

Part 631 Geology National Engineering Handbook

Chapter 4 Engineering Classification of Rock Materials

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Preface

Chapter 4 and related chapters in the National Engineering Handbook (NEH), Part 631 replace NEH Section 8, Engineering Geology, which was last released in 1978. Additionally, contents from the current NEH, Part 631, Chapter 12, Rock Material Classification System (released June 2002), and Technical Release (TR) 78, The Characterization of Rock for Hydraulic Erodibility, are included in this new chapter as well. NEH Section 8, NEH 631.12, and TR–78 are cancelled and archived upon publication of this new chapter.

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Chapter 4

Engineering Classification of Rock Materials

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Chapter 4

Engineering Classification of Rock Materials

631.0400 Engineering properties of rock

To use rock in engineering applications, certain properties of the rock must be assessed to reasonably predict performance in the as-built condition. The properties of rock fall into two broad classes: rock material properties relating to the rock itself and rock mass properties relating to the in-place rock mass, including its discontinuities.

(a) Rock material properties

Rock material properties that are essential in assessing hydraulic erodibility of rock include rock type, color, particle size, texture, hardness, and strength. Seismic velocity, weathering, and secondary cavities are properties related to both the rock material and mass. Rock material properties can be described in the field using qualitative methods and simple classification tests, or, if necessary, in the laboratory using standardized tests. The results are applicable to hand specimens and representative samples of rock material.

(b) Rock mass properties

Rock mass properties are comprised of features generally observed, measured, and documented in the field for in-place rock.

Discontinuities are distinct breaks or interruptions in the integrity of a rock mass that convert a rock mass into a discontinuous assemblage of blocks, plates, or irregular discrete rock particles. A discrete rock particle is an intact fragment of rock material whose shape and size are initially defined by the discontinuities that form its margins. Discrete rock particles may occur in their place of origin, such as fractured, broken, or jointed in situ rock, where particles retain their original form and size or moved from their place of origin with subsequent modification of size and shape occurring in the transport process. Naturally occurring examples include stream cobbles, talus, and glacial boulders; or they can be manufactured, as in the case of quarried rock. The properties of a rock mass are significantly different from the properties of samples of the same rock mass. The strength and mechanical behavior of the rock mass are commonly dominated more by the nature of its mass properties than by its material properties. A rock mass comprised of even the strongest intact rock material is greatly weakened by the occurrence of closely spaced discontinuities. Material properties, however, tend to control the strength of the rock mass if discontinuities are widely spaced or if the intact rock material is inherently weak or altered. Discontinuities within a rock mass, therefore, reduce its strength and stability and reduce the energy required to excavate or erode it.

It is important to recognize that many rock properties interact under performance conditions. A performance assessment for any given engineering application must be viewed in the broader context of these interactions.

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631.0401 Rock material properties

Rock material properties are measurable or describable lithologic properties of rock material that can be evaluated in hand specimens or tested in the laboratory. Rock material properties are related to the physical properties of the rock-forming minerals and the type of mineral bonding. Properties are determined from hand specimens, core sections, drill cuttings, outcroppings, and disturbed samples using qualitative procedures, simple classification tests, or laboratory tests. The results are applicable to hand specimens and representative samples of intact rock material. They do not account for the influence of discontinuities or boundary conditions of the rock. Typical classification elements include:

- principal rock type
- mineralogy (estimate percentage of principal and accessory minerals; note type of cement and presence of alterable minerals)
- primary porosity (free draining or not)
- hardness and unconfined compressive strength categories unit weight (dry)
- unit weight (dry)
- color
- discrete rock particle size (use D₅₀ or cube root of the product of its three dimensions)

(a) Rock unit identification

The rock unit is the basic mapping unit for the rock material field classification (RMFC) system. It is defined as a body of rock that is identified in the field and mapped according to measurable or otherwise describable physical properties or features at a scale useful for project analysis.

A rock unit is consistent in its mineralogical composition, geologic structure, and hydraulic properties. The boundaries are delineated by measurable or otherwise describable physical properties or features. It is traced in the field by surface and subsurface mapping techniques. Because the mapping criteria are performancebased engineering characteristics, rock units need not conform to formally recognized stratigraphic rock formations.

The term "rock unit" is similar to lithosome in that the body of rock has consistent, mappable characteristics, but differs in that lithosomes are formed under uniform physicochemical conditions.

