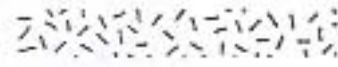


*Geophysical**Well**Logging***W**

e can gain direct access to rocks beneath the earth's surface by drilling. The best samples are obtained by core drilling, but this method is very costly and is seldom practical for depths of more than a few thousand feet. In addition, the conventional methods of deep drilling produce rock cuttings that are flushed from the borehole by drilling fluids. Because these rock cuttings become mixed and contaminated by the drilling fluid, they can be difficult to interpret. Furthermore, these broken fragments tell us little about

the porosity and permeability of the unbroken matrix of rock, or the natural fluids in the pore space. Therefore, instruments have been developed for measuring certain properties directly, while they are lowered in a borehole. The operation of such instruments is called *well logging*, and the strip chart on which the measurements are plotted is called a *well log*.

Geophysical well logging was introduced in 1928 by two brothers, Conrad and M. M. Berger. They devised a probe that could be lowered in a well, continuously measuring resistivity as it moved past different rock formations. A strip chart, the electrical output of the probe, was produced while the operation was underway. Variations in resistivity indicated the boundaries between different lithologic units more clearly than the rock cuttings obtained while the well was being drilled.

In the decades that followed, the inventory of well logging instruments expanded. Improvements increased the variety of electrical measurements. Resistivity was measured with different electrode configurations, and natural voltages were recorded. Several values were recorded simultaneously by means of a probe, called a *sonde*, on which several electrodes were mounted. These values could be analyzed in different combinations to estimate formation resistivity and to make inferences about the natural fluids filling the pore space.

Later improvements included the addition of devices to log radioactivity. These devices measure levels of natural gamma radiation, and they measure radiation produced by bombarding the formation with atomic particles. At about the same time, other logging tools were developed for measuring seismic wave speeds close to the wall of the well. This is called sonic logging. Combinations of radioactivity and sonic logs have proved very useful for determining formation density, and porosity. On a more limited scale, borehole gravimeters and magnetometers have been used in well logging operations.

In this chapter, we begin with a discussion of well drilling to point out certain factors that must be considered in interpreting well logs. Then we will describe the conventional methods for well logging and introduce methods for interpreting them. The general objective of well logging is *formation evaluation*. Well logs are used to discover as much as possible about the geology of the rock formations penetrated by a drill.

WELL DRILLING

Most modern well drilling is done with rotary drills and with percussion drills. The rotary drill can be used for both shallow and deep wells. The record depth reached with a rotary drill is more than 40,000 feet. A percussion drill is faster, but it cannot be operated if the well becomes flooded by groundwater while drilling is in progress. This problem restricts its use for the most part to depths of less than a few thousand feet.

Rotary Drilling

The basic parts of a rotary drill are shown in Figure 14-1. Drilling is done with a bit attached at the bottom of a column of tools inside a hollow pipe. The top of this column is connected to a square hollow bar, the *kelly bar*, which passes through a square hole in the rotary table. As the engine turns the rotary table, causing the tool column to rotate at speeds of 100 to 1,000 rpm. The teeth on the rotating bit cut through the rock, working the hole deeper into the formation.

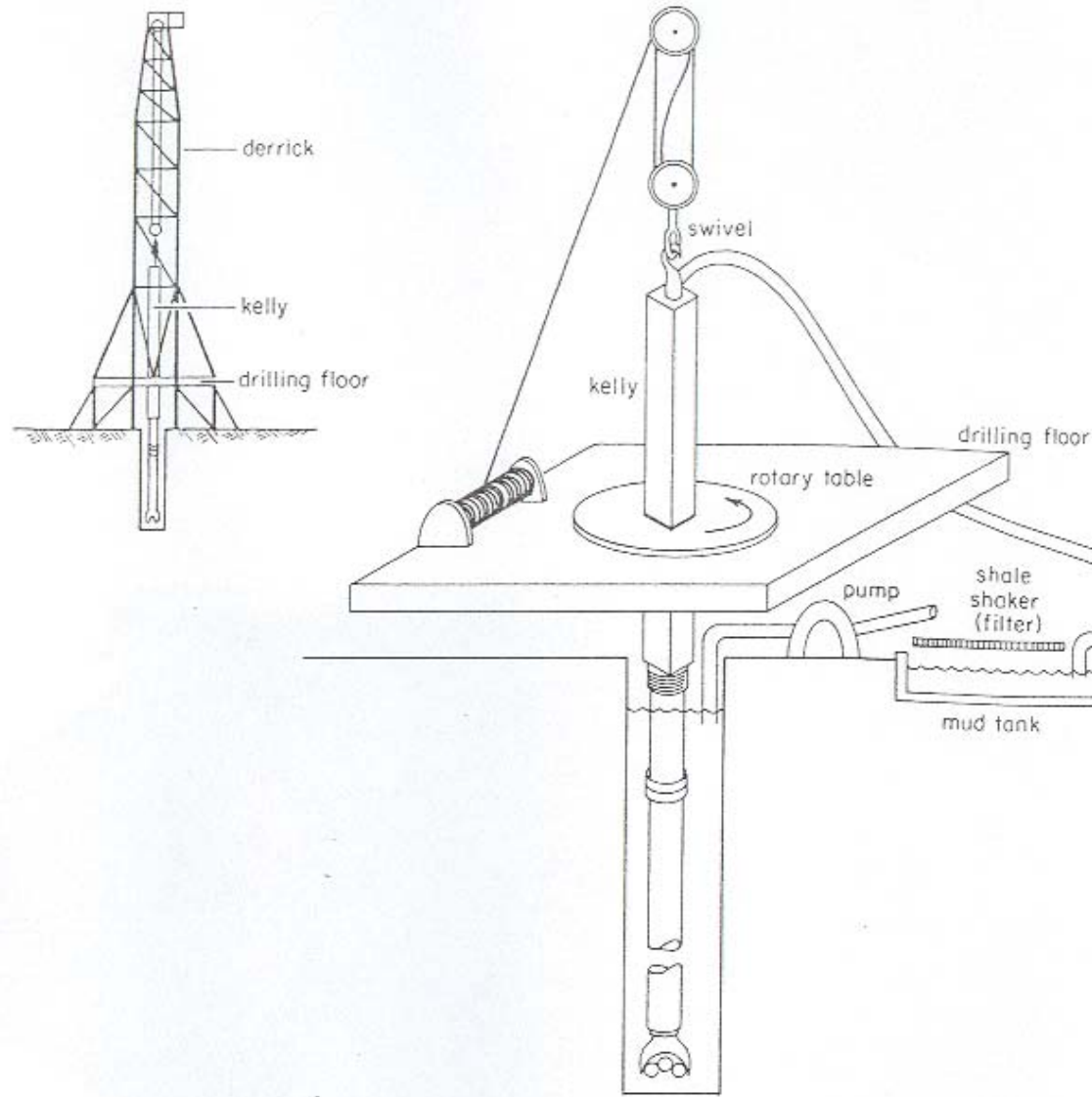


Figure 14-1
Principal parts of a rotary drill. The power system turns the rotary table, which then rotates the entire column of drilling pipe. The bit grinds the

rock at the bottom of the hole. Mud is pumped down through the column of pipe through the hole, flushing out the rock cuttings.

At the same time drilling fluid, stored in the mud tank, is pumped down the column of pipe. It flows out through holes in the bit and rises in the well, carrying the rock cuttings up to the land surface. On the surface the cut-

tings are filtered out, and the fluid returns to the mud tank.

As the well deepens, additional round pipe, threaded at the ends, is added beneath the kelly to lengthen the

Drilling continues until the bit becomes dull. To replace it requires that the entire column be raised by means of the cable and pulleys hooked to the swivel at the top of the kelly. The column is lifted, unscrewed section by section, and stacked in the derrick tower. A new bit is attached and the column is reassembled, after which drilling resumes. The task of disassembling the pipe, changing the bit, and reconnecting the pipe is called "making a trip." In a deep well, this operation can require at least several hours and perhaps more than a day.

Drilling fluid serves several purposes. We have already mentioned that it carries rock cuttings out of the well. For shallow depths water itself is suitable, but in deeper wells a more viscous fluid is desirable to hold the cuttings in suspension. The fluid also lubricates the rotating column of pipe, and it cools the bit. Another important function of the fluid is to seal the rock surface so that pore fluids cannot seep into the well. In this capacity, the drilling fluid acts to prevent gushers and blow-outs that would otherwise occur when the bit penetrates high-pressure oil and gas-bearing zones. To seal the rock surface effectively, the drilling fluid must exert pressure against it that exceeds the pressure of the groundwater, oil, or gas which fills the pores in the rock.

Pressure on the wall of the well depends on the weight of the drilling fluid, which increases with depth. To increase the weight at some particular depth, we must increase the density of the drilling fluid. Particles of different substances are added to turn the drilling fluid into a thicker and more viscous mud. Considerable thought goes into the choice of additives to achieve the desirable weight, viscosity, and lubrication.

By sealing the rock surface, the drilling fluid acts to hide the nature of the pore fluids

that would otherwise seep or gush into the well. Oil- and gas-bearing zones are completely sealed that we have no way of knowing they have been drilled into. One of the principal objectives of well logging is to detect the presence of these hydrocarbons after the well has been drilled. Normally, natural pore fluids prevented from seeping into the well, but because of its high pressure the drilling fluid itself seeps into the well, displacing the natural pore fluids.

The zone surrounding the well where the drilling fluid has infiltrated is called the *zone of invasion*; its structure is illustrated in Figure 14-2. At the side of the well where the drilling fluid first begins to seep into the rock, the additive particles are filtered out of the remaining filtrate with its dissolved solids. The filtrate passes into the rock. Close to the well the filtrate completely replaces the natural pore fluids, creating the *flushed zone*. Beyond this zone is the *annulus of invasion* where the proportion of additive particles diminishes gradationally with distance from the well. As seepage progresses, the additive particles build up a coating on the inner wall of the well called the *mud cake*. It is this mud cake that prevents further invasion.

In relatively impermeable rocks such as shale, the entire zone of invasion is only a few inches into the rock. Porous permeable sandstones and carbonates are invaded to distances of several feet. The mud cake may reach a thickness of several tenths of an inch, and the flushed zone may extend several inches to more than a foot into the rock. To "see through" the zone of invasion into the undisturbed formation requires combinations of several logging devices.

Coring is done using a tool joint equipped with a special hollow anvil

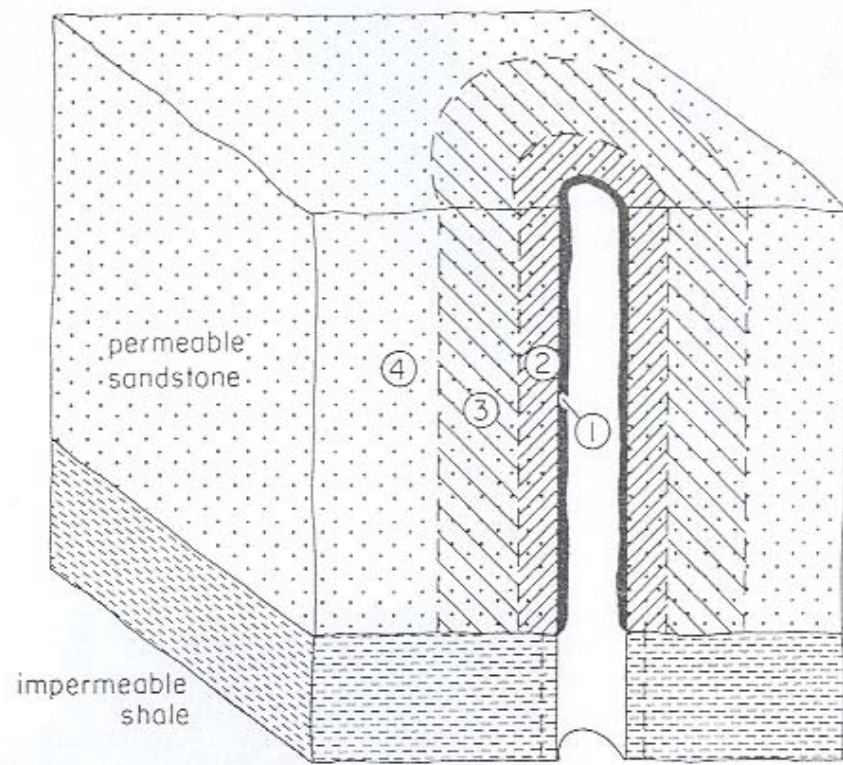


Figure 14-2

The zone of invasion (4) extends much farther into the permeable sandstone than the zone of partial invasion (3). The zone of invasion is (4) the zone of invasion into the formation. The zone of invasion extends much farther into the well in permeable sandstone than in relatively impermeable shale.

(Figure 14-3). The end of the bit is studded with fragments of industrial diamond or some other very hard substance. As the bit turns, it cuts a tubular hole around a solid core of rock which moves into a container, the *core barrel*, inside the column of drill pipe. When the core barrel is full, it is retrieved by "making a trip." This process is carried out much more frequently in core drilling than in noncore drilling, because of the limitation imposed by the length of the barrel, which is ordinarily less than 20 feet. In addition, drilling must proceed more slowly and carefully to minimize core breakage. For these reasons, core drilling is very expensive compared with other non-coring operations. The core drill produces the best rock samples, but the natural formation fluids are flushed out by the drilling fluid.

Percussion Drilling

Modern percussion drilling is a hammer activated by an air compressor. The principle is not unlike that of a hammer commonly used to break up pavement. A percussion drill rig includes a hammer bit, Figure 14-4, mounted at the bottom of the column of pipe. Air from a compressor is pumped through a high-pressure hose into the column and then down the pipe to drive the hammer.

A simplified sketch (Figure 14-4) shows the principal features of a bit assembly. It consists of a hammer attached to the end of the pipe. The hammer moves up and down in a cylinder. Pressured air, pumped into the cylinder, forces the piston downward. This



Figure 14-3
Coring bits studded
with industrial diamonds
(Courtesy of Sprague
and Metcalfe, Inc.)

presses the air that is sealed in the bottom chamber. When the piston is pushed down far enough, the compressed air in the top chamber escapes through holes in the side of the cylinder. Upon release of pressure in the top chamber, the compressed air in the bottom chamber expands, driving the piston upward. This closes the holes, allowing pressure to build up once again in the top chamber. The cycle is repeated several times per second. The rapid pounding of the hammer, which is studded with knobs of tungsten carbide or other hard materials, pulverizes the rock into a fine dust. Air escaping from the upper chamber blows the dust out of the well.

As drilling progresses, lengths of pipe, threaded at the ends, are added to the column. Eventually, the studding on the hammer wears away, and it is necessary to "make a trip" to replace the bit. Percussion drilling usually proceeds faster than rotary drilling. But a depth is reached beyond which the escaping air can no longer remove the rock dust. The depth that can be drilled is also limited by the effect of groundwater seepage, which obstructs the upward flow of air and rock dust.

Casing

Several difficulties in drilling and logging wells are overcome by means of casing. The well is cased by lining it with a column of pipe which is lowered into the hole after the drilling pipe has been removed. Cement is pumped into the well to fill the space between the casing pipe and to fix it solidly in place. This seals the well, preventing contamination fluids from seeping into it and prevents loose rock from collapsing and blocking the hole. After the casing has been set, the well is perforated at particular depths to allow water from an aquifer, or oil and gas from a reservoir, to flow into the well. The casing is sometimes set before a well is drilled, for example, when groundwater is so high that it floods the well so that a percussion well cannot be operated. In rotary drilling, the casing is set to prevent problems with collapsing rock and excessive loss of drilling fluid into fracture zones caused by the casing. After the casing is set, the well is resumed with a smaller bit than the one used through the casing pipe.

