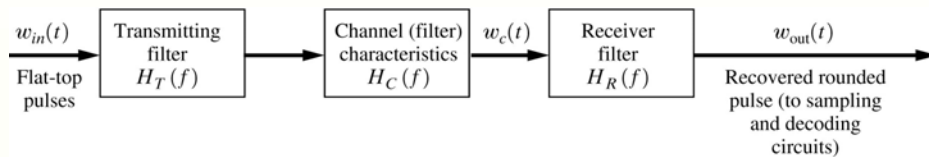


ISI- Inter-symbol Interference

Nyquist filters

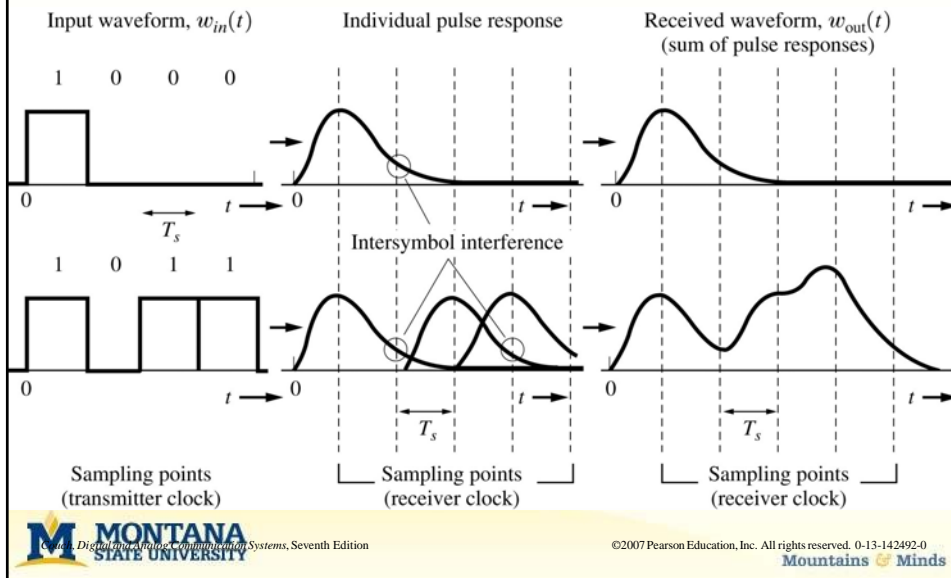
Lecture 13

Figure 3–24 Baseband pulse-transmission system.

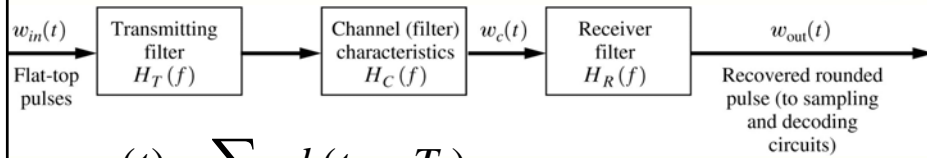


- $H_T(f)$ shapes the rectangular pulses to the desired pulse shape transmitted to control the Bandwidth
- $H_C(f)$ is the channel response modeled as a filter
- $H_R(f)$ is the receiver filter designed to remove the pulse distortion caused by the channel and maximize the S/N

Examples of ISI on received pulses in a binary communication system.



System Transfer Functions



$$w_{in}(t) = \sum_n a_n h(t - nT_s)$$

$$w_{out}(t) = \sum_n a_n \delta(t - nT_s) \otimes h(t)$$

$$h_e(t) = h(t) \otimes h_T(t) \otimes h_C(t) \otimes h_r(t)$$

$$H_e(f) = H(f)H_T(f)H_C(f)H_r(f)$$

System Transfer Function

Receive Equalization Filter

$$H_r(f) = \frac{H_e(f) = 1}{H(f)H_T(f)H_C(f)}$$

- H_r is designed to minimize ISI
- it may be fixed or adaptive
- Adaptive Filter
 - trained by using known symbol sequences called preambles

Raised Cosine-Rolloff Nyquist Filter

DEFINITION. The *raised cosine-rolloff Nyquist filter* has the transfer function

$$H_r(f) = \begin{cases} 1 & |f| \leq f_1 \\ \left[1 - \cos \left[\frac{\pi(f_1 - |f|)}{2f_\Delta} \right] \right] & f_1 < |f| < B \\ 0 & |f| > B \end{cases} \quad (3-69)$$