Identify each rock unit at the site by either its proper formation name (e.g., St. Peters Sandstone) or by an alphanumeric designation (e.g., Rock Unit L–6), whichever is the most useful. If a formation has multiple beds or units of differing engineering behavior, the alphanumeric designation is preferable.

Describe the location of each rock unit by station, elevation, and position in the stratigraphic section. Indicate its location and extent on a geologic evaluation map of the site.

(b) Rock type

Rock type is a simplified geologic classification of rock based on its genetic category, structure, composition, and grain size. Table 4–1 (after GSL 1977) is a rock type classification that uses common rock type names that can be assigned in the field without need for detailed lab tests or thin sections.

The equipment needed to identify rock type includes a geologist's hammer with pick end, 10x hand lens, hydrochloric acid (10 N solution: 1 part acid to 3 parts distilled water), pocket knife, 15-centimeter (6-in) scale, and AGI Data Sheets.

Using standard field identification procedures and table 4–1 as a guide, classify all identified rock units and record the rock type name and two-digit code number for each unit on a Rock Description Data Sheet (app. 4D).

Use more detailed mineralogical and rock descriptors only if they are needed for correlation purposes or to describe engineering properties of the rock. Use common terminology such as "schist," instead of technically correct, but jargon-rich terms such as "albiteepidote-amphibolite-schist." If more detailed guidance is required, refer to the AGI Data Sheets.

Table 4–1 Rock type classification (Geological Society of London 1977)

| Gene gro | | Detrital sedimentary | | | Chemical organic | Metam | orphic | Pyroclastic | | lger | neous | | | | | |
|--------------------------|-----------------------------|----------------------|---------------------------------|--|---------------------|------------------------|------------------------------------|---|-------------------------------|--------------------------------------|--|-----------------------------------|-----------------------------|-----------------------------|----------------------------|------------------|
| Usual st | ructure | | | Bedded | | | | Bedded | Foliated | Massive | Bedded | | Massive | | | |
| Compo | sition | | | Grains of rock, quartz, feldspar, At least 50% grains are of | | | | are of | Salts, carbonates, | Quartz, feldspars, micas, dark | Quartz, feldspars, micas, dark | At least 50% of grains are of | | feldspars, dark minerals | Feldspar; dark minerals | Dark minerals |
| | | | | | са | Indoi | nate | silica, carbonaceous | minerals | minerals, carbonates | igneous rock | Acid | Intermediate | Basic | Ultrabasic | |
| Very | | | Gra | ains are of rock fragi | ments | | | CLINKER (31) | | | Rounded grains: | | | | | |
| coarse- grained | 75 | Rudaceous | Rounded grains: CONGOMER | | | | CALCIRUDITE | SALINE ROCKS Halite (32) | MIGMATITE (42) GNEISS (43) | GLOMERATE (51) | AGGLOMERATE (61) Angular grains: | | PEGMATITE (| /1) | | |
| Coarse- grained | (3") | | Angular grains: BRECCIA (12 |) | | sd (21) | (23) | Anhydrite (33) Gypsum (34) | | MARBLE (52) GRANULITE (53) | VOLČANIC BRECCIA (62) | GRANITE (72) | GRANODIORITE | GABBRO (91) | PYROX- ENITE | |
| Medium- grained | 4.75 (ou ever | Arenaceous | Grains are mainly SANDSTONE | mineral fragments (13) | | (undifferentiated (21) | CALCARENTIE | CALCAREOUS ROCKS | SCHIST (44) | QUARTZITE (54) | TUFF (63) | SYENITE (73) | (82) ANORTHOSITE (83) | DIABASE (92) | (01) PERIDO- | |
| Fine- grained | (4) 0.074 (200) (200) | Arena | ARKOSE (14) GRAYWACKE | (Argillaceous ss) (15) | | | (27) | | Amphib | iolite (45) | | APLITE | MONZONITE | (02) | TITE (02) | |
| Very | t grain size | or Lutaceous | MUDSTONE (16) SHALE: fissile | SILTSTONE>50% fine-grained particles (18) | DNE (22) | LIMESTONE | CALCISILTITE (25) CHALK (26) | LIMESTONE (35) | PHYLLITE (46) | HORNFELS (55) | Fine-grained TUFF (64) | (74) RHYOLITE or FELSITE | (84) Dacite (85) | BASALT (93) | DUNITE (03) | |
| fine- grained | Predominant grain | Argillaceous c | mudstone (17) | CLAYSTONE>50% very fine grained particles (19) | MARLSTONE | | CHALK (26) CALCILUTITE (27) | DOLOMITE (36) | Mylon SLATE (48) | ite (47) | Very fine-grained TUFF (65) | (75) | ANDESITE (86) | () | BASALT (04) | |
| 0 | ľ | | | | | | | SILICEOUS ROCKS Chert (37) Flint (38) | Ultramyl | onite (49) | Welded TUFF (66) | VOI | LCANIC GLAS | SES | | |
| Glassy amor- phous | | | | | | | | CARBONACEOUS ROCKS | | | | OBSIDIAN (76) | PITCHSTONE (87) | TACHYLYTE (87) | | |
| | | | | | | | | LIGNITE/COAL (39) | | | PUMICE (67) | | | | | |