Casing creates some serious problems in well logging. Electric logs cannot be run in wells with steel casing. Sonar logs

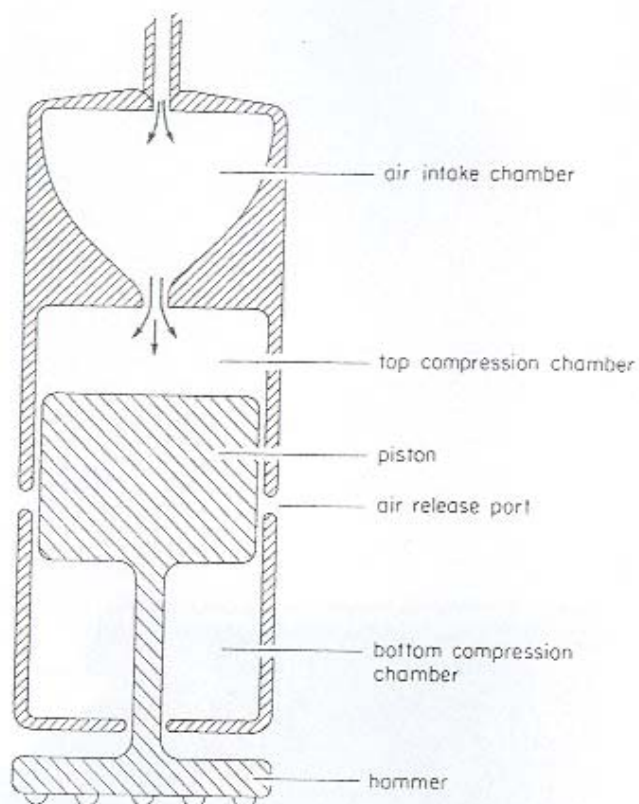


Figure 14-4

Schematic drawing of a bit assembly used for percussion drilling. The hammer is driven by compressed air, which is pumped down through the column of drilling pipe into the air intake chamber. Rock cuttings are blown out of the hole by compressed air escaping from the air release ports.

also be severely distorted. But, certain radioactivity logs can be run effectively where casing prevents other kinds of logging.

FORMATION EVALUATION

The properties of a formation that can be estimated from well log measurements include lithology and bed thickness, porosity, perme-

ability, and the proportions of hydrocarbons occupying the pores. What kinds of information are needed to determine these properties? We will answer these questions first, before describing the logs and the instruments and techniques used to obtain formation data.

Lithology and Bed Thickness

Electrical resistivity, natural voltage, natural gamma-ray, natural radioactivity, sonic log, and seismic wave speed can all help us to identify different lithologies. None of these properties uniquely characterizes particular rock, however. We already know that there is some overlap in the ranges of values measured in typical sandstones, shales, and other lithologies. Nevertheless, differences usually exist for particular sequences of interbedded lithologies in particular areas. For example, in an area with alternating sandstone and shale, the values of natural voltage, radioactivity, and travel time over a fixed interval are high in shale and low in sandstone. These differences (Figure 14-5) exist almost everywhere, even though the actual values in one area can be quite different from those in another area.

Cuttings produced by drilling are used to determine, initially, what kinds of rock are penetrating the well. Because of the mixing that occurs, these cuttings are carried in suspension in the drilling fluid, they do not provide a clear picture of formation about bed thicknesses and positions of bed boundaries. But they do provide some information about what patterns we should look for in logs like those in Figure 14-5, so that we can use them for accurate measurement of these properties and thicknesses.

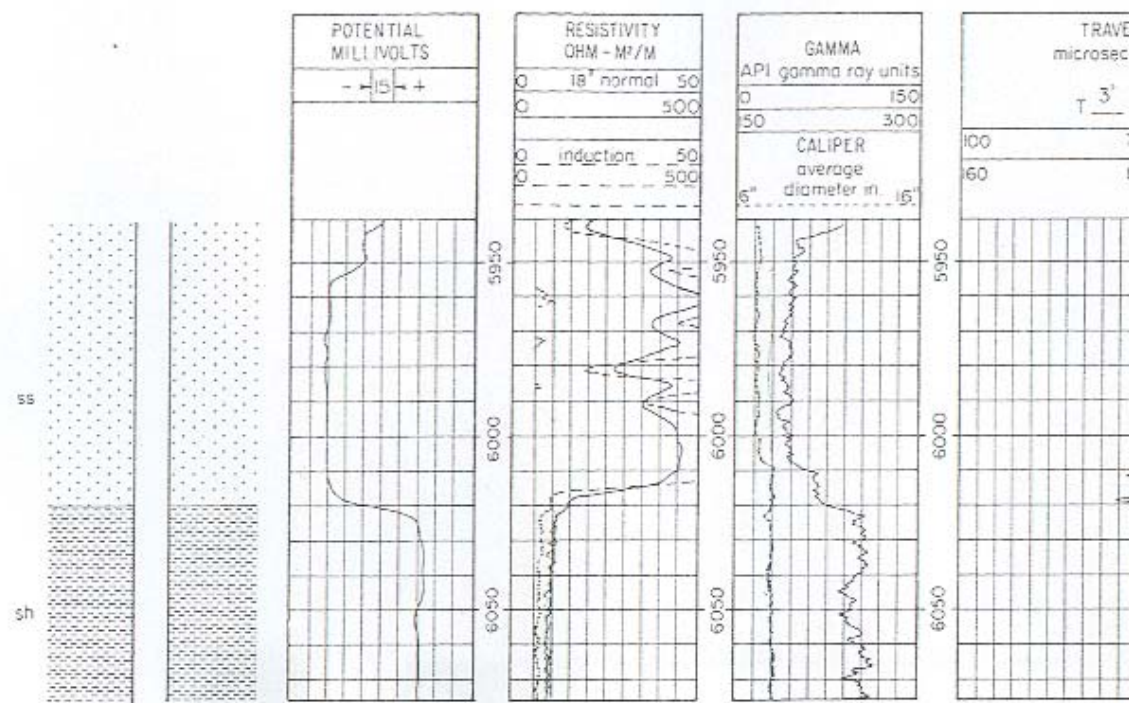


Figure 14-5
 Representative well logs illustrating the variation across the boundary between sandstone and shale layers of spontaneous potential (natural voltage),

electrical resistivity, natural gamma ray, and sonic transit time (*P*-wave travel time) with receivers one foot apart.

The usual practice is to interpret lithology in a well by comparing logs from that well with reference logs from another well in the area in which lithology is already known from careful study of cuttings and, perhaps, rock cores. Patterns of variation corresponding to these lithologic units are recognized by visual correlation of the logs (Figure 14-6). It is useful to know that peaks and troughs on well logs are not usually recorded exactly at bed boundaries. Rather, these boundaries are located by more subtle inflections between the high and low points on a log. The reasons for these subtle indications are discussed in a later section.

For correlation purposes, it is necessary to understand exactly how the patterns of variation are produced by the different rock layers. More important is the ability to recognize the patterns within a pattern that marks a layer boundary. Because different types of logging instruments record different patterns of variation, it is quite difficult to correlate, say, a log from one well with a radioactivity log from another well. Accurate identification of a layer boundary in different wells is possible only by comparing logs recorded with the same kind of instrument. No particular instrument turns out to be generally superior.

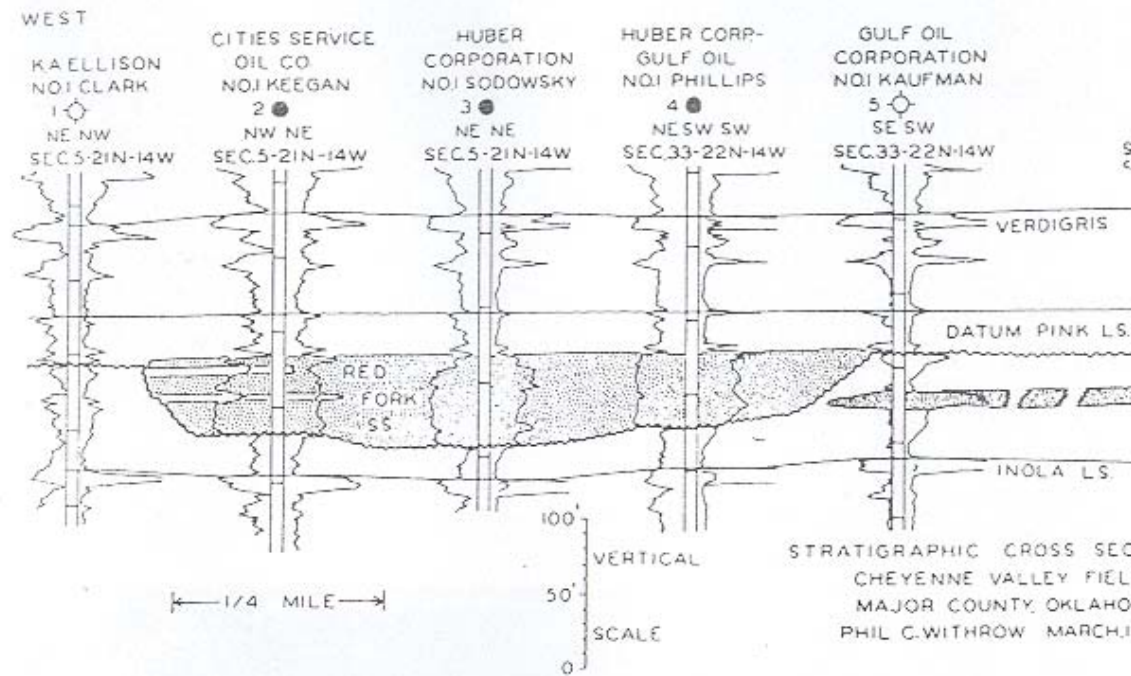


Figure 14-6
Correlation of formation boundaries between different wells based on similar patterns of variation identified on logs from these wells. (From Phillip C. Withrow, *Depositional*

environments of Pennsylvanian Red Fork Sandstone in Northeastern Anadarko Basin, Oklahoma, Bulletin of the American Association of Petroleum Geologists, v. 52, n. 9, pp. 16-17, September 1968.)

areas, resistivity logs are easiest to compare, but in other places the correlation patterns are clearer on radioactivity logs.

Porosity

In a sample of a rock formation, the proportion of the volume that consists of openings between grains, along fractures, and in cavities is the *porosity*. The porosity of reservoir rocks containing petroleum, natural gas, or fresh water is especially important because it indicates the volume of fluid that can be stored in the rock. Methods for estimating po-

rosity from well log measurements are based mostly on experiments that have shown a relationship between porosity and resistivity. In some cases, clear emissions in rock specimens indicate the porosity is known from independent measurements.

Insofar as the pore fluid resistivity is related to the solid matrix resistivity, a relationship between formation resistivity and porosity. In 1942 G. E. Archie established such a relationship. It was determined from laboratory measurements of the resistivity of sandstone cores that had been saturated with water containing different concentrations of dissolved NaCl. The porosities of

were measured by a method independent of resistivity. Archie introduced a property called the *formation resistivity factor* F , which depends on the formation resistivity R_0 and the pore fluid resistivity R_w :

$$F = R_0/R_w \tag{14-1}$$

He then plotted values of F and porosity ϕ that had been found for the different cores on a logarithmic graph (Figure 14-7). Because a straight line could be fitted to this logarithmic plot, he recognized that ϕ and F could be related by an equation of the form

$$\phi = aF^{-m} \tag{14-2}$$

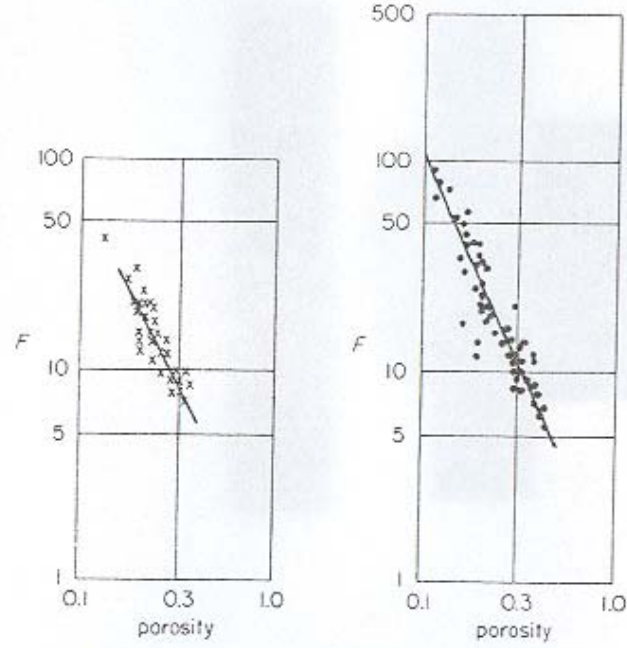


Figure 14-7
Graphs of the variation of formation factor (F) with porosity (ϕ), based on values measured in sandstone cores from two regions. (From G. E. Archie, *Transactions of the AIME*, v. 146, pp. 54-62, 1942.)

where m is a constant that depends on the cementation of the reservoir rock a constant that must be found by test in an area of interest. This equation is known as the Archie formula, has become the most widely used equation in formation evaluation. Tests for many different formations show that values for a are mostly between 1.0, and values for m are mostly between 1.0 and 3.0.

Another property of a formation related to porosity is the compressional wave speed, which well loggers usually measure. The sonic wave speed through the pore fluid is usually different from speed (V_w) through the rock. Because the sonic wave speed (V_0) is characteristic of the formation depends on the proportions of these two parts, it can be related to porosity:

$$\frac{1}{V_0} = \frac{\phi}{V_w} + \frac{1 - \phi}{V_m}$$

The formation wave speed (V_0) can be determined from the travel time (T_0) between two points that are a known distance apart (Equation 14-3). Because these points remain a fixed distance apart on a sonic logging instrument, porosity can be related directly to the travel time:

$$T_0 = \phi T_w + (1 - \phi) T_m$$

where T_w and T_m are travel times for the same distance through a fluid in the pores. The wave speed is V_w and through a solid rock the wave speed is V_m . This formula can be rearranged to find the porosity:

$$\phi = \frac{T_0 - T_m}{T_w - T_m}$$

The last porosity relationship to be considered concerns the formation

This physical property depends on the proportion of pore fluid, which has the density of ρ_w , and the proportion of solid matrix, which has the density of ρ_m . Therefore, it can be related to the porosity:

$$\rho_0 = \varphi\rho_w + (1 - \varphi)\rho_m \quad (14-6)$$

This equation can be rearranged to obtain

$$\varphi = \frac{\rho_m - \rho_0}{\rho_m - \rho_w} \quad (14-7)$$

We know that density of formation water is close to 1 g/cm^3 , and that the matrix density is typically between 2.6 and 2.7 g/cm^3 . Radioactivity can be used to estimate the formation density in two ways. The first employs a device for bombarding the formation with electromagnetic photons, which become scattered by collisions with electrons in the formation. As a result of the scattering process, a certain proportion of these photons are returned to a detector. This proportion depends on the concentration of electrons, hence the density (ρ_0) of the formation. The other method bombards the formation with neutrons which become absorbed into atomic nuclei in the formation; this causes the nuclei to emit gamma rays. The level of gamma radiation reaching a detector depends on the formation density. Values of ρ_0 measured in these ways can be used in Equation 14-7 to calculate porosity.

Water and Hydrocarbon Saturation

The pore space in rocks is almost everywhere filled with water. Except at shallow depths, this water ordinarily contains some dissolved NaCl and other ions. Because of these dissolved constituents, the water becomes a good

electric conductor with low resistivity. In contrast, the common rock-forming minerals making up the solid matrix of a formation are poor conductors with high resistivity. Consequently, the flow of electric current through a formation is almost entirely through the water.

Very sparsely distributed in sedimentary rocks are zones containing petroleum and natural gas. These zones are elusive targets of the exploration geophysicist. Petroleum and natural gas, like the silicate minerals, are poor conductors with high resistivity. Therefore, when these hydrocarbons percolate into a reservoir rock, displacing some of the pore water, the electrical resistivity of the formation increases.

A typical reservoir rock contains a mixture of water and hydrocarbon fluids. Because of their lower densities, the hydrocarbons tend to migrate upward, becoming more concentrated in the upper part of the reservoir. As the water is completely replaced by hydrocarbons, the resistivity diminishes gradually to an irreducible level. Therefore, a reservoir containing hydrocarbons tends to have an upward increase in electrical resistivity.

For purposes of estimating production from a well, it is useful to know the proportions of water and hydrocarbons in different parts of the reservoir by means of resistivity measurements. In 1942 C. S. G. proposed a formula for finding the water saturation, otherwise called the *water saturation* (S). It is based on laboratory measurements of the resistivities of sandstone cores with different proportions of petroleum and water having a fixed salinity. Logarithms of S and the fraction R_0/R_T could be plotted as straight lines, indicating that

$$S = (R_0/R_T)^{1/n}$$

where R_t is the resistivity of rock containing a mixture of hydrocarbons and water, and R_0 is the resistivity of the same rock matrix completely saturated with water. Because the formation factor F is defined in terms of rock that is completely water-saturated, the formula can also be written as

$$S = (FR_w/R_t)^{1/n} \quad (14-9)$$

where R_w is the resistivity of the water that partly fills the pore space. In a reservoir where the water saturation (S) decreases gradationally upward, the value of R_0 must be measured from well log readings in the lower part that is completely saturated with water.