where B is the *absolute bandwidth* and the parameters

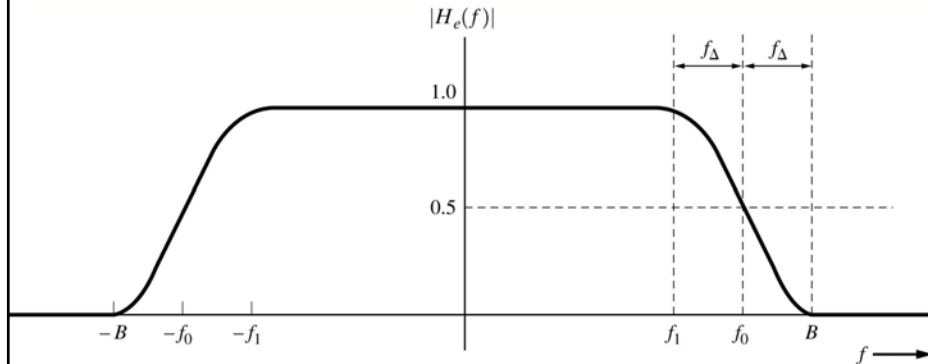
$$f_\Delta = B - f_0 \quad (3-70)$$

and

$$f_1 \triangleq f_0 - f_\Delta \quad (3-71)$$

f_0 is the *6-dB bandwidth* of the filter. The *rolloff factor* is defined to be

Raised Cosine-Rolloff Nyquist Filter



Raised Cosine-Rolloff Nyquist Filter

f_0 is the 6-dB bandwidth of the filter. The *rolloff factor* is defined to be

$$r = \frac{f_{\Delta}}{f_0} \quad (3-72)$$

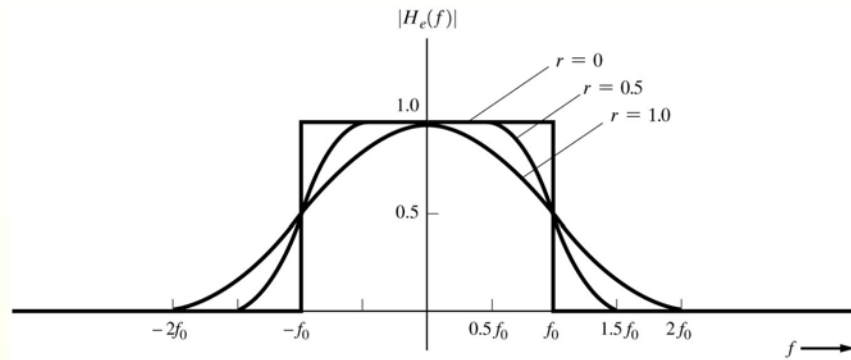
This filter characteristic is illustrated in Fig. 3-25. The corresponding impulse response is

$$h_e(t) = \mathcal{F}^{-1}[H_e(f)] = 2f_0 \left(\frac{\sin 2\pi f_0 t}{2\pi f_0 t} \right) \left[\frac{\cos 2\pi f_{\Delta} t}{1 - (4f_{\Delta} t)^2} \right] \quad (3-73)$$

Plots of the frequency response and the impulse response are shown in Fig. 3-26 for rolloff factors $r = 0$, $r = 0.5$, and $r = 1.0$. The $r = 0$ characteristic is the minimum-bandwidth case, where $f_0 = B$ and the impulse response is the $(\sin x)/x$ pulse shape. From this figure, it is seen that as the absolute bandwidth is increased (e.g., $r = 0.5$ or $r = 1.0$), (1) the filtering requirements are relaxed, although $h_e(t)$ is still noncausal, and (2) the clock timing requirements are relaxed also, since the envelope of the impulse response decays faster than $1/|t|$ (on the order of $1/|t|^2$ for large values of t).

Raised Cosine-Rolloff Nyquist Filter

Figure 3–26 Frequency and time response for different rolloff factors.



$h_e(t)$

Raised Cosine-Rolloff Nyquist Filter

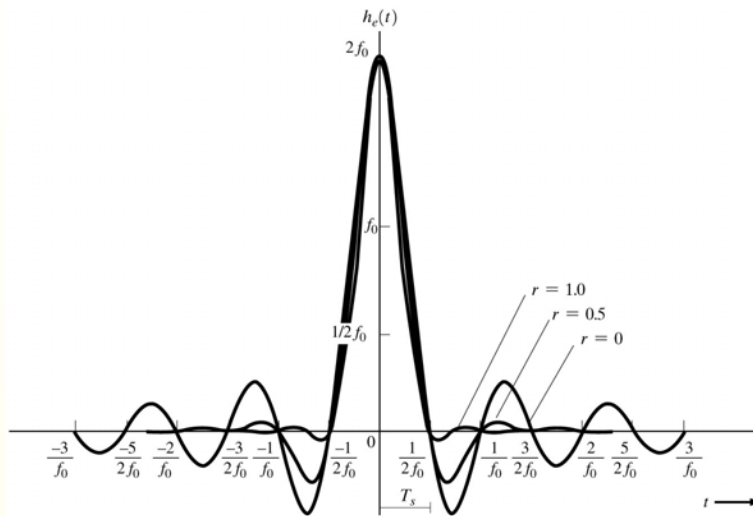
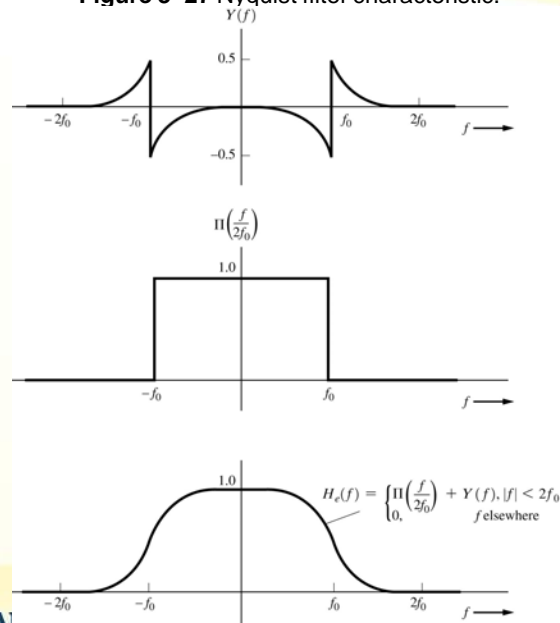