Engineering significance of rock type

Geologic names and geologic classifications may not always relate directly to engineering properties of rock, but are useful for identification and correlation purposes.

Rock type may also indicate what processes acted on the rock during and after its formation. These facts may be valuable in predicting the size, shape, extent, and location of beds, lenses, and stringers that may be discontinuities. Rock type can indicate mineralogical and textural characteristics, which may provide insight into the physical and chemical interaction between the grains. Some near-surface or exposed granites, for example, form horizontal stress relief fractures with reduced confining pressures as erosion removes overlying materials.

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(c) Hardness

Hardness is the subjective description of the resistance of an earth material to permanent deformation, particularly by indentation (impact) or abrasion (scratching) (ASTM D653).

Rock hardness is not the same as mineral hardness. The Mohs scale is a qualitative scale for a set of empirical tests used to differentiate minerals in hand specimens by scratching. The scale has no useful application in describing most rock material for engineering purposes because most rock types are aggregates of more than one mineral.

For each igneous or crystalline metamorphic rock unit, record the rock texture using the descriptors in table 4–2 as a guide. Refer to the AGI Data Sheets if more detailed descriptors are needed.

Hardness is simply a qualitative expression of earth material strength; the hardness categories form a scale of ranges in strength values obtained from the laboratory test for strength (section 631.0401(d)).

Field tests for rock hardness are given in table 4–3 for the evaluation of excavation characteristics and hydraulic erodibility of rock and for classifying rock for excavated auxiliary spillways. The equipment needed to perform the field tests for hardness includes a pocket knife, a geologist's hammer with pick end, and a common 20d steel nail. For each rock unit, determine the hardness category by using the field tests given in table 4–3.

Engineering significance of hardness of rock

The hardness of rock material is a function of the individual rock type, but may be modified (weakened) by chemical or physical weathering (section 631.0405(b)).

Hardness categories provide reasonable estimates of rock material strength for classifying earth material as rock in excavated auxiliary spillways. The designer must carefully consider the characteristics of the rock mass before reaching a decision on alignment and location of a rock spillway.

| Table 1-2 | texture descriptors for igneous and crystallite inclantorphic focks |
|---------------|---|
| | |
| Textural term | Description |
| Aphanitic | Crystalline components cannot be seen with the naked eye (syn.: cryptocrystalline, or microcrystalline) |
| Crystalline | Composed entirely of contiguous or interlocking crystals |
| Glassy | Certain extrusive igneous rocks that cooled rapidly, without distinct crystallization. (syn.: vitreous) |
| Pegmatitic | Very coarse-grained, crystals >10 mm in diameter |
| Porphyritic | Large crystals set in a fine-grained ground mass that may be glassy or crystalline |