Permeability

The capacity of a formation to transmit fluid is called its *permeability*. It depends on the extent to which the pores are interconnected and on the diameter of the openings. It is the most difficult property to estimate from well log measurements.

The permeability of a core sample of rock can be measured with the apparatus shown schematically in Figure 14-8. Fluid is forced to flow through the specimen by applying different pressures at either end. The permeability (k) can be expressed in terms of the discharge (q , volume per unit of time) through the core, the length (L) of the core, the pressure difference ($P_1 - P_2$), and the viscosity (μ) of the fluid:

$$k = \frac{q\mu L}{P_1 - P_2} \quad (14-10)$$

The permeability has units of area, the most common being the *darcy*, which has as its value 1 darcy = 0.987×10^{-8} cm²; and the *millidarcy*, with the value 1 darcy = 1000 millidarcies.

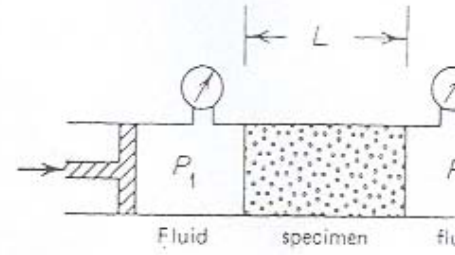


Figure 14-8 Schematic diagram of the apparatus permeability in rock cores. Pushing on the left and drawing out the plunger on the right makes the pressure P_1 in the left chamber higher than the pressure P_2 in the right chamber. This pressure difference causes fluid to flow through the specimen from the left chamber to the right chamber.

Using permeability measurements on limestone cores, G. E. Archie showed that the permeability (k) and the corresponding formation factor (F) plotted close to a straight line on a logarithmic graph (Figure 14-9). Other factors such as the capillary pressure, which depends on the diameters of the interconnected pores, also influence permeability. Other factors cause the inclination of the straight line to change too much from place to place to obtain a reliable relation between k and F .

Additional experimentation has shown that capillary force effects can be expressed in terms of the capacity of the rock to hold water. We know that migrating hydrocarbons are able to displace all but a minimum amount of water. This minimum fraction of water is called the *irreducible saturation* (S_{irr}). The value of S_{irr} is estimated from resistivity measurements on a reservoir formation in which water saturation is decreased to the irreducible level by hydrocarbon displacement.

A relation between permeability and formation resistivity factor is evident

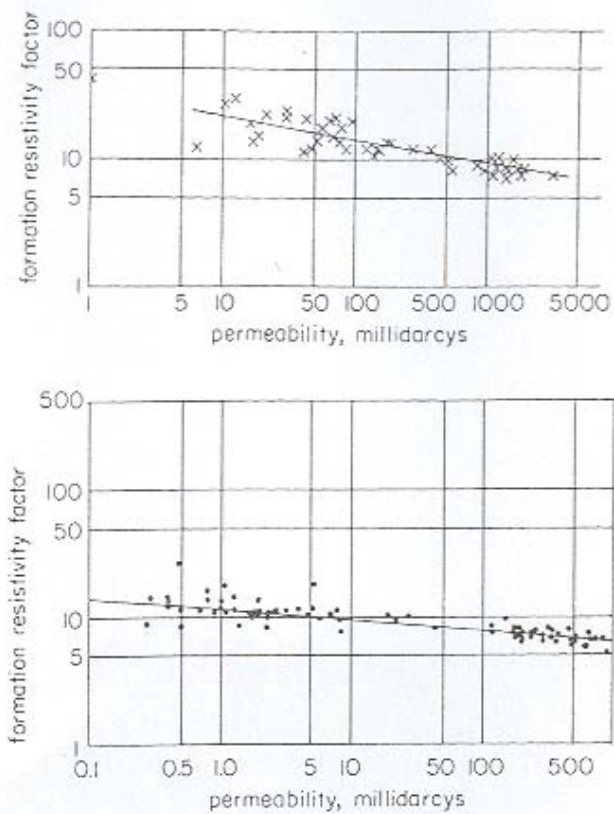


Figure 14-9

Graphs of the variation of formation factor (F) with permeability (k), based on values measured in sandstone cores from two regions. (From G. E. Archie, *Transactions of the AIME*, v. 146, pp. 54-62, 1942.)

14-9. We know from Equation 14-2 that the formation resistivity factor also depends on porosity. These two facts suggest that permeability is influenced by porosity. Measuring permeability in rock cores having different porosity and water saturation tests the combined effects of porosity and capillary force. Graphs of the results indicate the following approximate relation,

$$k \approx (C\phi^3/S_{irr})^2 \quad (14-11)$$

where the constant C depends on the lithology and average grain size of the rock. The prob-

lem with using this formula for permeability is that values of ϕ must first be estimated from well logs. Any error in ϕ will be magnified, and errors in S_{irr} and C will be twofold in the estimate of k . This is why permeability is a difficult measure.

We have now introduced some formulas that are used for quantitative evaluation. To use these formulas we are able to measure electrical properties, resistivity, and sonic wave speeds in a well. We turn now to the well logging procedure that provides this information.

ELECTRIC LOGGING

Electric logging is the procedure of measuring the resistivity and the natural potential in the formations penetrated by the well. The measurements are made with a sonde, which moves in the well on a wire line. Electrodes on the sonde are connected in different circuits to measure resistivity, designed to test the resistivity in different zones of the formation and to detect the natural potential, more commonly called the spontaneous potential (SP). It is necessary to test the resistivity in different zones to correct for the effect of invasion by a drilling fluid that has a resistivity different from that of the formation fluid. We now describe each of the methods used in conventional electric logging.

Special Forms of Ohm's Law

The basis for resistivity logging is Ohm's law, which was introduced in Chapter 13 again at Equation 13-8, which is

Ohm's law used in the analysis of resistivity measurements made with the electrodes placed on the land surface. Recall that in a homogeneous material, current spreads out from the source electrode through concentric hemispherical shells (Figure 13-3). The factor 2π in Equation 13-8 originates from the expression of the area of a hemispherical surface of radius r , which is $2\pi r^2$.

The situation will be different if the electrodes are placed underground so that current can spread out through concentric spherical shells (Figure 14-10) rather than hemispherical shells. Because the area of a sphere of radius r is $4\pi r^2$, the factor 2π in Equation 13-8 must be changed to 4π in the equation we use in the analysis of resistivity measurements made in wells. Otherwise, the same reasoning is used to obtain the following expression of Ohm's law,

$$v_{MN} = \frac{IR}{4\pi} \left(\frac{1}{AM} - \frac{1}{AN} - \frac{1}{BM} + \frac{1}{BN} \right) \quad (14-12)$$

where v_{MN} is the change in potential between two electrodes M and N, I is the current flowing between a source electrode A and a sink electrode B, R is the resistivity of the material in which the electrodes are embedded, and AM, AN, BM, and BN are distances between the electrodes (Figure 14-11).

Let us consider the zone that is tested with the electrode arrangement in Figure 14-11. Observe that electrodes M and N are situated on two equipotential surfaces. The potential difference v_{MN} is related to the flow of current I and the resistivity R everywhere in the shaded zone between these two surfaces. If the electrodes M and N were placed at any other points on these surfaces, the same value of v_{MN} would be measured. The entire shaded zone between these equipotential surfaces is tested.

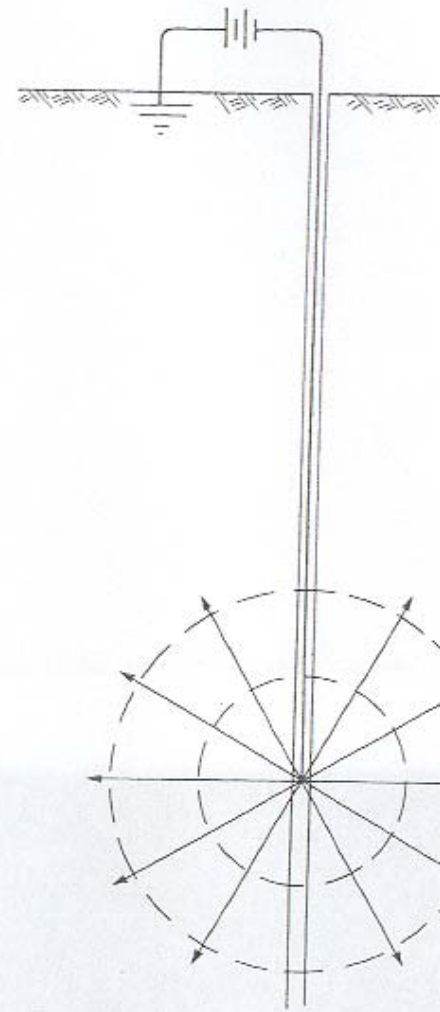


Figure 14-10 Spherical radiation of electric current from a source electrode A and a sink electrode B situated underground, far from the surface, as compared with the hemispherical radiation from electrodes situated on the land surface.

We can express Ohm's law in a form that applies to particular electrode arrangements. It is common practice in well logging to place the sink electrode B on a surface far from the other electrodes. This practice makes the distances BM and BN very large, the terms $1/BM$ and $1/BN$

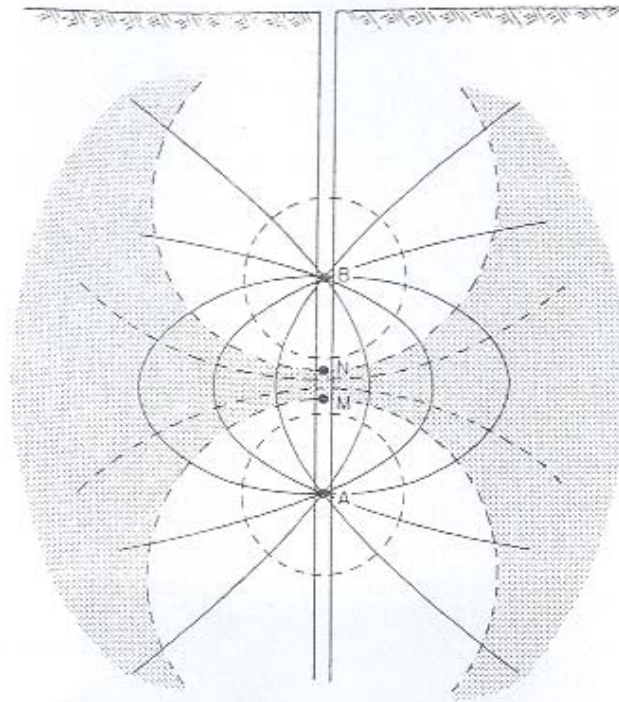


Figure 14-11

Current rays (solid lines) and equipotential surfaces (dashed lines) illustrating the flow of current and the electric field between a source electrode (A) and a sink electrode (B) situated underground in a homogeneous formation. The difference in potential measured between two other electrodes M and N is affected by all the material in the shaded zone between the equipotential surfaces on which M and N are located.

very small and can be neglected. Equation 14-12 can then be modified to the form

$$v_{MN} = \frac{IR}{4\pi} \left(\frac{1}{AM} - \frac{1}{AN} \right) \quad (14-13)$$

In this arrangement, the M and N electrodes are situated on nearly spherical equipotential surfaces, with the A electrode at the center. Therefore, the zone being tested is a spherical shell with inner radius AM and outer radius AN (Figure 14-12).

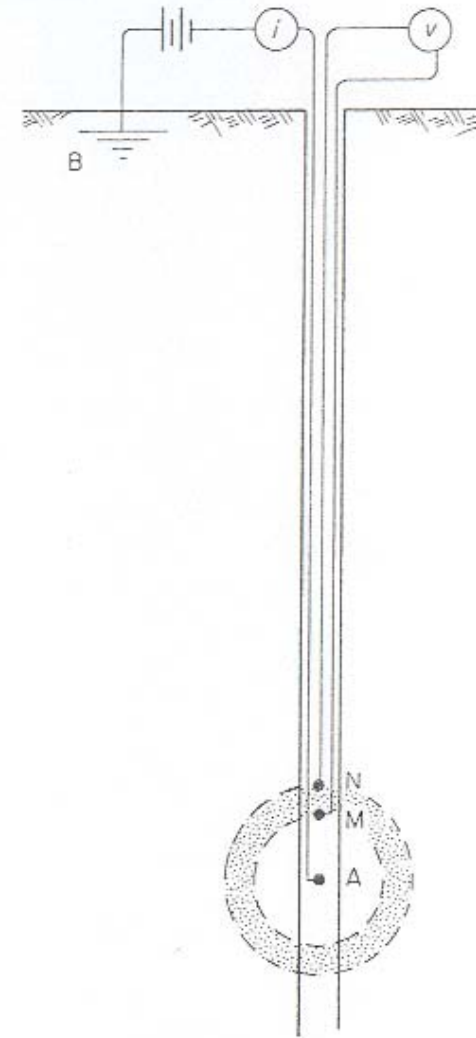


Figure 14-12

Electrode arrangement in which the source electrode (A) is located far from the sink electrode (B), and the difference in potential (v) between the M and N electrodes that are close to A and far from B. The value of v is affected by all the material in the spherical shell having an inner radius AM and an outer radius AN.

Let us consider another electrode arrangement in which A and M are close together, and both B and N are placed far away. Because AN is very large, the term $1/AN$ becomes small enough to neglect. Equation 14-13 can then be modified to obtain

$$v_{MN} = IR/4\pi AM \quad (14-14)$$

The zone tested by this electrode arrangement is a thick shell with inner radius AM and a very large outer radius (Figure 14-13). However, most of the change in potential occurs in the innermost part of this shell. We can understand why by considering the change in potential that would be measured if the N electrode were placed at the distance $AN = 2AM$. By substituting $2AM$ for AN in Equation 14-13, we obtain $v_{MN} = 0.5 \times IR/4\pi AM$, which is one-half the value of v_M given by Equation 14-14. This tells us that one-half of the change in potential found from Equation 14-14 occurs within a distance of $2AM$ from the source electrode. If the N electrode is placed at the distance $AN = 10AM$, the same analysis indicates that 90 percent of the potential change found from Equation 14-14 occurs within a distance of $10AM$ from the source electrode. It is clear, then, that even when the N electrode is placed far from A and M, measurements are the most strongly influenced by rock in a relatively thin spherical shell with the inner radius AM. The gradational shading in Figure 14-13 illustrates how the effect of rock within this zone diminishes with distance from the inner equipotential surface.