Figure 3-27 Nyquist filter characteristic.



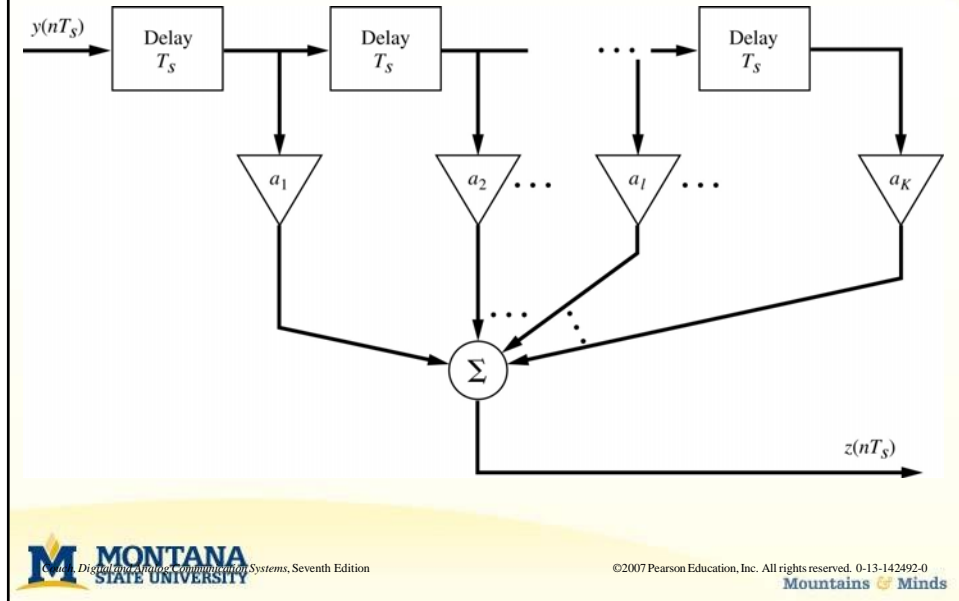
Raised Cosine-Rolloff Nyquist Filter

$$D = \frac{2B}{1+r} \quad (3-74)$$

Where D is the Supported Data rate without ISI

Look over example in the txt

Figure 3–28 Transversal filter.