Texture descriptors for igneous and crystalline metamorphic rocks

Table 4-2

Table 4–3

Hardness and unconfined compressive strength of rock materials

| Hardness category | Typical range in unconfined compressive strength (MPa) | Strength value selected (MPa) | Field test on sample | Field test on outcrop |
|---|--|--|--|---|
| Soil* | < 0.60 | | Use USCS classification | S |
| Very soft rock or hard, soil- like material | 0.60–1.25 | | Scratched with fingernail. Slight indentation by light blow of point of geologic pick. Requires power tools for excavation. Peels with pocket knife. | |
| Soft rock | 1.25–5.0 | | Permits denting by moderate pressure of the fingers. Handheld specimen crumbles under firm blows with point of geologic pick. | Easily deformable with finger pressure. |
| Moderately soft rock | 5.0–12.5 | | Shallow indentations (1–3 mm) by firm blows with point of geologic pick. Peels with difficulty with pocket knife. Resists denting by the fingers, but can be abraded and pierced to a shallow depth by a pencil point. Crumbles by rubbing with fingers. | Crumbles by rubbing with fingers. |
| Moderately hard rock | 12.5–50 | | Cannot be scraped or peeled with pocket knife. In- tact handheld specimen breaks with single blow of geologic hammer. Can be distinctly scratched with 20d common steel nail. Resists a pencil point, but can be scratched and cut with a knife blade. | Unfractured outcrop crum- bles under light hammer blows. |
| Hard rock | 50–100 | | Handheld specimen requires more than one hammer blow to break it. Can be faintly scratched with 20d common steel nail. Resistant to abrasion or cutting by a knife blade, but can be easily dented or broken by light blows of a hammer. | Outcrop withstands a few firm blows before breaking. |
| Very hard rock | 100–250 | | Specimen breaks only by repeated, heavy blows with geologic hammer. Cannot be scratched with 20d common steel nail. | Outcrop withstands a few heavy ringing hammer blows but will yield large frag- ments. |
| Extremely hard rock | > 250 | | Specimen can only be chipped, not broken by re- peated, heavy blows of geologic hammer. | Outcrop resists heavy ringing hammer blows and yields, with difficulty, only dust and small fragments. |

Method used to determine consistency or hardness (check one):

Field assessment: _____ Uniaxial lab test: _____ Other: _____ Rebound hammer (ASTM D5873): _

* See NEH631.03 for consistency and density of soil materials. For very stiff soil, SPT N values = 15 to 30. For very soft rock or hard, soil-like material, SPT N values exceed 30 blows per foot.

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(d) Strength

Strength is the ability of a material to resist deformation induced by external forces. The strength of a material is the amount of applied stress at failure (ASTM D653). The laboratory uniaxial (unconfined) compressive strength is the standard strength parameter of intact rock material.

If strength is to be determined by correlating with hardness, use table 4–3 as a guide. Record results and the test method used on the Rock Mass Description Data Sheets for each identified rock unit.

The strength of rock is influenced by the mineralogical composition, shape of grains, texture, crystallinity, stratification, lamination, modification by heat or pressure, and other factors. Secondary processes of cementation and weathering strongly influence rock strength.

(1) Cementation

Cementation of rock is an important secondary process influencing its strength. Principle cementing materials are silica, calcium carbonate, iron oxide, and clays. Most durable are bonds of silica, whereas clay bonds are weakest, particularly when saturated. It is important, therefore, to note the nature of cementing material when describing rock. A summary of description of weathering terminology is shown in table 4–4, and terminology to describe cementation conditions of rock in table 4–5.

(2) Dry density

Information provided by the accessory minerals in the name of a rock can provide clues to properties that have engineering significance. For example, a mica schist might indicate potentially weak rock because the sheet silicates (the micas and chlorite) impart low shear strength to the rock mass. See table 4–6.

Engineering significance of rock material strength

Rock material strength and rock material hardness are used in classifying earth material as rock in earth spillways. Rock material strength can be reasonably estimated from the rock hardness scale (table 4–3) without conducting a laboratory strength test (NEH628.52).

Rock mass strength is largely affected by the discontinuities within the rock mass. The field strength of the in situ rock mass will always be less than the laboratory strength of an intact sample of the mass.

| Term | Weathering description | Grade |
|----------------------|---|-------|
| Fresh | No visible sign of weathering: perhaps slight discoloration on major discontinuity sur- faces. | Ι |
| Slightly weathered | Discoloration indicates weathering and discontinuity surfaces. May be discolored and somewhat weakened by weathering. | II |
| Moderately weathered | Less than half is decomposed or disintegrated to a soil material. Fresh or discolored rock is present either as a continuous framework or as corestones. | III |
| Highly weathered | More than half of the rock material is decomposed and/or disintegrated to a soil. Fresh or discolored rock is present either as a continuous framework or as corestones. | IV |
| Completely weathered | All rock material is decomposed and/or disintegrated to soil. The original mass structure is still largely intact | V |
| Residual soil | All rock material is converted to soil material. The mass structure and material fabric are destroyed. There is a large change in volume, but the soil has not been significantly transported | VI |