Normal Logs

One of the most widely used electrode arrangements for logging resistivity is called the

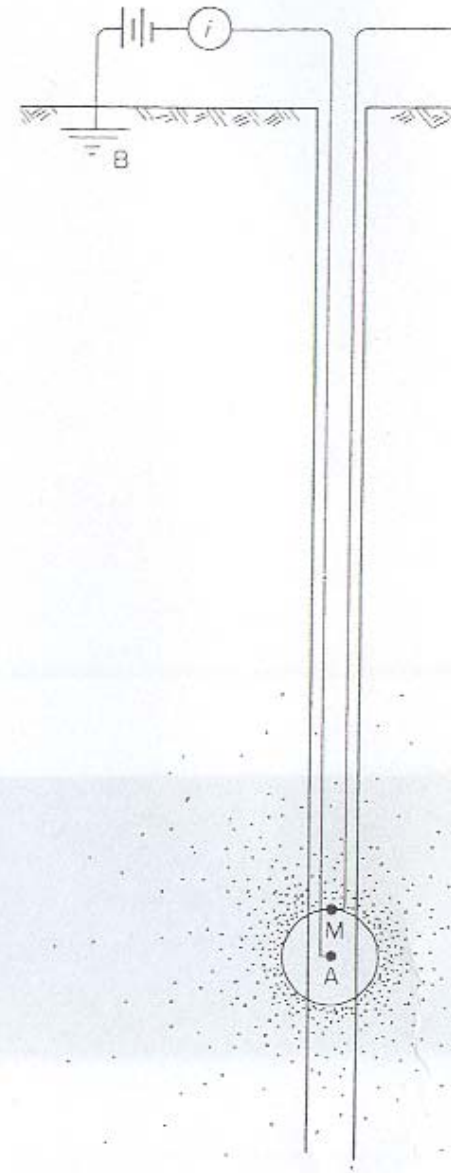


Figure 14-13

Electrode arrangement in which the source electrode (A) is located far from the sink electrode (N). The difference in potential (v) is measured between the M electrode, placed near A, and the N electrode, which is placed far from M. The value of v is influenced by all the material in a spherical shell of inner radius AM and outer radius AN, but material near A has a much larger influence than material far from M, as illustrated by the gradation of shading.

normal electrode configuration (Figure 14-14). Only the source electrode A and the potential electrode M are mounted on the sonde. The sink electrode B and the other potential electrode N are situated far from the sonde. A

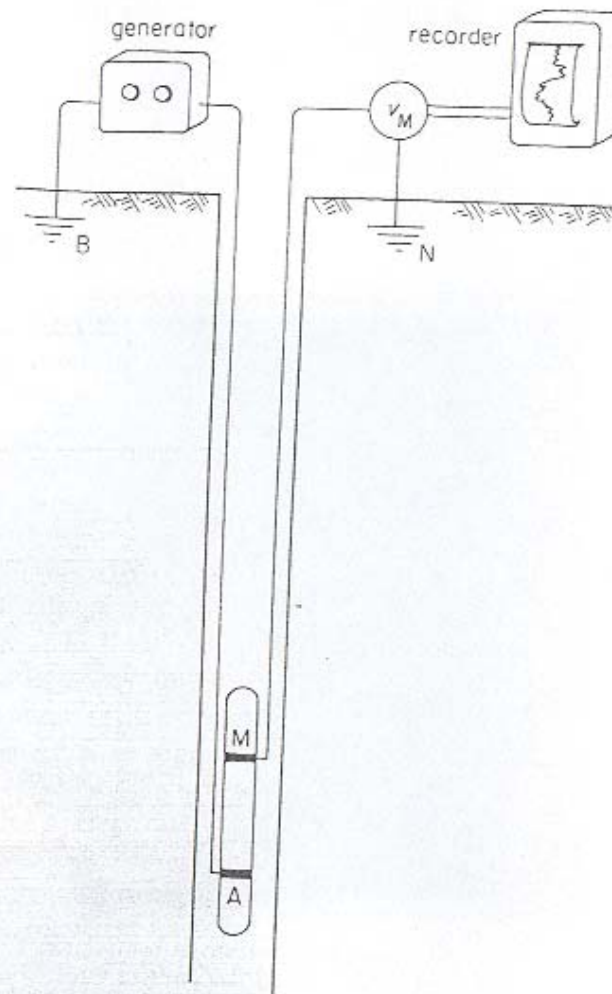


Figure 14-14
Schematic diagram of a normal logging circuit. The source electrode A is far away from the sink electrode B, and the electrode M is far away from the electrode N. The difference in potential v_M is measured between M and N.

generator connected between A and B supplies a constant current I , and the potential v_M is measured between M and N. The voltmeter output is plotted on the recorder as the *normal log*, as the sonde moves down the well. For this electrode configuration the resistivity R is found by rearranging the equation into the form

$$R = \frac{4\pi AM}{I} v_M$$

Because the A and M electrode spacing and the distance apart on the sonde are held constant, we see that R is proportional to v_M . Therefore, the strip chart is scaled in resistivity units (usually ohm-feet) rather than in voltage. It is possible to read resistivity directly from the log.

A normal logging sonde moves through a very thick homogeneous formation. If there is a continuously changing zone of resistivity, as illustrated in Figure 14-13. But normal logging is not done in a homogeneous environment. The zone of testing includes a zone of contrasting resistivity, and the sonde is operated in a well filled with drilling mud which has yet another resistivity. The current emanating from the A electrode spreads out through the drilling mud and the surrounding formation. Rays representing this current refract into different directions at a boundary where the resistivity changes (Figure 14-15). Observe how the equipotential surfaces, which must be perpendicular to these rays, are distorted from their spherical shapes. Because these equipotential surfaces indicate the shape of the zone being logged, it is clear that this zone will not be electrically symmetrical, and that its resistivity will change as the sonde moves through

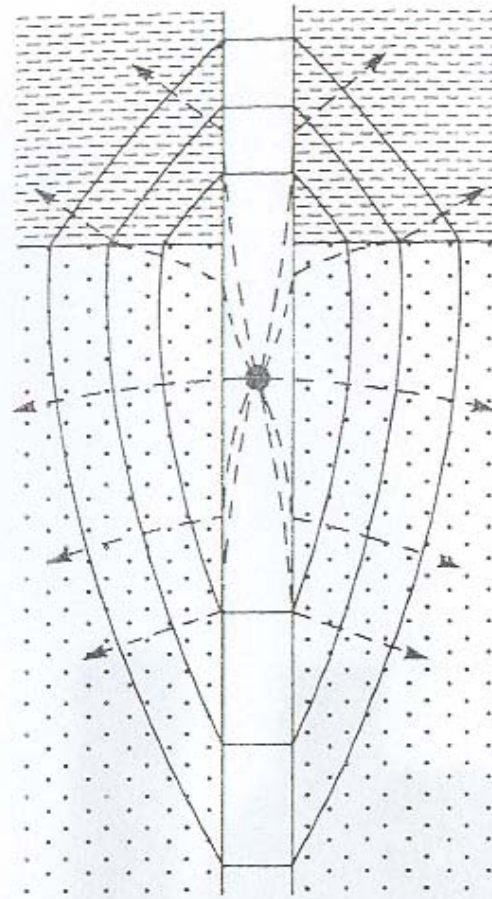


Figure 14-15
 Refraction of current rays at the side of the well and at a boundary between two formations of different resistivities. (From Interpretation Handbook for Resistivity Logs, Schlumberger Document No. 4, Schlumberger Well Surveying Corporation, 1951.)

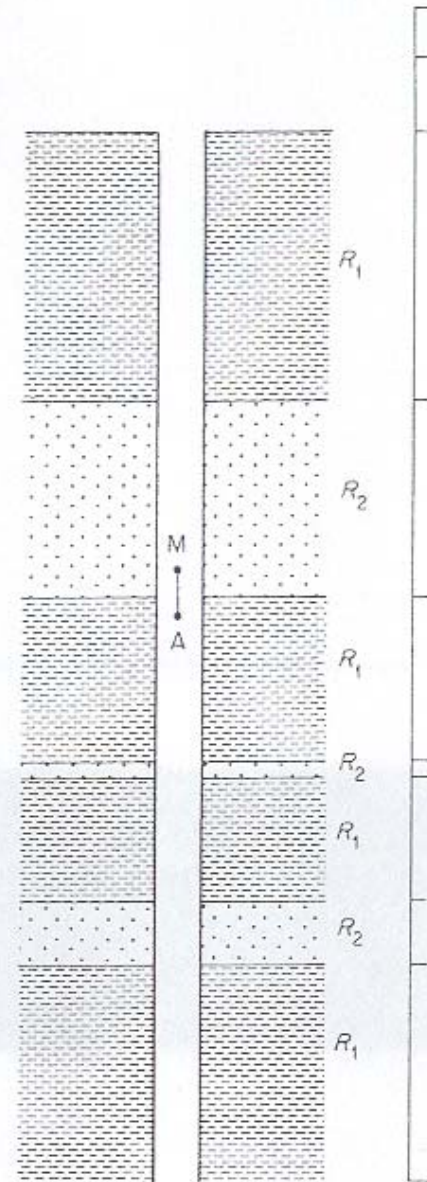


Figure 14-16
 Idealized normal log variation at boundary between beds of different thicknesses and contrasting resistivities. Contrasts between high and low resistivity are properly indicated for the thick bed and M. For the thin bed, the response is considerably thicker than the distance between A and M. For the thin bed, the response is which gives an incorrect indication of resistivity contrast.

this heterogeneous environment, Equation 14-15 expresses only an apparent resistivity that depends on the proportions of the zone of testing which have contrasting resistivities.

Suppose that we obtain a normal log in a well that penetrates beds of contrasting resistivities. An idealized example (Figure 14-16) illustrates how the apparent resistivity changes

as the sonde moves through the well. Observe that there are no abrupt changes in R as the sonde passes bed boundaries. Rather, we see gradational changes. The reason why is that the A and M electrodes mark the inner radius of a zone of testing that reaches beyond the dimensions of the sonde. Therefore, the zone of testing moves through a bed boundary before the sonde actually passes this boundary. Therefore, a nearby bed influences the apparent resistivity measurements, even though the sonde is still moving through another bed.

Observe in Figure 14-16 that the apparent resistivity measured with the sonde near the center of a thick bed comes closest to the true formation resistivity R_f . Here the bed occupies most of the zone of testing, and distortion caused by the beds above and below is at a minimum. For beds that are thicker than $10AM$, the measured resistivity should differ from R_f by less than 10 percent near the center of the bed. For thinner beds, the value of R_f is not accurately indicated on a normal log.

There is a particular problem when a bed thinner than AM is encountered. Look at the apparent resistivity variation near the thin layer in Figure 14-16. Small increases appear at its upper and lower boundaries, but low apparent resistivity is indicated near the center where R_f is high. This distortion results from refraction of current rays, which occurs when the A electrode is below the layer and the M electrode remains above it. The proportion of current flowing in the layer is reduced so that an incorrect measure of resistivity is recorded.

Another factor affecting the measurement of apparent resistivity is invasion. Insofar as the resistivity of the drilling mud differs from that of the natural pore fluid it has displaced, the resistivity in the invaded zone will be different from R_f . Therefore, where invasion is deep, even the apparent resistivity

measured near the middle of a thick bed is quite different from the true formation resistivity.

One aim of electric logging is to determine, for purposes of calculating the porosity, permeability, and saturation of a formation, the problems posed by thin beds. How do they prevent us from obtaining accurate resistivity measurements? To overcome these difficulties, we begin by finding bed thickness and then the depth of invasion. We do this by comparing electric logs recorded with different electrode spacings. The common method is throughout most of the petroleum industry to record a short normal log with an AM spacing of 16 inches, and a long normal log with an AM spacing of 64 inches, as shown in Figure 14-16. We will discuss later how to interpret these logs, which we will discuss later.

What can we learn from logs recorded with different normal logs? Consider first the effect of invasion. Suppose that resistivity in the invaded fluid is higher than the resistivity in the natural pore fluid. The effect of invasion is to increase the resistivity R_i in the zone of testing so that $R_i > R_f$. Next, consider the effect of testing by long and short normal logs. In the long normal log, this zone of testing reaches farther into the undisturbed zone of the formation. Invasion affects a smaller portion of this zone compared with the short normal log. Therefore, the long normal log will indicate a lower value of apparent resistivity. This difference can be seen in Figure 14-16. In both long and short normal logs, the resistivity in the high-resistivity bed between 1750 and 1820 feet. The apparent resistivity values indicated by these logs are compared with values read from standard resistivity charts that have been calculated for beds consisting of beds with different thicknesses, resistivity contrasts, and

invasion.¹ The true resistivity R_t and the depth of invasion are found from the particular chart that best reproduces the apparent resistivities on the 16- and 64-inch normal logs.

Even though the short normal log is more adversely affected by invasion, it is useful for detecting thin beds, which are incorrectly represented on a long normal log. Compare the logs in Figure 14-17 near 6677 feet. Here only the short normal log properly indicates the presence of a high-resistivity bed which must be between 16 and 64 inches thick.

The Lateral Log

Another way to measure resistivity is with the *lateral* electrode configuration (Figure 14-18). The M and N electrodes are placed near each other on the sonde. Farther away in the well is the A electrode, and very far away at the land surface is the B electrode. In the petroleum industry the M and N electrodes are usually spaced 32 inches apart and the A electrode 18 feet, 8 inches from the point O situated midway between M and N. Because it is impractical to operate a sonde of this length, the A electrode is mounted on the wire line above a shorter sonde. The lateral log is almost always operated in combination with normal logs or other kinds of electric logs.

As with normal logging, the procedure in lateral logging is to supply constant current I from the generator connected between A and B. The potential difference v_{MN} is measured continuously with a voltmeter connected between M and N, as the sonde moves through

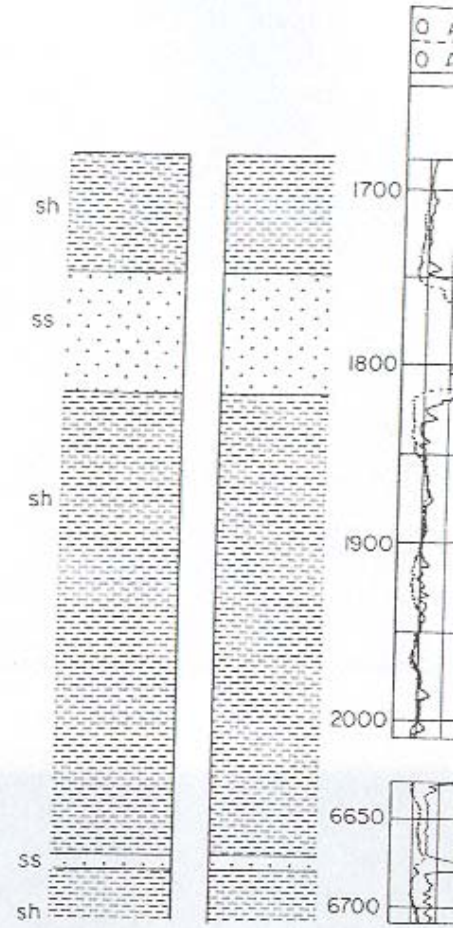


Figure 14-17

The effect of invasion on apparent resistivity measured with 16-inch and 64-inch normal logging devices. The 16-inch normal log is strongly influenced by the high-resistivity zone in the thick sandstone layer. The 64-inch normal log does not properly detect the sandstone bed near 6680 feet.

the well. Because the spacing of the electrodes remains fixed, this potential difference is in direct proportion with resistivity according to Equation 14-13. The lateral log is obtained by recording the voltmeter output on a chart scaled in resistivity units.

In a very thick, homogeneous

¹Interested readers can find correction charts for normal logs and other kinds of well logs in George B. Asquith and Charles B. Gibson, *Basic Well Log Analysis for Geologists*, Tulsa, Okla., American Association of Petroleum Geologists, 1982.

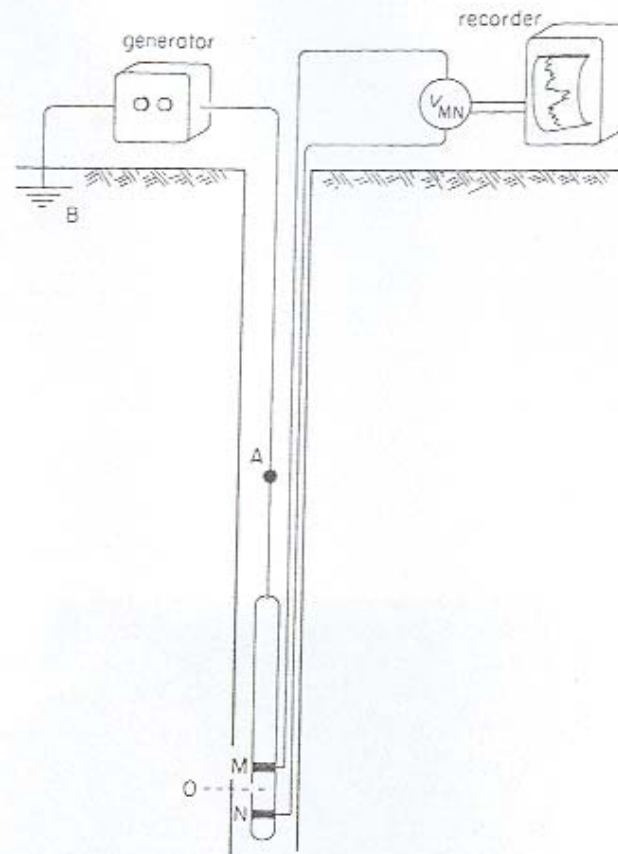


Figure 14-18

Schematic diagram of a lateral logging circuit. The M and N electrodes are quite close to the source electrode A but remain far away from the sink electrode B.

the lateral log would test a spherical shell with inner radius AM and outer radius AN (Figure 14-12). However, in an environment consisting of beds of contrasting resistivities, the zone of testing is distorted into a nonspherical shell because of the refraction of current rays (Figure 14-15). Regardless of this distortion, the zone tested by lateral logging reaches much farther from the well than the zones tested by conventional normal logging. For this reason, a much larger proportion of the

lateral zone occupies formation contaminated by invasion. Therefore, the apparent resistivity measured in a lateral logging tends to be closer to the values obtained from normal logging. Lateral logs have peculiar variations in apparent resistivity near bed boundaries. These distortions are related to the refraction of current rays that occurs where the M and N electrodes are moving through one bed while electrode A is still moving through the overlying bed. This refraction produces typical features of a lateral log that are illustrated in Figure 14-19.