Exam 1 solution in class

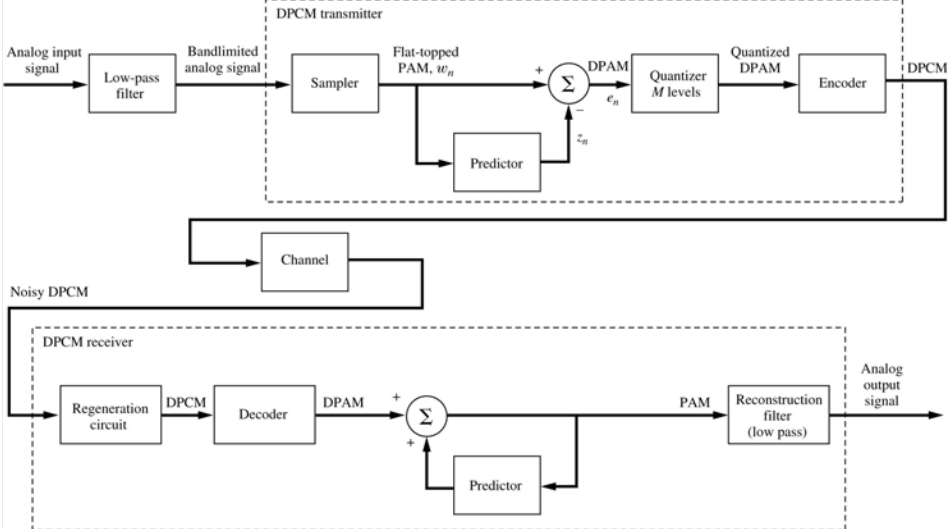
ELE445-14

Lecture 23

DPCM and single bit A/D

EELE445-14
Lecture 23

Differential Pulse code Modulation: DPCM



Differential Pulse code Modulation: DPCM

$$\frac{S}{N} \text{ dB} = 6.02n + \alpha$$

$-3 < \alpha < 15$ for DPCM Speech

Used For Speech - up to a 25 dB S/N improvement over μ -law 255

See pp92 in text

Delta Modulation –DM is single bit DPCM

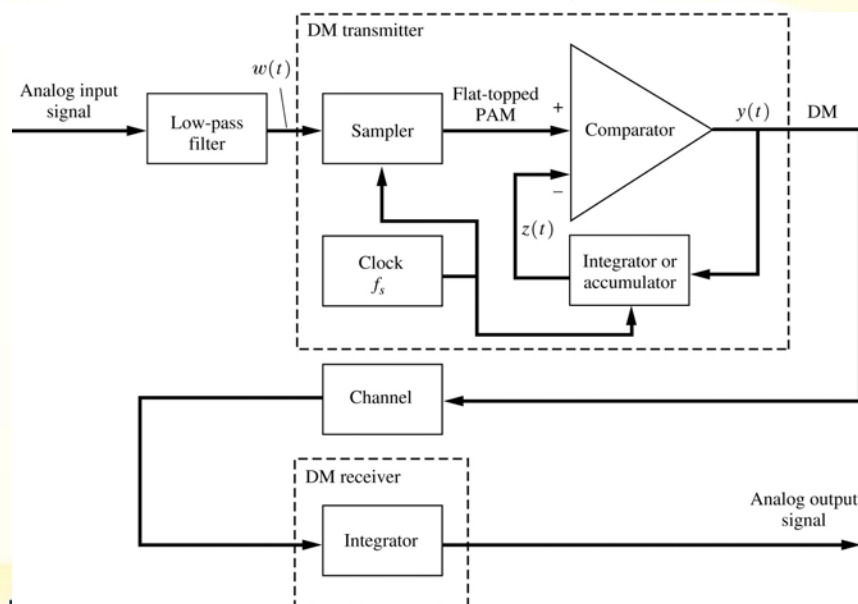
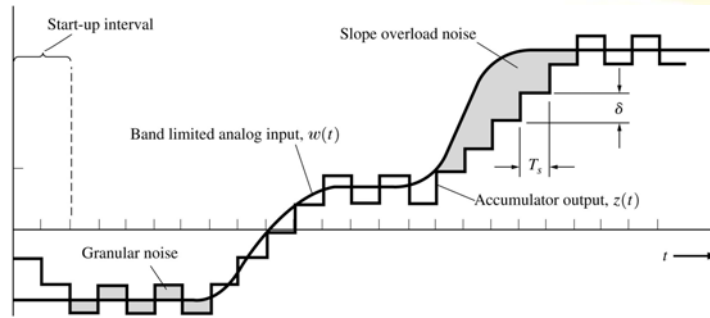
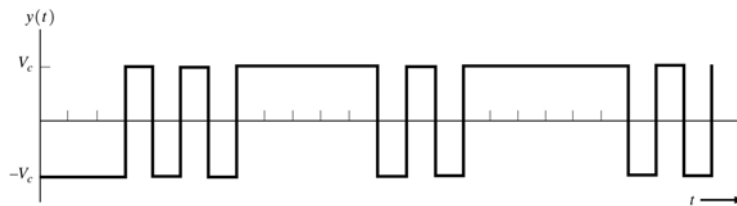


Figure 3–32 DM system waveforms.

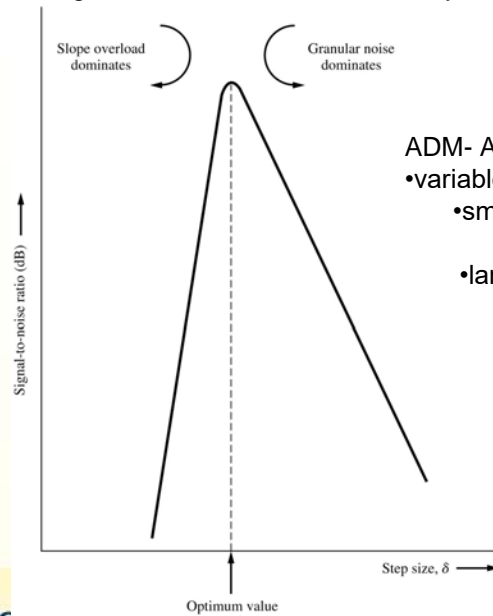


(a) Analog Input and Accumulator Output Waveforms



(b) Delta Modulation Waveform

Figure 3–33 Signal-to-noise ratio out of a DM system as a function of step size.