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| Table 4–5 | Cementation chart | | |
|-----------|--|--|--|
| | Cementation | | |
| Weak | Crumbles or breaks with handling or little finger pressure | | |
| Moderate | Crumbles or breaks with considerable finger pressure | | |
| Strong | Will not crumble or break with finger pres- sure | | |

| lb/ft ³ | Mg/m ³ | Check one |
|--------------------|-------------------|-----------|
| < 60 | < 0.96 | |
| 60-70 | 0.96-1.12 | |
| 70-80 | 1.12-1.28 | |
| 80-90 | 1.28-1.44 | |
| 90-100 | 1.44-1.60 | |
| 100-110 | 1.60-1.76 | |
| 110-120 | 1.76-1.92 | |
| 120-130 | 1.92-2.08 | |
| 130-140 | 2.08-2.24 | |
| 140-150 | 2.24-2.40 | |
| 150-160 | 2.40 - 2.56 | |
| > 160 | > 2.56 | |

(e) Color

Rock color is an attribute of visual perception that can be described by color names (ASTM 1986).

In wide use are the Munsell Soil Color Charts and Rock Color Chart (Munsell 2009a and 2009b). For rapid field logging purposes, e.g., reconnaissance investigations, table 4–7 can be used as an alternative.

Color is difficult to describe because a perceived color greatly depends not only on the spectral power distribution of the color stimulus, but also on the size, shape, structure, and envelop of the stimulus area. For example, a given color will appear differently when seen next to other colors; grey appears bluish when seen next to orange or brown earth colors. Perceived color also depends on the observer's experience with similar observations; so a color may often be named differently by different persons. When using table 4–7, a color from column 3 can be supplemented, if needed, with a term from column 2, column 1, or both. Terms such as "banded," "mottled," streaked," "speckled," and "stained" may be used as modifiers.

Record the color of each rock unit in both its wet and dry states. Indicate whether the sample is fresh or in an altered condition since these conditions can affect color.

| Color | | | | | |
|-------------------|--|--|---------|--|--|
| | | | Dry | | |
| | | | Wet | | |
| | | | Fresh | | |
| | | | Altered | | |
| 1st descriptor | 2nd descriptor | 3rd descriptor | - | | |
| light dark | yellowish buff orangish brownish pinkish reddish bluish purplish range olive greenish greyish | white yellow buff orange brown pink red blue green purple olive grey black | | | |

Engineering significance of rock color

Color can be an indication of the weathered state of the rock. Discoloration of rocks to shades of red, yellow, orange, and brown indicates leaching of iron, Fe^{+2} , from unstable minerals and its fixation as Fe^{+3} in oxide pigments. The degree of discoloration may therefore provide an indication of the degree of stability of minerals in rocks.

Color changes may indicate changes in the rock's mineral assemblage, texture, organic carbon content (shales), or other properties.

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(f) Particle size and texture

Particle size refers to the size of the particles that make up a sedimentary or pyroclastic rock. Texture refers to the crystallinity and granularity of igneous and crystalline metamorphic rocks.

The particle sizes used in the description of rocks for engineering purposes should be consistent with those used for soils (ASTM D422, D2488, and D653). The format of table 4–8 is modified after USBR (1989) and GSL (1977). The lithified product is the name for the equivalent sedimentary or pyroclastic particles after lithification of the material. A hand lens is usually sufficient to identify particle size and rock texture.

Use the rock particle size descriptors given in table 4–8 for sedimentary and pyroclastic rock types. Record the particle size or lithified product of each rock unit and the descriptive system used.

The strength of rock masses is greatly influenced by the presence of bedding, cleavage, schistosity, and similar features, as well as by the presence of joints and fractures. The spacing, pattern, attitude, and other characteristics of these features are important in evaluating strength of a rock mass. The presence of bedding, cleavage, schistosity, joints, fractures, and faults can affect the rock strength by increasing or decreasing the fracturing density.

Engineering significance of particle size

Bonding strength between particles that constitute rock material may determine particle size and texture with mechanical or chemical weathering of the rock.