First, let us examine the variation in apparent resistivity related to the thickness of a high-resistivity bed. Observe the small peak that appears close to its upper boundary. This occurs because the M electrode has moved below the boundary while the N electrode remains above it, where the current is concentrated differently. Apparent resistivity increases gradually after N moves below the boundary, and then increases more sharply when the A electrode passes below the boundary. The change ceases in the middle part of the bed where the apparent resistivity level is a value close to R_t . A sharp rise is recorded at the base of the bed, reaching a maximum close to its lower boundary as the A electrode moves below. After N passes this boundary, the apparent resistivity decreases to a moderate level and then diminishes after A, too, moves below the bed.

A different pattern of variation is recorded in the thin, high-resistivity layer in Figure 14-19. The small decrease that is recorded occurs when N passes the upper boundary of the bed by a sharp increase, reaching a peak. After these electrodes pass the lower boundary, the log decreases sharply after M and then after A is moved below the bed. Then, at t

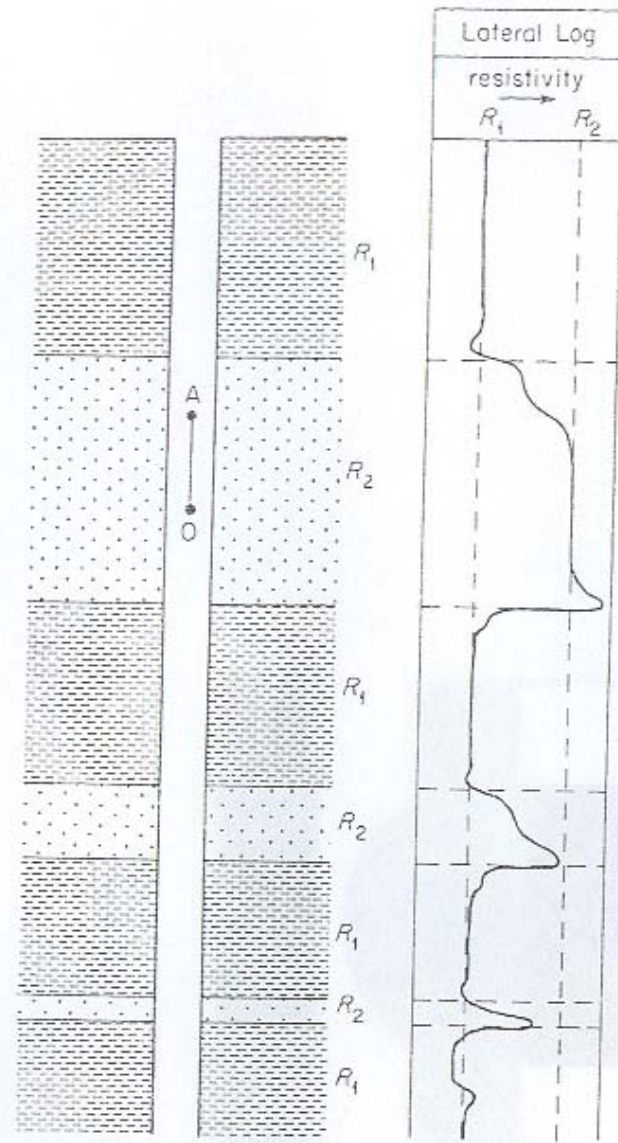


Figure 14-19
 Idealized lateral log variation at boundaries between beds of different thicknesses and contrasting resistivities. The spurious effects are measured close to the bed boundaries and at a distance below a thin bed that is equal to the AO electrode spacing.

AO beneath the bed, a small increase is indicated. This effect is a change in current refraction as the electrode moves through the thin bed. It is a completely spurious variation that should not be mistaken for the effect of another bed.

The advantages of a lateral log over normal logs are (1) a more accurate measurement of R_t in the middle part of a bed and (2) a much sharper indication of bed boundaries. A similarly sharp indication of the upper bed boundary can be obtained by lateral logging with the A electrode near M and N. Deep invasion causes some distortion in the resistivity curve of a lateral log, albeit less severe than that of normal logs. Corrections for the effect of deep invasion can be estimated from standards similar to those used in normal logs. The spurious resistivity variations recorded below thin beds are a serious drawback of lateral logging. When close to thin beds are encountered, it can be difficult to interpret lateral logs.

The Laterolog

The electric logs that we have been discussing are often referred to as unfocused logs because no attempt is made to control the direction of current flow. It spreads out in all directions from the A electrode. Current is refracted at boundaries where resistivity contrasts exist (Figure 14-15). There is a procedure, called *laterologging*, in which circuits are designed to focus the current in particular ways.

The most widely used laterologging method directs the current in a sheet that spreads horizontally outward from the well. One method of accomplishing this is illustrated

14-20. The sonde consists of a short electrode centered between two long electrodes, called the *guard* electrodes, which are connected to each other. Current, which can be controlled separately for the guards and the central electrode, is adjusted automatically to maintain all of these electrodes at the same fixed potential. It then becomes impossible for current to flow

from any one of these electrodes to the other. Therefore, current from the central electrode must move outward in the surrounding formation. Because the potential is constant, the amount of current from the central electrode varies in proportion to the resistivity of the formation into which it flows. The current is plotted on a strip chart scaled in resistivity units to obtain the *laterolog*.

Laterolog sondes ordinarily use a central electrode that is more than five times as long as the guard electrodes. The length of the central electrode can vary from as short as three inches to as long as one foot. The zone tested by the laterolog is a circular disk (Figure 14-21) with a diameter approximately equal to the central electrode length. Within this zone, the rock closest to the well has the greatest effect on the measurement. Closely spaced rays of current flow with the greatest current intensity. The effect of the formation farther from the well diminishes as the rays spread apart.

Compared with unfocused electric logging, the laterolog is much more sensitive to thin beds. It can properly detect a bed as thin as one-tenth of the central electrode length. If the effect of the bed is small, the apparent resistivity measured by the laterolog is close to R_t . However, the effect of the bed can introduce significant distortion because the invaded zone is close to the well. This has a proportionally larger effect on the laterolog than on unfocused electric logging. The principal disadvantage of the laterolog is that corrections can be determined from charts if the depth of invasion can be determined independently from normal and

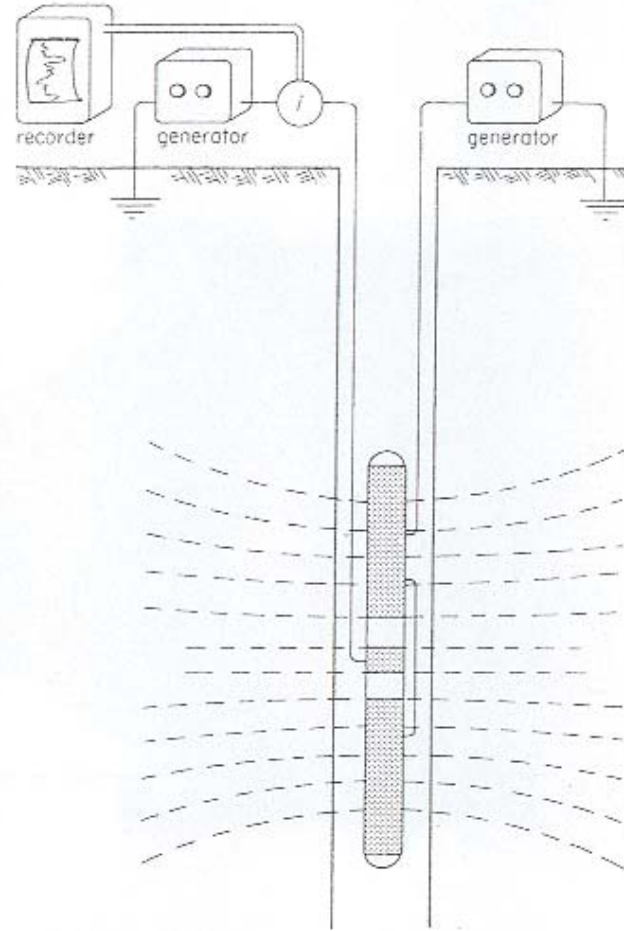


Figure 14-20

Schematic diagram of a laterologging circuit. The effect of the guard electrodes above and below, which are held at the same potential, is to make nearly horizontal current rays (dashed lines) flow outward from the center source electrode.

Induction Logging

Up to this point, we have been concerned with logging devices that introduce current

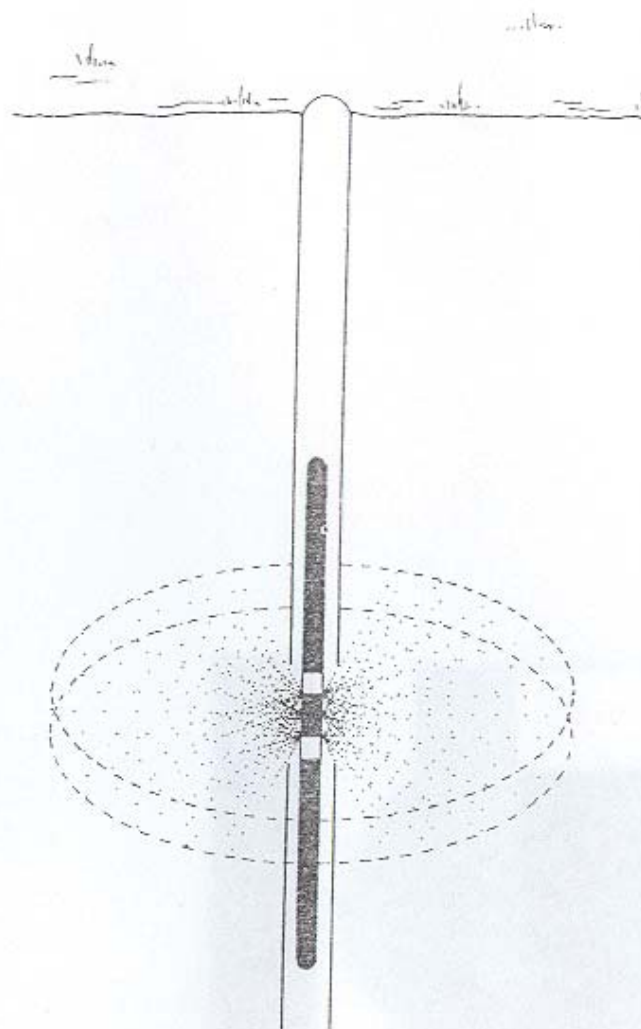


Figure 14-21

The zone tested by a laterolog is a circular disk with a thickness equal to the length of the central electrode. The material closest to the well has the strongest influence on the resistivity measurement. Influence diminishes gradationally with distance from the well, as illustrated by the gradational shading.

formation by means of electrode
a sonde. To reach the formation
first flow from the electrode thro
ing fluid to the side of the well
that the well is filled with noncon
the sonde will be insulated and h
of introducing current into th
This difficulty can be encou
crude oil rather than water is us
the drilling mud.

A different procedure, *indu*
has been developed for opera
filled with nonconducting fluids.
of coils rather than electrode
mounted on the sonde. Electro
duction is the means for introdu
into the formation and for mea
fects. Unfocused induction log
done with a two-coil sonde (Fig
generator produces alternating c
transmitting coil. This alternat
ates an alternating magnetic fie
gion surrounding the coil, which
the formation. Electromagnetic i
sociated with this field compels cu
through the formation in circula
tered on the well. This alterna
current creates a secondary magne
compels current to flow in the re
again by electromagnetic inducti
tensity of the ground current vari
tivity, and so do the secondary m
intensity and the induced curren
ceiving coil. The induced curren
ceiving coil is recorded on a strip
tain an unfocused induction log.

Suppose that the sonde is plac
thick homogeneous formation. Th
sible to calculate the intensity of
magnetic field and the correspon
sity of the ground current at any p
formation. Such calculations help

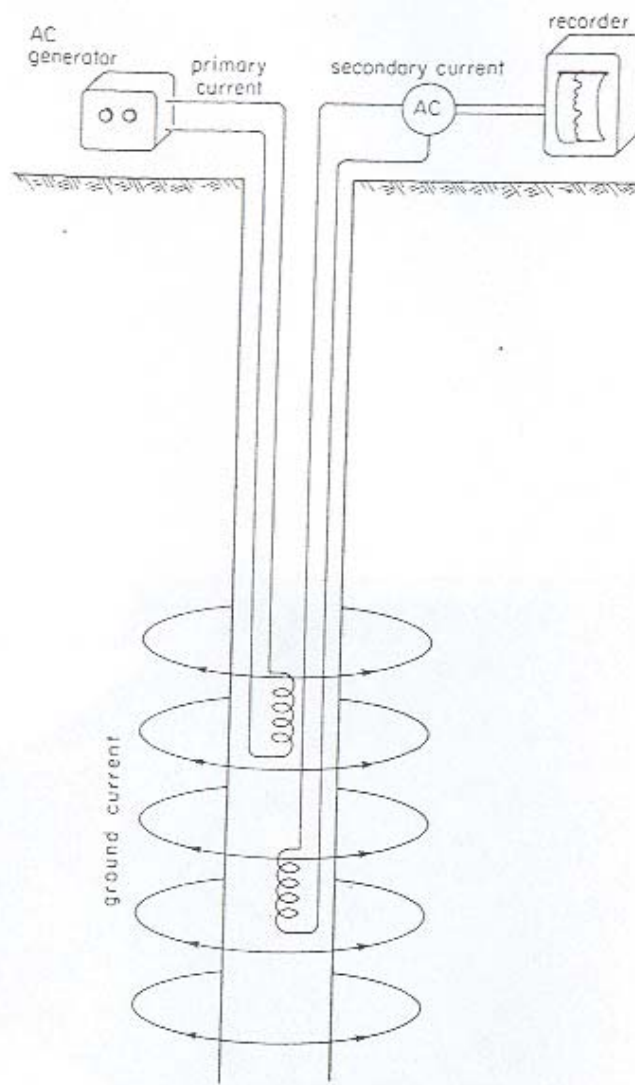


Figure 14-22
Schematic diagram of an unfocused two-coil induction logging circuit, showing the ground currents induced by the alternating magnetic field of the primary coil. The alternating magnetic field associated with these ground currents induces alternating current in the secondary coil.

mine the zone that is tested by the logging procedure. Graphs in Figure 14-23 illustrate how the effect of different formation vary with distance from the well. They show that the ground currents are concentrated mostly in the zone within about three times the coil spacing.

An unfocused induction log records a gradual change in apparent resistivity as the sonde passes the boundary between two beds of contrasting resistivity. This is shown in Figure 14-24. In a thick bed in which the coil spacing is more than three times the coil spacing, either the upper or lower boundary is not measured; the apparent resistivity should be constant unless the results are distorted by invasion. Corrections for invasion can be obtained from standard charts, but additional information is required; this information can be obtained from other kinds of logs.