- ADM- Adaptive Delta Modulation
- variable step size
 - small step for slow variation
 - reduce granular noise
 - larger step for fast variation
 - reduce slope overload

Delta Modulation

$$\text{Granular Noise, } N = \langle n^2 \rangle = \int_{-B}^B P_n(f) df = \frac{\delta^2 B}{3 f_s}$$

$$N = \frac{4\pi^2 A^2 f^2 B}{3 f_s^3} \quad S = P_x = \frac{A^2}{2}$$

$$\frac{S}{N_{out}} = \frac{3 f^3}{8\pi^2 f^2 A^2 B}$$



For the A / D we had:

$$\langle q^2 \rangle = \frac{(x_{max})^2}{3 \times 4^n} = P_{nq} \quad A/D$$

$$SQNR = \frac{3 \times 4^n P_x}{x_{max}^2}$$

Mountains & Minds

TDM Time-Division Multiplexing for PAM, PCM, DM

EELE445-14

Lecture 24



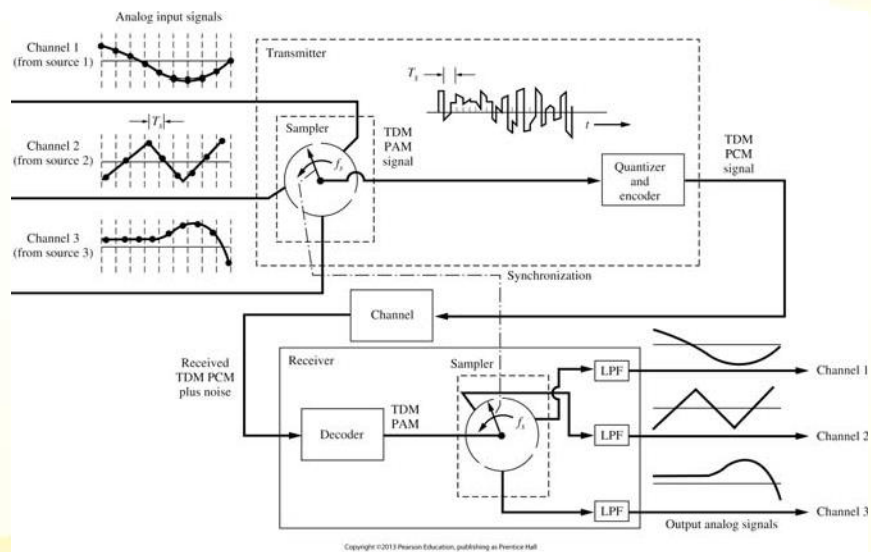
Mountains & Minds

Time-Division Multiplexing

Definition:

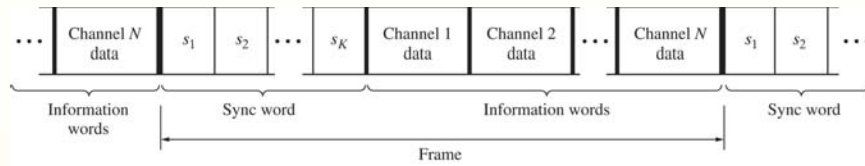
Time-division multiplexing (TDM) is the time interleaving of samples from several sources so that the information from these sources can be transmitted serially over a single communication channel.

Figure 3–35 Three-channel TDM PCM system.



Time-Division Multiplexing

Figure 3–36 TDM frame sync format.



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Figure 3-37 Frame synchronizer with TDM receiver front end.

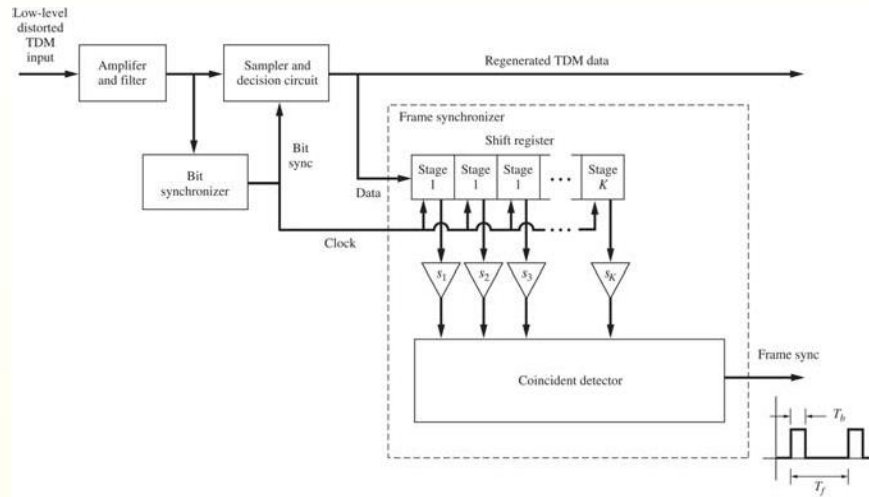


Figure 3-38 Two-channel bit-interleaved TDM with pulse stuffing.

