0} \mathbf{m m}$ | $\mathbf{3 . 5 m}$ | $\mathbf{2 0 m}$ | $\mathbf{1 0 0 m}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{C}_{\mathbf{v}}$ | 0.959 | 0.967 | 0.975 | 0.991 | 0.994 |

## Note:

$\square$ An Average value of $C_{v}$ is about 0.97.
$\square$ The theoretical velocity of jet at vena contracta is given by relation :

$$
V=\sqrt{2 g h}
$$



## 3. Coefficient of Discharge:

$\square$ "It is the ratio of actual discharge through an orifice to the theoretical discharge."
$\square$ Mathematically,

$$
\begin{aligned}
C_{d} & =\frac{\text { Actual discharge }}{\text { Theoretica l discharge }} \\
& =\frac{\text { Actual velocity } \times \text { Actual area }}{\text { Theoretical velocity } \times \text { Theoretical area }} \\
& =\mathrm{C}_{\mathrm{v}} \times \mathrm{C}_{\mathrm{c}}
\end{aligned}
$$

$\square$ Average value of coefficient of discharge varies from 0.60 to 0.64.

## 4. Coefficient of Resistance:

" "The ratio of loss of head in the orifice to the head of water available at the exit of the orifice is known as coefficient of resistance."
$\square$ Mathematically,

$$
C_{r}=\frac{\text { Loss of head in the orifice }}{\text { Head of water }}
$$

$\square$ The loss of head in the orifice takes place, because the walls of the orifice offer some resistance to the liquid as it comes out.
$\square$ The coefficient of resistance is generally neglected, while solving numerical.

## Problems:

1. A jet of water issues from an orifice of diameter 20 mm under a head of 1 m . What is the coefficient of discharge for the orifice, if actual discharge is $0.85 \mathrm{lit} / \mathrm{s}$. (Ans, 0.61 )
2. A 60 mm diameter orifice is discharging water under a head of 9 m . Calculate the actual discharge through the orifice in $\mathrm{Lit} / \mathrm{s}$ and actual velocity of the jet in $\mathrm{m} / \mathrm{s}$ at vena contracta, if $\mathrm{C}_{\mathrm{d}}=0.625$ and $\mathrm{C}_{\mathrm{v}}=0.98$. (Ans, $\mathrm{Q}=23.5 \mathrm{lit} / \mathrm{s} \& \mathrm{~V}_{\mathrm{ac}}=$ $13 \mathrm{~m} / \mathrm{s}$ )