Observe in Figure 14-24 that the inflection points on the induction log lie close to the boundaries. These inflections can be used to identify boundaries. A sharper indication of boundaries can be obtained by means of focused induction logging. This requires additional control on the ground currents, which is accomplished by adding more coils to the transmitting and receiving circuits. The simplest focusing arrangement is shown in Figure 14-25. Two coils are used. One is in series with the original transmitting coil but is situated further down the well than the original receiving coil; the other is in series with the original receiving coil but is situated near the original transmitting coil. This arrangement is maintained with this arrangement is maintained with the unfocused log in Figure 14-22. Focusing coils produce a sharper indication of bed boundaries, but they introduce oscillations in apparent resistivity. Focusing coils can be arranged in

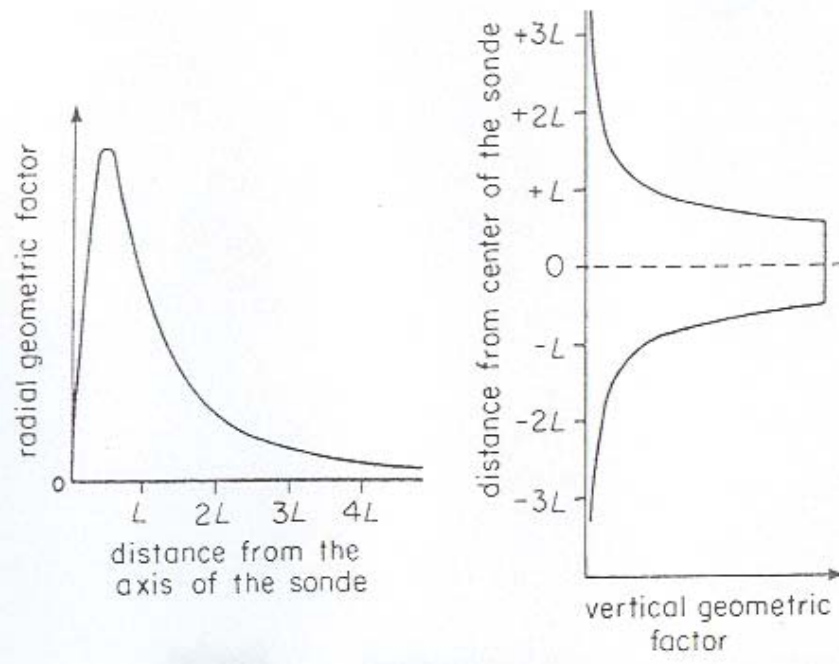


Figure 14-23
 Graphs illustrating the geometric factors read from these graphs at different distances above and below the sonde. (From H. G. Doll, *Introduction to Induction Logging and Logging of Wells Drilled with Base Mud*, *Journal of Petroleum Technology*, AIME, p. 1949.) The distance is in units of coil spacing.

plicated circuits to suppress these oscillations while retaining the steeper change in apparent resistivity at the bed boundary.

The induction log was introduced for the purpose of testing wells filled with nonconducting drilling mud. This logging procedure can also be used in wells containing mud that does conduct current.

Spontaneous Potential Logging

Natural potential differences have been found to exist near bed boundaries. The circuit for measuring these so-called *spontaneous potentials* (SP) is quite simple. A voltmeter is connected between an electrode mounted on a sonde and another electrode fixed at the land surface (Figure 14-26). The SP log is obtained by recording the voltmeter output on a strip chart.

Why do spontaneous potentials develop though their origin is not clearly understood, we have some ideas about the cause. If pore water solutions that have different concentrations are in contact, ions will move across the boundary to equalize the concentration. Insofar as some ions move more easily than others, charge differences can develop, creating potential differences.

Consider the situation in which permeable sandstone is in contact with impermeable shale. Suppose that the sandstone contains the same saline pore water as the shale, however, and the NaCl concentration of the mud filtrate is different from the concentration in the natural pore water near the well, along the boundary between these beds, the mud filtrate in the sandstone is in contact with the natural pore water in the shale.

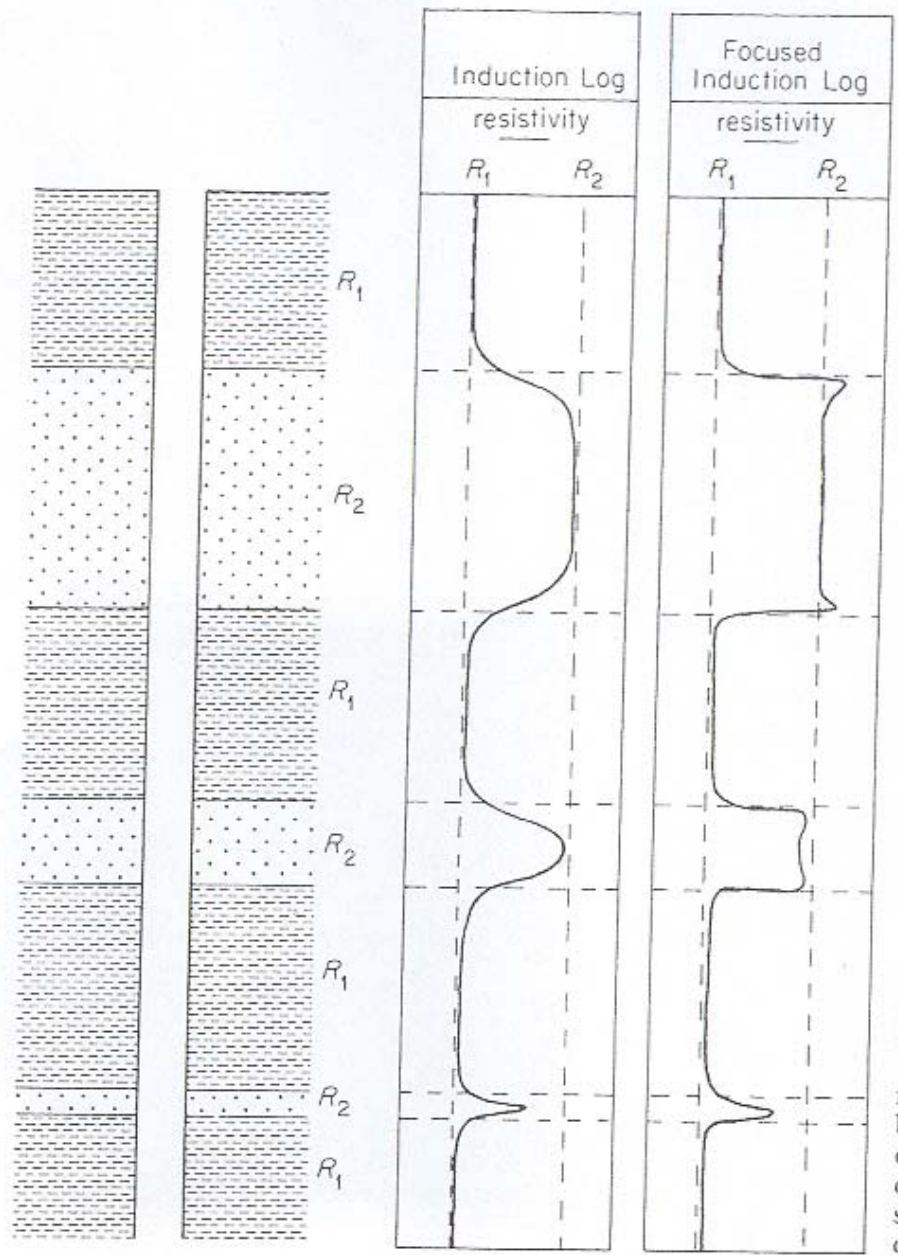


Figure 14-24
 Idealized unfocused
 induction log variati
 boundaries between
 different thicknesses
 contrasting resistivity
 spurious effects are
 close to the bed bound

The movement of ions to equalize the concentrations in these two solutions is impeded by surface charges on the clay particles in the shale. These charges tend to immobilize the negative chloride ions but have little effect on

the positive sodium ions. Therefore, an imbalance develops across the boundary and a spontaneous potential is created. In the permeable sandstone, both sodium and chloride ions are mobile, but

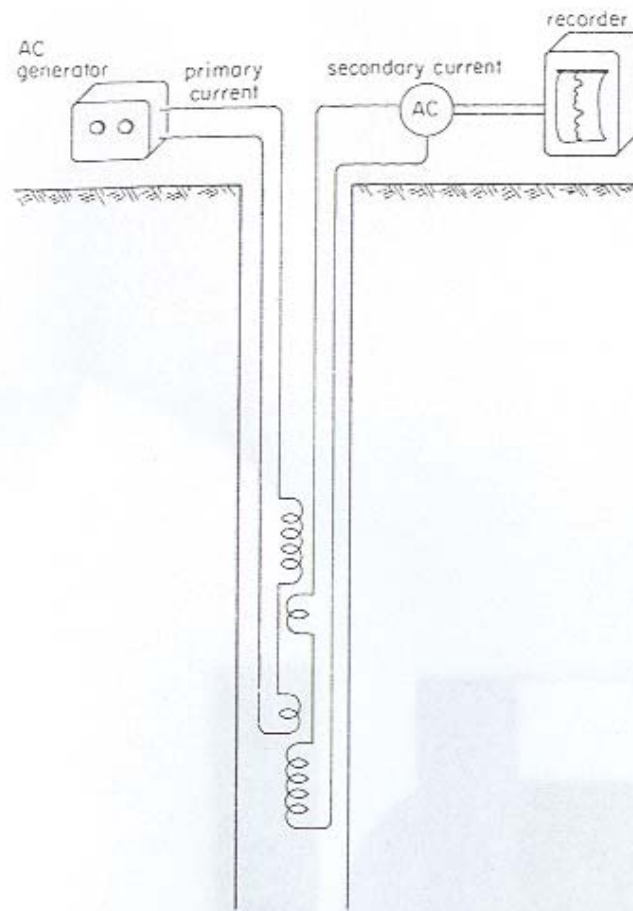


Figure 14-25
Schematic diagram of a focused four-coil induction logging circuit. Both the primary circuit and the secondary circuit contain two coils. The small secondary coil is placed close to the large primary coil, and the small primary coil is placed close to the large secondary coil.

ions tend to move more freely. Therefore, another source of spontaneous potential is the transitional boundary between the mud filtrate near the well and the natural pore water beyond the invaded zone. We do not fully understand the nature of these and other processes that contribute to spontaneous potential variations. But we can measure their

combined effect; it produces a few tens to a few hundred volts.

Some important features of S seen in Figure 14-27. In a sequence of sandstone and shale beds, a negative potential is recorded as the sonde passes from shale into sandstone. This is the opposite of what is recorded with conventional resistivity logs.

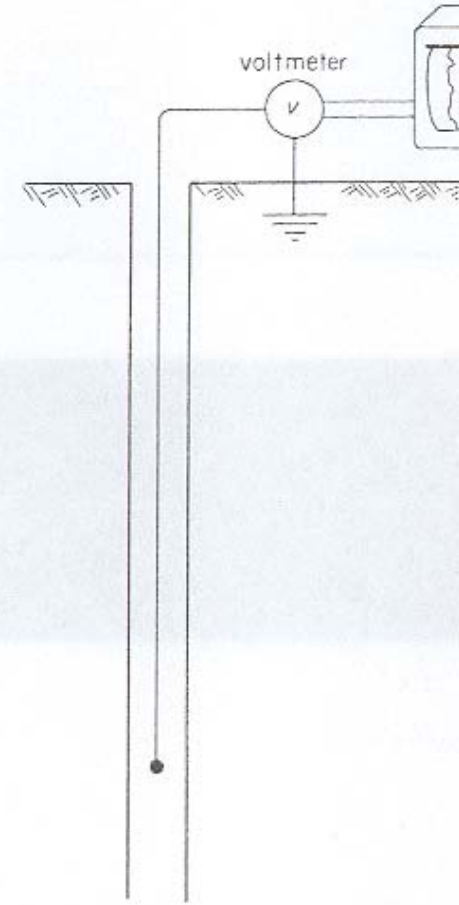


Figure 14-26
Schematic diagram of a circuit for measuring spontaneous potential. The potential is measured between an electrode mounted on the sonde and another electrode placed on the ground surface.

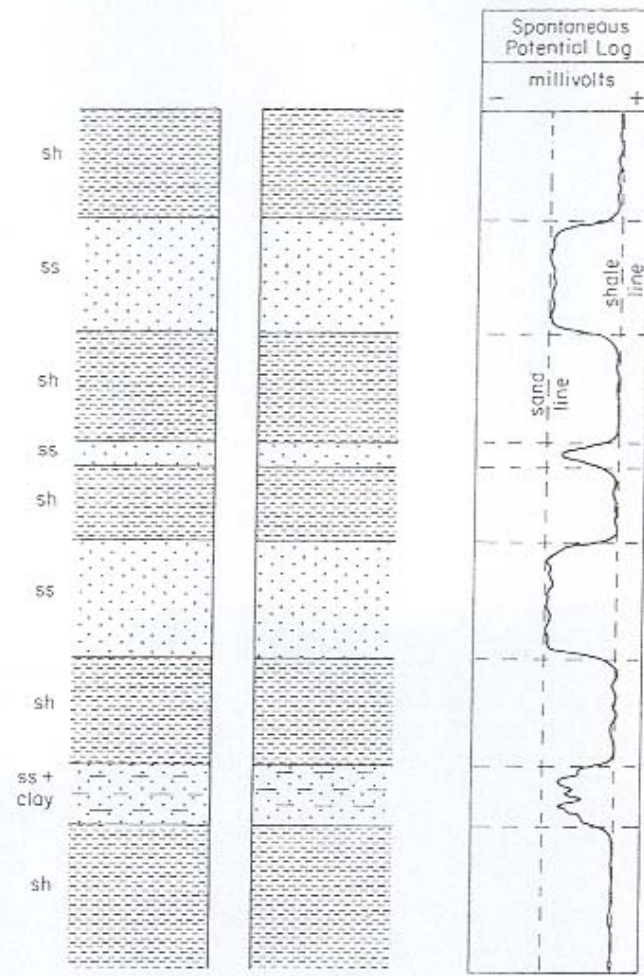


Figure 14-27
Idealized spontaneous potential variations in alternating beds of sandstone and shale. The inflection points on the log occur close to the bed boundaries.

change more steeply, with the inflection point on the curve occurring at the boundary. This feature of the SP log provides an accurate means of locating bed boundaries.

A feature observed in many regions is that all the shale beds are at approximately the same spontaneous potential. Then it is possible to draw a straight line, called the *shale line*

(Figure 14-27), along the right-hand side of the SP log, showing the alignment of the log that were recorded in a well also encounters relatively uncontaminated sandstone uncontaminated by clay. It is not unusual to measure the spontaneous potential in these beds. The *sand line* (Figure 14-27), can be drawn on the left-hand side to show the extremes of these parts of the SP log. Having these two SP extremes, we can detect clay contamination in other beds by intermediate spontaneous potentials measured. If an uncontaminated sandstone is thin, the sharp peak recorded on the log will not reach the sand line. Nevertheless, the boundaries are correctly indicated by inflection points above and below the

Micrologs

Special sondes have been designed for measuring resistivity with very closely spaced electrodes. These electrodes are placed in a well which can be pressed firmly against the side of a well (Figure 14-28). These electrodes are usually one or two inches apart and are connected into different circuits to obtain *normal logs*, *microlateral logs*, and *induction logs*.

These micrologs can detect very thin beds. However, their principal purpose is to measure the resistivity of the mud cake in the well and the resistivity in the interval of interest. These measurements are of critical importance for determining correction factors that are needed to calculate true resistivity from standard-normal, lateral, and induction logs.

Because the microlog electrode is pressed against the side of the well, it has to move very slowly. It is ge-



Figure 14-28

A micrologging sonde with electrodes mounted on a pad which can be pressed against the side of the well. (Courtesy of Schlumberger, Limited.)

practical to run micrologs through the entire depth of a well. Only zones of particular interest are logged.

Electric Log Combinations

The apparent resistivity measured by an electric log depends on the true resistivity R_t in a bed, the resistivity in the invaded zone, and

the resistivities in other nearby beds. By using different electrode configurations test zones of different proportions of these resistivities can be measured by combining apparent resistivities measured with different electrode configurations. How can we calculate R_t ?

The electric logging apparatus consists of a sonde with several electrodes. These are automatically switched into different circuits, so that several logs can be obtained simultaneously on the same strip chart as the sonde moves through the well. In modern operations, the recording equipment and electronic controls are mounted in a truck. The truck also carries the winch and wire line used for lowering and raising the sonde (Figure 14-29). In offshore operations, the same equipment can be installed in a small vessel or is airlifted to an offshore drilling platform. Different combinations of logs can be attached to the wire line, each providing a different combination of logs.

The combination most widely used in the petroleum industry includes the 8-inch normal log, the 8-inch and 64-inch normal logs, and the 8-inch lateral log (Figure 14-30). A very common combination includes the 8-inch normal log, the laterolog, and two induction logs. In both of these combinations, the sonde is used to locate bed boundaries, and the induction logs provide data for estimating formation resistivity measurements. Different sondes equipped for micrologging can be attached to the wire line.