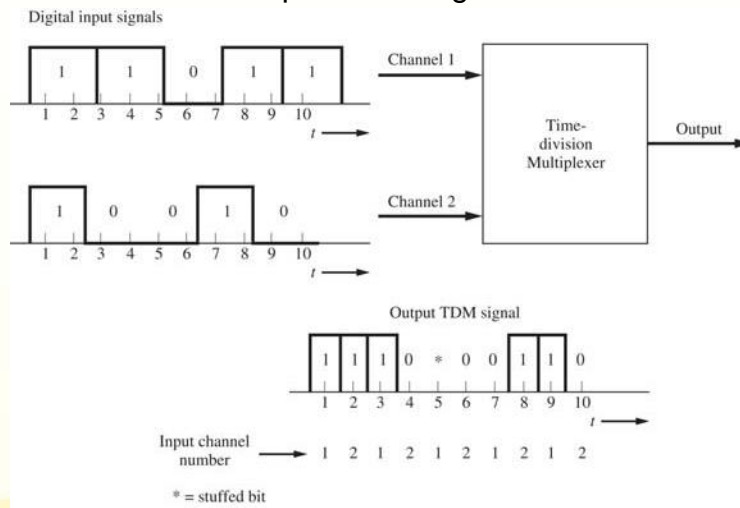


Figure 3–39 TDM with analog and digital inputs as described in Example 3–17.

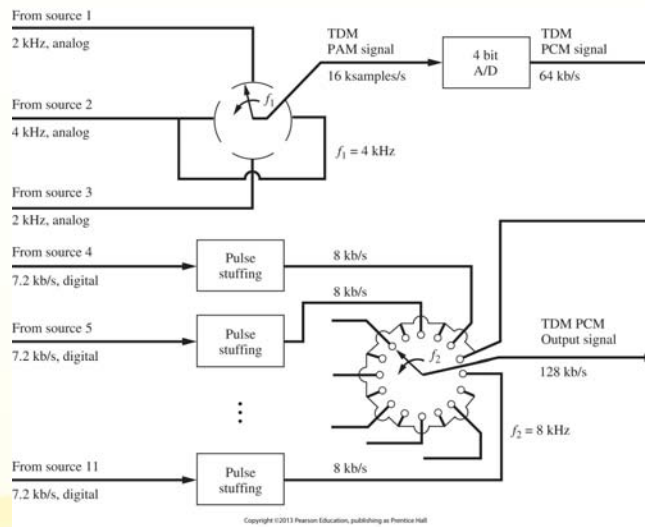


Figure 3–40 North American digital TDM hierarchy.

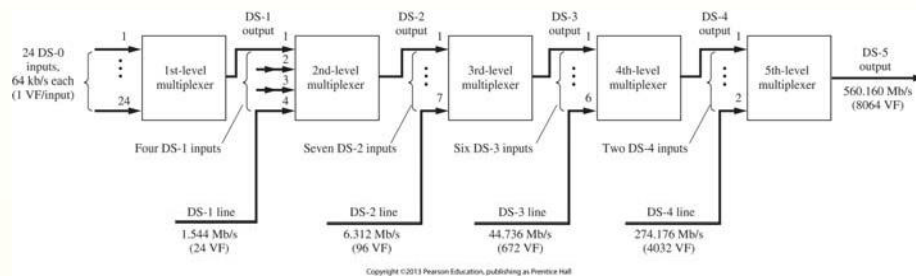


TABLE 3-8 TDM STANDARDS FOR NORTH AMERICA

TABLE 3-8 TDM STANDARDS FOR NORTH AMERICA

| Digital Signal Number | Bit Rate, <i>R</i> (Mbits/s) | No. of 64 kbits/s PCM VF Channels | Transmission Media Used |
|-----------------------|------------------------------|-----------------------------------|-------------------------|
| DS-0 | 0.064 | 1 | Wire pairs |
| DS-1 | 1.544 | 24 | Wire pairs |
| DS-1C | 3.152 | 48 | Wire pairs |
| DS-2 | 6.312 | 96 | Wire pairs, fiber |
| DS-3 | 44.736 | 672 | Coax., radio, fiber |
| DS-3C | 90.254 | 1344 | Radio, fiber |
| DS-4E | 139.264 | 2016 | Radio, fiber, coax. |
| DS-4 | 274.176 | 4032 | Coax., fiber |
| DS-432 | 432.000 | 6048 | Fiber |
| DS-5 | 560.160 | 8064 | Coax., fiber |

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TABLE 3-9 SPECIFICATIONS FOR T-CARRIER BASEBAND DIGITAL TRANSMISSION SYSTEMS

TABLE 3-9 SPECIFICATIONS FOR T-CARRIER BASEBAND DIGITAL TRANSMISSION SYSTEMS

| System | Rate (Mbits/s) | System Capacity | | Medium | Line Code | Repeater Spacing (miles) | Maximum System Length (miles) | System Error Rate |
|--------|----------------|--------------------|----------------|------------------------|----------------------|--------------------------|-------------------------------|----------------------|
| | | Digital Signal No. | Voice Channels | | | | | |
| T1 | 1.544 | DS-1 | 24 | Wire pair | Bipolar RZ | 1 | 50 | 10 ⁻⁶ |
| T1C | 3.152 | DS-1C | 48 | Wire pair | Bipolar RZ | 1 | — | 10 ⁻⁶ |
| T1D | 3.152 | DS-1C | 48 | Wire pair | Duobinary NRZ | 1 | — | 10 ⁻⁶ |
| T1G | 6.443 | DS-2 | 96 | Wire pair | 4-level NRZ | 1 | 200 | 10 ⁻⁶ |
| T2 | 6.312 | DS-2 | 96 | Wire pair ^a | B6ZS ^b RZ | 2.3 | 500 | 10 ⁻⁷ |
| T3 | 44.736 | DS-3 | 672 | Coax. | B3ZS ^b RZ | ^c | ^c | ^c |
| T4 | 274.176 | DS-4 | 4032 | Coax. | Polar NRZ | 1 | 500 | 10 ⁻⁶ |
| T5 | 560.160 | DS-5 | 8064 | Coax. | Polar NRZ | 1 | 500 | 4 × 10 ⁻⁷ |

^a Special two-wire cable is required for 12,000-ft repeater spacing. Because T2 cannot use standard exchange cables, it is not as popular as T1.

^b BnZS denotes *binary n-zero substitution*, where a string of *n* zeros in the bipolar line code is replaced with a special three-level code word so that synchronization can be maintained [Fike and Friend, 1984; Bic, Duponteil, and Imbeaux, 1991].

^c Used in central telephone office for building multiplex levels; not used for transmission from office to office.

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Figure 3–41 CCITT digital TDM hierarchy.

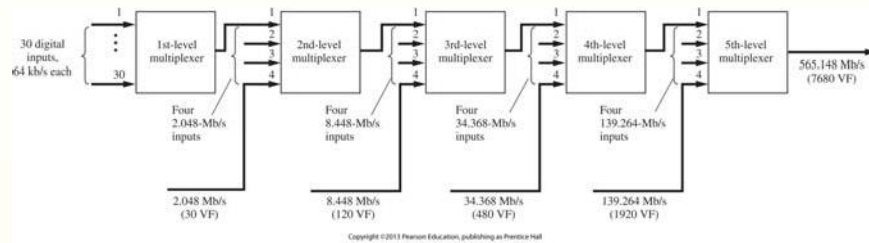


TABLE 3–10 SONET SIGNAL HIERARCHY

TABLE 3–10 SONET SIGNAL HIERARCHY

| Optical OC Level | Electrical STS Level | Line Rate (Mbits/s) | Equivalent Number of | | |
|------------------|----------------------|---------------------|----------------------|--------|-----------|
| | | | DS-3s | DS-1s | DS-0s |
| OC-1 | STS-1 | 51.84 | 1 | 28 | 672 |
| OC-3 | STS-3 | 155.52 | 3 | 84 | 2,016 |
| OC-9 | STS-9 | 466.56 | 9 | 252 | 6,048 |
| OC-12 | STS-12 | 622.08 | 12 | 336 | 8,064 |
| OC-18 | STS-18 | 933.12 | 18 | 504 | 12,096 |
| OC-24 | STS-24 | 1,244.16 | 24 | 672 | 16,128 |
| OC-36 | STS-36 | 1,866.24 | 36 | 1,008 | 24,192 |
| OC-48 | STS-48 | 2,488.32 | 48 | 1,344 | 32,256 |
| OC-192 | STS-192 | 9,953.28 | 192 | 5,376 | 129,024 |
| OC-768 | STS-768 | 89,813.12 | 768 | 21,504 | 516,096 |
| OC-3072 | STS-3072 | 159,252.48 | 3,072 | 86,016 | 2,064,384 |

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Figure 3–42 T1 TDM format for one frame.
On every sixth frame this VF PCM bit is replaced by a signaling bit for this channel.

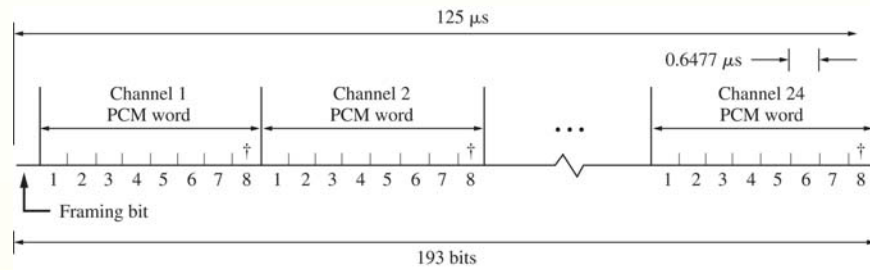


Figure 3–43 Pulse time modulation signaling.

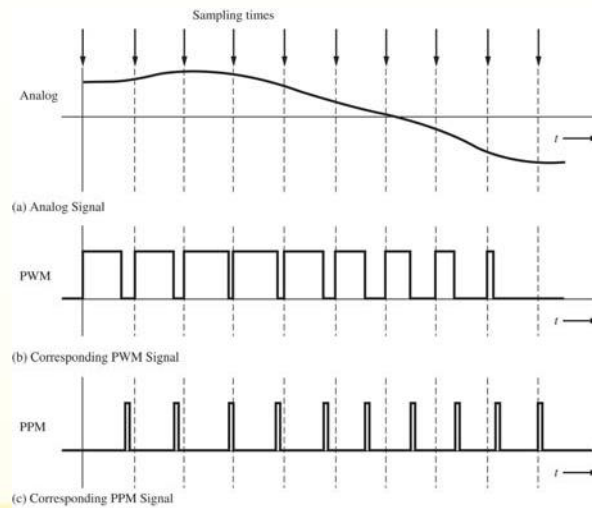


Figure 3–44 Technique for generating instantaneously sampled PTM signals.