The trucks used for electric logging are usually equipped for radioactivity logging as well as for sonic logging. In addition to chart recorders, these trucks have magnetic tape recorders, which record on magnetic tape, which can be read later on a computer processor. Some carry small computers for on-line data processing.

Not all electric logging is done on land. Trucks designed to operate several

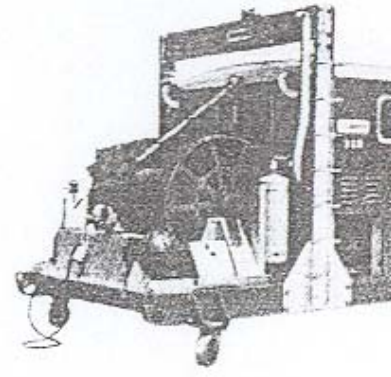
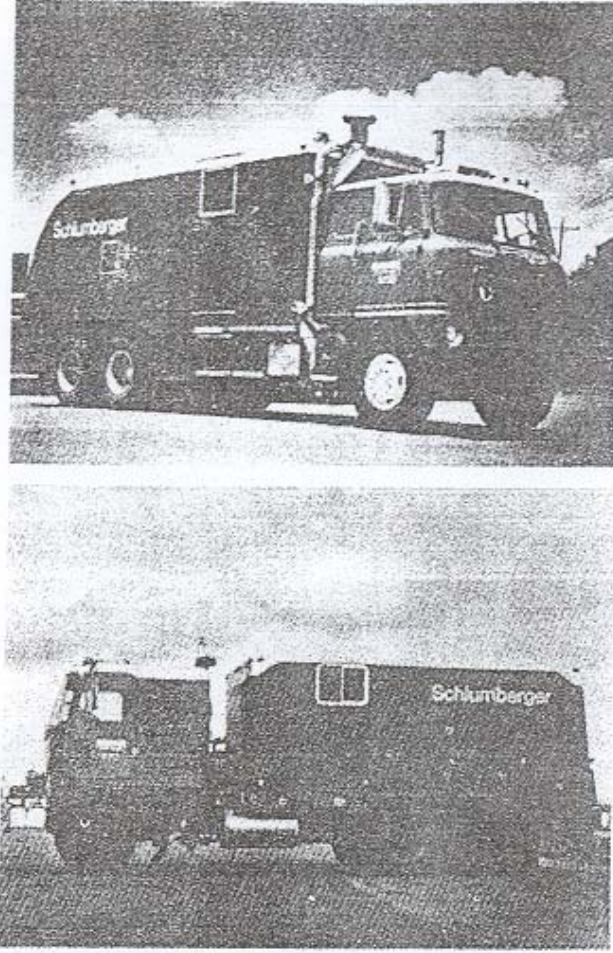


Figure 14-29

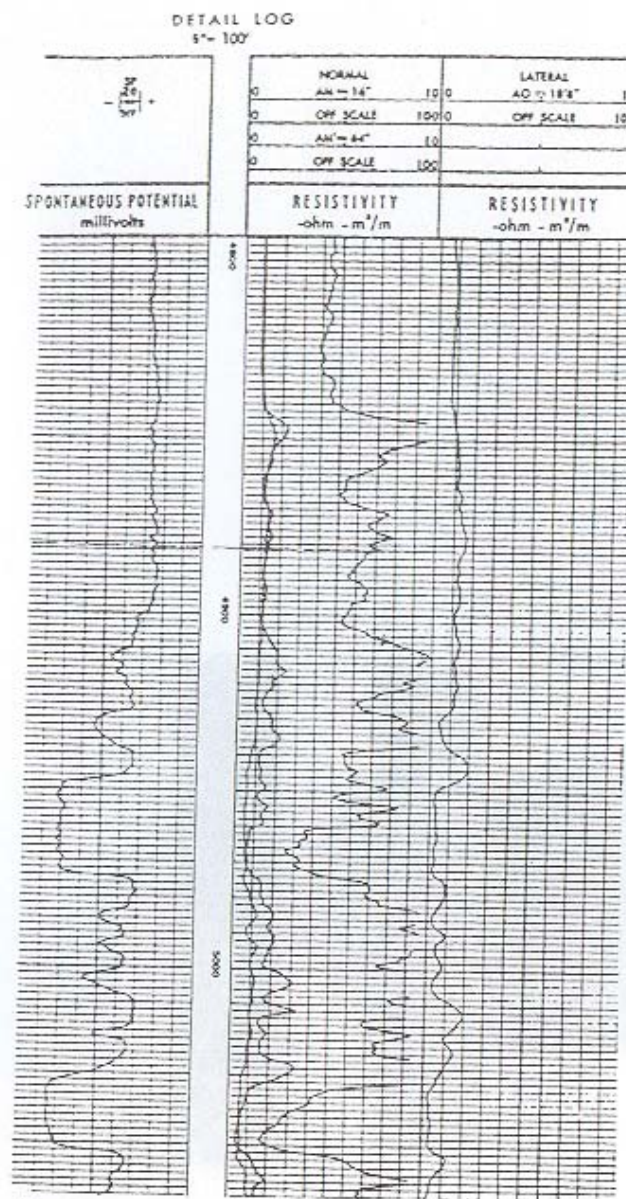
Typical field trucks and winch assembly used in well logging. (Courtesy of Schlumberger)

sondes. There are small, portable units that can be backpacked into remote areas for obtaining SP and normal logs and natural radioactivity logs.

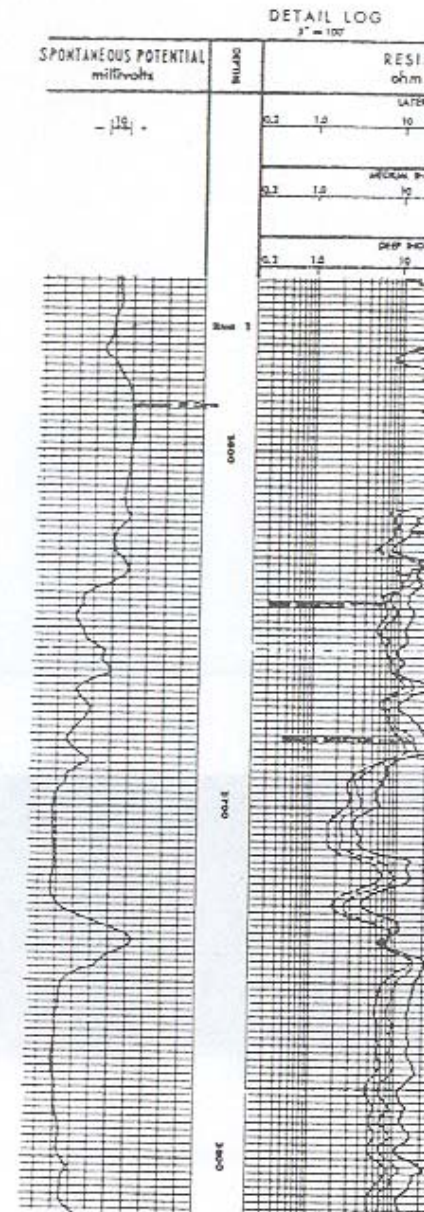
RADIOACTIVITY LOGGING

The process by which particles of mass or energy are spontaneously emitted from an atom is called radioactivity. These emissions consist of protons, neutrons, electrons, and photons of electromagnetic energy that are called

gamma rays. In nature they come from unstable nuclei or radioactive elements such as uranium, thorium, rubidium, and potassium-40. Similar emissions from the same or other elements can be stimulated by bombarding them with gamma rays or neutrons. Radioactivity logging methods make use of both natural and stimulated emissions. There are three methods of radioactivity logging. The first uses a detector mounted on a truck to measure the gamma rays produced by naturally occurring radioactive elements in a formation. In the second method gamma radiation is introduced



(a)
Figure 14-30
 Typical electric log combinations: (a) SP log, 16-inch and 64-inch normal logs, and 18-foot, 8-inch



(b)
 lateral log; (b) SP log, induction logs, laterolog.

the formation from a source mounted at one point on the sonde, and the intensity of this radiation is measured by a detector mounted at another point a fixed distance from the source. In the third method neutron bombardment of the formation stimulates gamma radiation. The neutron source is placed at one point on the sonde, and a gamma-ray detector is mounted at another point.

Common to these three kinds of radioactivity logging is the detection of gamma rays. A device called a *scintillation counter* is the usual instrument; it consists of a special crystal and a photoelectric tube. Certain crystals, such as sodium iodide crystals, emit flashes of light as they absorb gamma-ray photons. A flash of light produced in this way can be converted into a pulse of electric current by a photoelectric tube. Radioactivity logs are obtained by plotting the scintillation counter output on a strip chart.

Natural Gamma Radiation Logging

Small concentrations of radioactive elements exist in most shale beds. Potassium in the micas and the clay minerals produced by decomposition of micas and alkali feldspars includes small proportions of the radioactive isotope potassium-40. Trace amounts of uranium and thorium also occur in shale. These unstable elements produce measurable levels of gamma radiation. Quartz sandstones and carbonate beds have much lower concentrations of these radioactive impurities. Therefore, the principal use of natural gamma-ray logging is to distinguish shale beds and to estimate the clay content in impure sandstones and carbonates.

The scintillation counter used for natural gamma-ray logging counts the number of

light flashes that occur in the crystal during a fixed interval of time. This is the average rate recorded on the log. Because of the irregular and sporadic nature of radioactive gamma-ray emissions can vary from one moment to the next. Therefore, the instrument counting time is brief, and, second, the log can register considerable irregularity as the sonde passes through a shale bed. Over larger periods of time, however, the number of emissions becomes more regular. With the instrument counting time set at, say, five seconds, a much more uniform level of radiation would be indicated for the same bed.

The sensitivity of natural gamma-ray logging to boundaries between shale and less radioactive beds depends on the counting time and the speed of the sonde is moving. Each value on the log represents the average radiation level of the rock through which the sonde has passed during the interval of counting time. Consider the three logs in Figure 14-8. Log a was obtained with a short counting time and a fast sonde speed, and log c with a long counting time and slow sonde speed. That is, if the counting time is too short, the natural irregularity of emissions may obscure a boundary between shale and sandstone. This irregularity can be reduced by increasing the counting time, but if the sonde is moving too fast, the log will indicate a gradual change rather than a sharp change in radiation level near the boundary. This gradation can be sharpened by slowing the sonde speed, but for practical reasons, we cannot slow the sonde too slowly. Therefore, a balance must be made in choosing the counting time and the sonde speed that will yield the best log. Typically, good results can be obtained

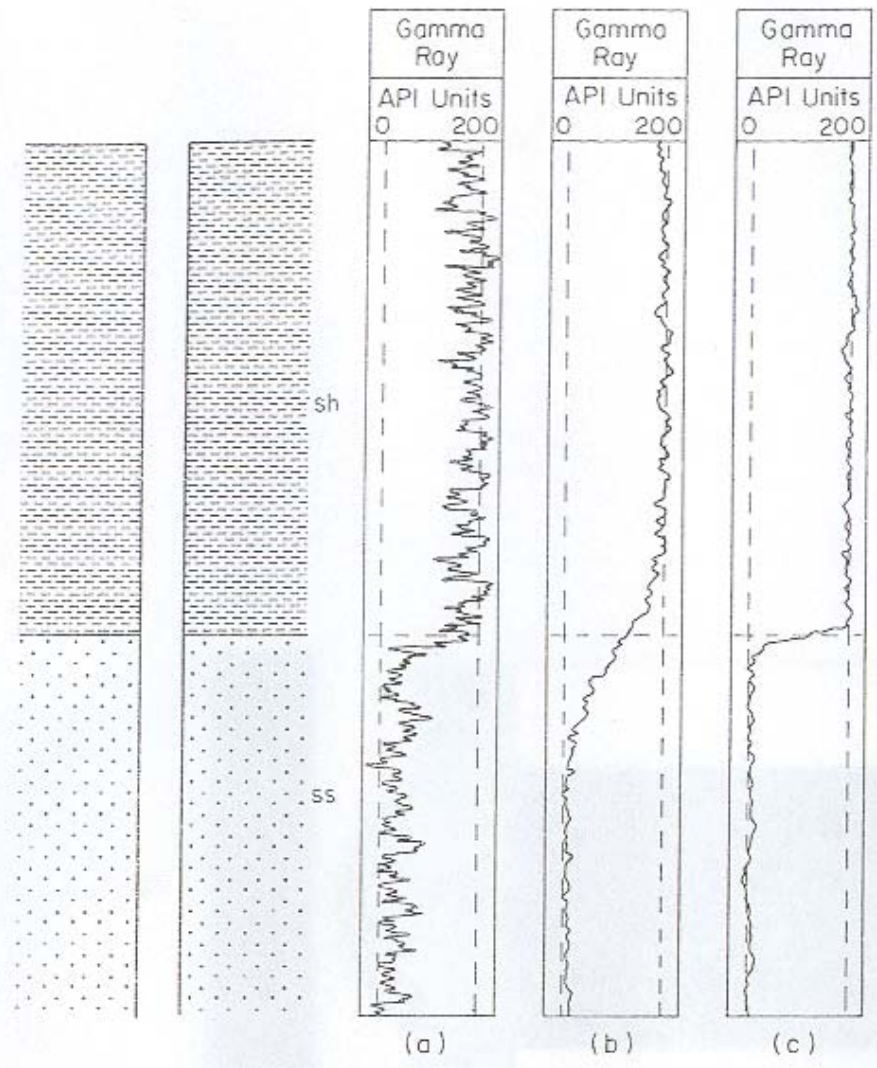


Figure 14-31
Idealized diagram showing variation of natural gamma radiation near the boundary between sandstone and shale beds obtained by (a) a short counting time and fast sonde speed, (b) a long counting time and fast sonde speed, and (c) a long counting time and slow sonde speed.

with a counting time of 2 seconds and a sonde speed of about 30 feet per minute.

An important advantage of natural gamma radiation logging is that it can be done in cased wells. Electric logging cannot be done in cased wells because most of the current flows in the highly conductive casing pipe rather than through the formation. Gamma radiation detected at the sonde comes from the formation within a few feet from the well.

Gamma-Ray Density Logging

Gamma radiation is emitted in collisions of electromagnetic energy with atoms. We can think of these photons as particles of energy. While traveling through a substance, they frequently collide with electrons. At each collision, some energy is transferred to the electron, thus reducing the energy of the photon. This process

Compton scattering. The number of collisions occurring during a fixed interval of time depends on the abundance of electrons, which is proportional to the density of the substance.

Gamma-ray density logging is the procedure for estimating formation density ρ_0 by measuring gamma radiation that has undergone Compton scattering. A source element mounted on the sonde emits gamma radiation into the formation. A scintillation counter mounted at another point on the sonde detects the portion of this gamma radiation that has been returned to the sonde by Compton scattering. This level of gamma radiation is proportional to the electron density index ρ_e of the formation. The gamma rays produced by the source have a different range of wavelengths than that of natural gamma radiation emitted within the formation. The scintillation counter output is plotted on a strip chart to obtain a log of the electron density index.

The relation between formation density ρ_0 and the electron density index ρ_e depends on the chemical elements present. The number of electrons possessed by each atom of an element is specified by the atomic number N of that element. By summing the atomic numbers of all elements in the formation, we can calculate ρ_0 ,

$$\rho_0 = \rho_e w / 2 \Sigma N \quad (14-16)$$

where w is the molecular weight of the combined constituents of the formation, and ρ_e is read from a log. The value of ρ_0 obtained in this way can be used in Equation 14-7, together with estimated values of pore fluid density and solid matrix density, to calculate formation porosity.

Good results can be obtained only if the source element and the detector are pressed firmly against the side of the well. The sonde must be equipped with a blade for cutting

through any mud cake to ensure contact with the rock surface. To maintain this contact, the sonde must move quite slowly down the well at speeds of less than 30 feet per hour. Therefore, in deep wells, gamma-ray density logging is usually restricted to zones of particular interest.