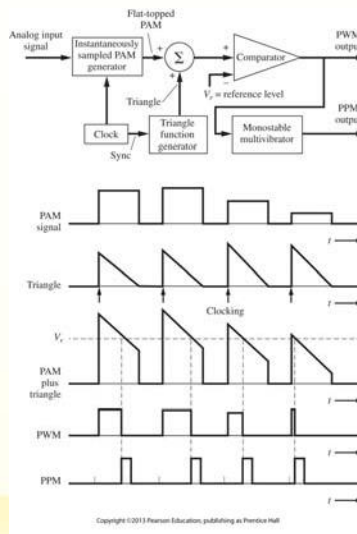


Figure 3–45 Technique for generating naturally sampled PTM signals.

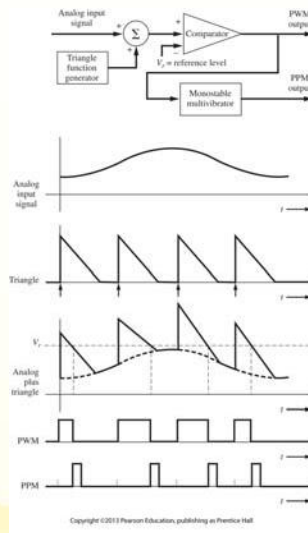


Figure 3–46 Detection of PWM and PPM signals.

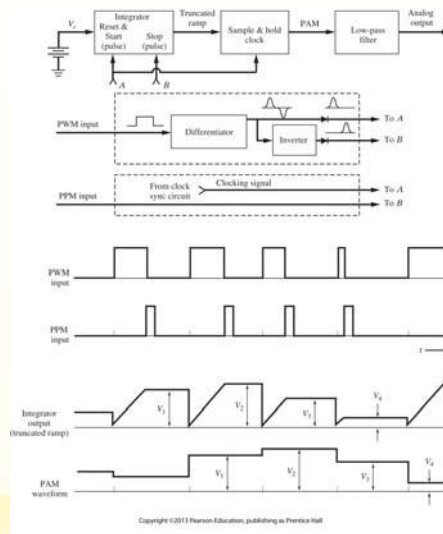


Figure 3–47 Solution for SA3-1. (See SA3_1.m.)

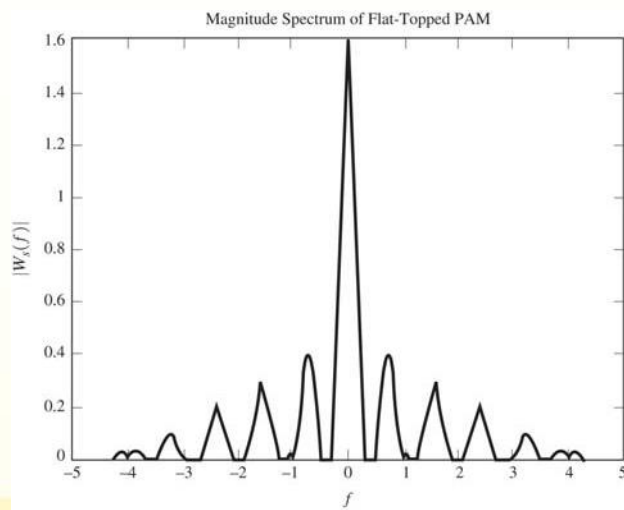


Figure 3–48 PSD of an RS-232 signal with a data rate of 38,400 bits/s. (See SA3_4.m.)

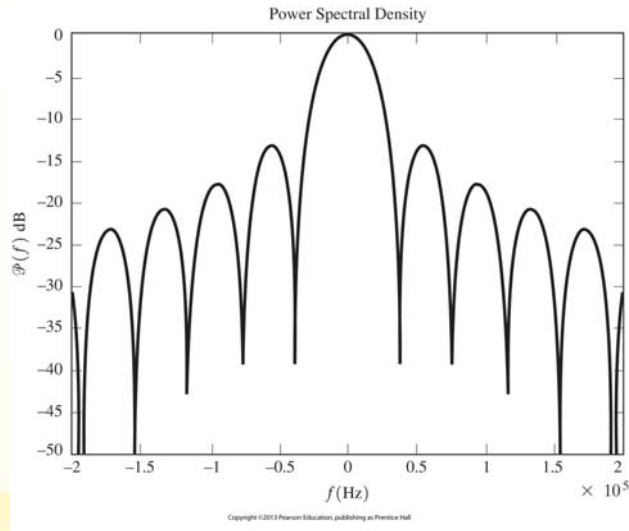


Figure P3–3