Neutron-Gamma-Ray Logging

Nonradioactive elements in a formation can be stimulated to emit gamma radiation when they are bombarded by neutrons. This process yields neutron-gamma-ray logs which provide information about porosity. The sonde contains a neutron source and a scintillation counter mounted a fixed distance from the source. The source consists of a small amount of radioactive material such as plutonium-241, which emits neutrons during its natural radioactive decay.

Neutrons emitted from the source travel through the formation, colliding with the nuclei of most elements. The nuclei of most elements in the formation, such as silicon, oxygen, and aluminum, are much more massive than a neutron. Therefore, a colliding neutron is likely to bounce away with almost no loss of kinetic energy. Of all the elements in the formation, only hydrogen possesses approximately the same mass. For this reason, upon collision, a neutron can transfer a significant portion of its kinetic energy to a hydrogen nucleus, a proton. Such collisions reduce the kinetic energy of a neutron until its kinetic energy is not enough for it to be absorbed into the nucleus of a larger nucleus. Absorption, or capture, of a neutron stimulates the emission of gamma radiation. A portion of this gamma radiation reaches the sonde and is detected by the scintillation counter.

The intensity of capture gamma radiation detected at the sonde depends on its distance from points of neutron capture. If neutrons travel a considerable distance before capture, only a small portion of the capture gamma rays manages to reach the sonde. But when the neutrons are quickly absorbed close to the well, a high level of capture gamma radiation is recorded.

The concentration of hydrogen in a formation is, by far, the most important factor affecting the distance that a neutron travels before it is captured. Where hydrogen content is high, neutron capture occurs close to the well, and a high level of capture gamma radiation is detected. The neutron-gamma-ray log, then, indicates variations in hydrogen concentration.

What influences hydrogen concentration? Hydrogen exists in molecules of water and petroleum and in crystals of hydrated minerals such as the silicate clays, micas, amphiboles, and gypsum. Therefore, in quartz sandstones and carbonate rocks, hydrogen occurs almost entirely in the pore water or petroleum. Its concentration depends on the formation porosity. In shale, however, micas and clay minerals as well as pore water contribute to the content of hydrogen.

It can be difficult to distinguish a shale bed from porous sandstone or carbonate beds by means of a neutron-gamma-ray log. These different beds may all contain the same concentration of hydrogen. Other kinds of logs, such as the natural gamma-ray log, must be used to make these lithologic distinctions. The principal use of the neutron-gamma-ray log is to detect porosity variations within sandstone beds or carbonate beds, as illustrated in Figure 14-32. We can identify the sandstone and shale beds by means of the natural gamma-ray log. Then we can look at the neutron-gamma-

ray log variation within an ironstone bed. The log in this example shows the highest hydrogen content, the highest porosity, near the top of the bed.

The neutron-gamma-ray log is used in cased or uncased wells. The log is obtained with a skid mounting the source and detector against the wall of the well. Capture gamma radiation is obtained from neutron capture at distances of 2 feet from the well. Typical logging speed is about 30 feet per minute. The counting time of the scintillation counter is at 2 seconds. The scintillation counter is constructed to detect wavelengths of capture gamma radiation, which are different from the wavelengths of natural gamma-

SONIC LOGGING

The final logging procedure we will discuss involves a small-scale seismic refraction experiment. This experiment can be conducted with a source and two receivers mounted on the sonde (Figure 14-33a). In the standard design, the receivers are placed one on each side of the source with the source three feet from the nearest receiver. Sound pulses are emitted from the source at 0.1-second intervals. Because the wave speed is faster in the formation than in the fluid filling the well, the wave refracts toward the rock at the side of the well nearest the receivers. Each pulse activates a circuit that records the difference in transit times to the two receivers. This value is the *interval transit time* T_0 . The interval transit times are plotted on a strip chart to produce a sonic log.

The procedure we have described can be run without problems. If the sonde is tilted

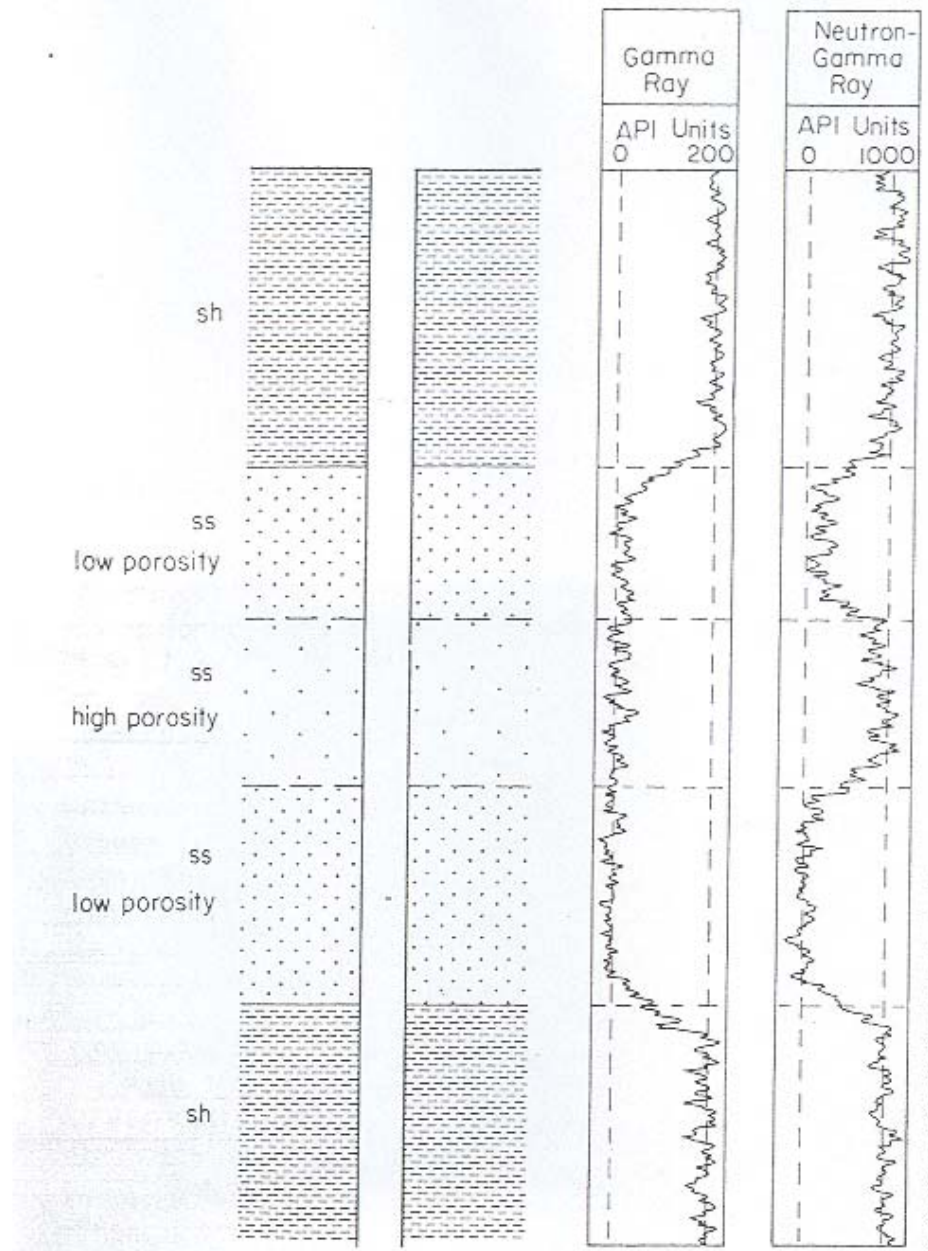


Figure 14-32

Idealized diagram showing the effect of lithology (shale and sandstone) and porosity on gamma radiation and neutron-gamma radiation logs. Gamma radiation depends on the concentration of radioactive elements in a rock unit, and neutron-gamma radiation depends principally on the proportion of water space in a rock unit.

well, or if the well diameter varies, travel paths through the fluid filling the well to the two receivers will have different lengths (Figure 14-33b). This problem is similar to that with dipping layer refraction (Figure 3-10), which

means that an apparent interval is being measured rather than the true interval T_0 in the formation. To overcome this difficulty, we can mount another source on the sonde in a position

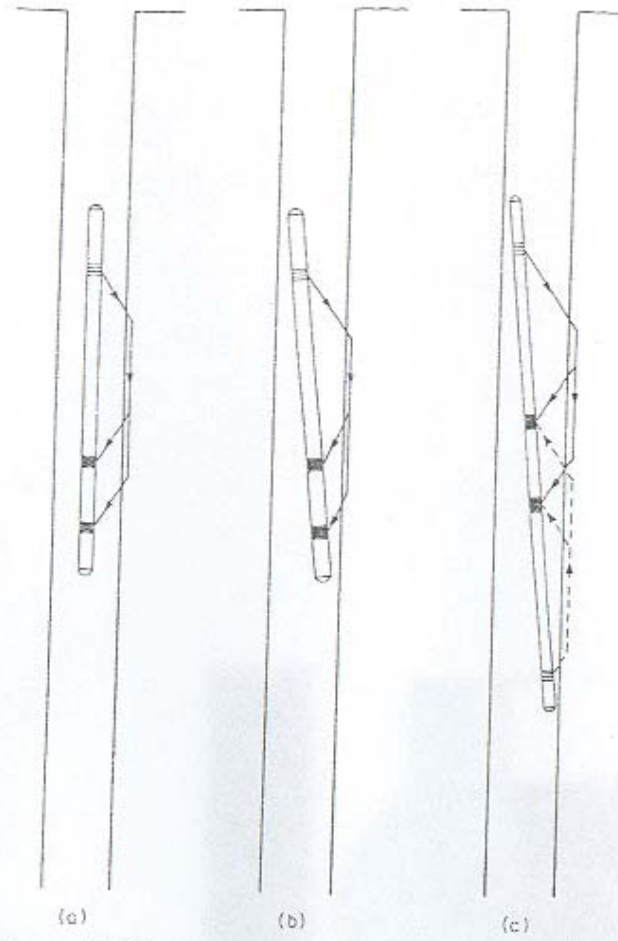


Figure 14-33
Schematic diagram of source-receiver configurations for (a) a nonborehole-compensated single-transmitter device aligned vertically and (b) tilted in the well, and (c) a two-transmitter borehole-compensated device which plots the average of the transit times measured from the two sources.

the original source (Figure 14-33c). Now we have a *borehole-compensated sonde*. Sound pulses are emitted alternately from the sources, and the apparent interval transit times from the two oppositely traveling refracted waves are averaged electronically to obtain the true

value of T_0 . This practice is similar to recording along reversed refractors in order to obtain the apparent velocity. To solve the dipping layer problem, interval transit times are recorded on a strip chart to obtain a borehole-compensated (BHC) sonic log.

The P -waves reaching the receiver are laterally refracted at the side of the well. Therefore, the sonic log tests only the interval very close to the well. Interval transit times (T_0) read from a log depend on the properties of solid matrix and fluid within the interval. These readings together with estimated interval transit times in the solid (T_m) and fluid (T_f) parts are used in Equation 14-4 to determine values of formation porosity. The estimation is based on information about lithology obtained from drill cuttings and other logs. The values given in Table 14-1 are typical for the kinds of rock common in oil and gas wells. The estimation requires some independent knowledge of the formation fluid, which might

TABLE 14-1 Sonic Transit Time and P-Wave Velocities in Different Materials

MATERIAL	TRANSIT TIME (μ s/foot)	P -WAVE VELOCITY (ft/sec)
Sandstone	51-55.5	18,000
Limestone	43.5-47.6	21,000
Dolomite	43.5	
Anhydrite	50.0	
Salt	66.7	
Shale	62.5-167	6,000
Water (pure)	218	
Water (10% NaCl)	208	
Oil	238	
Methane	626	

from electric logs. Typical values of T_w are also given in Table 14-1.

Sonic logs have proved very useful for correlation between nearby wells. Beds as thin as the spacing of the two receivers, commonly one foot, can be detected. Sonic logs are also very useful in the interpretation of seismic surveys of nearby areas. The variations in interval transit time indicate boundaries from which reflections might be expected. By summing the transit time through a continuous succession of intervals reaching to such a boundary, we can calculate the probable reflection travel time.

SUMMARY STATEMENT

Well logs are essential for discovering the nature of rock formations penetrated by a drill. The drill itself does not provide unambiguous information about these formations. Rock cuttings tell us what lithologies are present but are unclear about exactly where they occur. Even core drilling, which can be prohibitively expensive, yields incomplete information about formation fluids, and 100 percent core recovery is seldom possible. Therefore, we need an assortment of well logs for more complete evaluation of the formations.

Electric logs have proved the most useful for evaluating formation fluid properties. But the results from any individual log are distorted by the electrode configuration and by effects of invasion. Only in combination with other logs do they yield reliable information

for estimating the salinity of pore fluids, and the proportions of water and natural gas. Because both petroleum and natural gas are nonconductors, they are difficult to distinguish from each other by electric logs. Their elastic properties are very different, so that sonic logs are useful for making this distinction.

We cannot unambiguously identify different kinds of rock by any single log, such as resistivity, density, radioactivity, or transit time. A much clearer picture of the subsurface if these properties are considered together. Electric logs, gamma density logs, gamma logs, and sonic logs are used together for this purpose.

Formation porosity can be estimated independently from electric logs, a gamma log, a neutron-gamma log, and a sonic log. Nonetheless, each separate result is subject to error introduced by invasion, mud cake, and irregularity in the wellbore. To the extent that results from different logs confirm one another, they can obtain reliable values.

For more than half a century, well logging has played a central role in the discovery and development of petroleum and natural gas resources. These resources have not been so fully used for mining as they have in the search and development of other resources, and as a part of engineering and drilling operations. Today modern logging techniques are being used more extensively for these purposes.

STUDY EXERCISES

- The cross section in Figure 14-34 shows a borehole that crosses the boundary between two rock layers. The dashed line is an equipotential surface related to the current source shown in the well. From the shape of this surface, determine which resistivity value is largest and which is smallest, where R_w is the resistivity of the drilling fluid filling the well, and R_1 and R_2 are resistivities in the upper and lower layers.

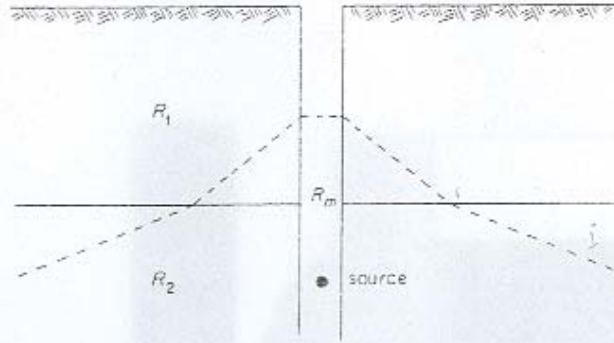


Figure 14-34
Cross section showing a borehole that penetrates two formations, a source of electric current, and an equipotential surface (dashed line).

- Describe the conditions that cause an annulus of invasion to form in the rock surrounding a borehole. Sketch a graph showing the approximate variation in resistivity with distance away from the center of the hole, assuming that the resistivity of the drilling fluid is higher than the resistivity of the natural fluid filling the pores of the formation.
- In a sandstone layer, suppose that the resistivity is 30 ohm-m, and that the resistivity of the fluid filling the pores is 6 ohm-m. What is the highest

value for porosity that you would calculate for this rock by means of the formula?

- In a layer of quartz sandstone, as the sonic transit time is 82 $\mu\text{s}/\text{foot}$. If the velocity of 20,000 feet/s as the P -wave velocity, calculate the porosity of the sandstone.
- A layer of relatively impermeable limestone, 50 feet thick, lies between two layers of sandstone, each of which is 50 feet thick. A well penetrating these layers, a log, an 18-foot, 8-inch lateral log, and a laterolog were obtained. The central electrode spacing of the laterolog sonde was 10 inches. The resistivity in the limestone is higher than in the sandstone.
 - Which log or logs indicate a high resistivity in the limestone? Explain your answer.
 - Which log will produce the most accurate value of limestone resistivity? Explain your answer.
 - Which log or logs will produce the most accurate value of the sandstone resistivity? Explain your answer.
- Suppose that a layer of sandstone is contaminated by clay mineral grains similar to those ordinarily found in shale. Both a gamma-ray log and a neutron-gamma-ray log from a well penetrating this layer show an increase in resistivity with depth through the layer. Do you think that porosity changes with depth? Do you think that contamination changes with depth? Explain your answers.

R

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