Chemical weathering not only influences strength of rocks, but also the characteristics of derived soil materials. Some rocks break down into equidimensional grains, whereas others break down into platy grains such as clay minerals. Rocks that contain minerals of variable resistance to chemical weathering may become highly permeable through the alteration and removal of easily weathered materials, leaving the more resistant materials. Rainfall and runoff that percolate through soil and fractured limestone and other carbonate rocks may develop solution channels and collapse features, or karst terrain.

Table 4–8 Particle-size descriptors for sedimentary and pyroclastic rocks

| Descriptive term (rocks) | inches | U.S. standard sieve no. | mm | Unified soil classification system ^{1/} | Sedimentary particle or fragment | Sedimentary lithified product | Volcanic fragment | Volcanic lithified product |
|-----------------------------|------------------------------|----------------------------|---|--|--|--|----------------------|---|
| very coarse-grained | 12 | | 4026- 2048- 1024- 512- 300- | boulder | boulder | boulder conglomerate | block | volcanic breccias (angular grains) |
| | 10 6 3 | | 256— 128— 75— | cobble | cobble | cobble conglomerate | bomb | agglutinate (round grains) |
| | 1 | | 64 - 75 - 25.4 - 75 | coarse gravel | | | splatter | agglutinate |
| coarse-grained | 0.75 0.5 0.375 0.25 | 4 | $ \begin{array}{r} 19 - \\ 16 - \\ 12.7 - \\ 9.5 - \\ 8 - \\ 6.35 - \\ 4.76 - \end{array} $ | fine gravel | pebble | cobble conglomerate | lappilus | lapillistone tuff |
| | | | 4— | coarse sand | granule | granule conglom | | |
| medium-grained | | | 2 | medium sand | course sand | sandstone (v. coarse, | coarse ash | coarse tuff |
| | | | 0.25 — 0.125 — 0.074 — | fine sand | medium sand fine sand | coarse, medium, fine or very fine) | | |
| fine-grained | | | 0.0625 — 0.05 — 0.031 — 0.0156 — 0.0078 — | silt or clay | silt | sitlstone or silty shale | fine ash | fine tuff |
| very fine-grained | | | 0.005 - 0.0039 - 0.0039 | | clay | claystone clay shale | | |

1/ Unified Soil Classification System, ASTM D2487

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631.0402 Rock mass properties: general

(a) Classification elements

Rock mass properties are measurable or describable lithologic properties, characteristics, or features of the rock mass that are evaluated on a macroscopic scale in the field. They include fractures, joints, and faults, as well as abrupt changes in lithology due to erosion or deposition. Rock mass properties are too large or extensive to be observed directly at a single outcrop and are difficult or impossible to sample for laboratory analysis.

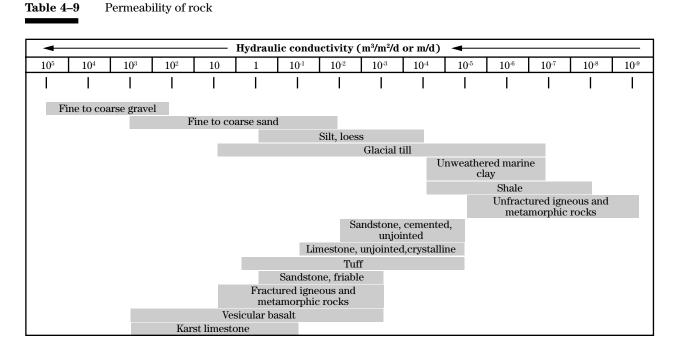
The properties of a rock mass are often significantly different from the properties of intact rock samples of the same rock mass. The mechanical behavior and strength of a rock mass are commonly dominated more by mass properties than by material properties. For example, a rock mass composed of the strongest intact rock material is weakened in proportion to the number of discontinuities in a given volume. Material properties, on the other hand, dominate the strength of a rock mass where discontinuities are widely spaced or nonexistent. Discontinuities lower the strength and stability of a rock mass and reduce the amount of energy required to excavate, erode, remove, or blast the rock mass.

(b) Permeability

Foundations, abutments, and reservoir basins that are highly fractured and contain solution channels, or are the products of differential weathering, may be highly permeable. A low porosity rock mass may be highly permeable due to fractures and joints. Jointing is not restricted to any particular type of rock, but certain types of rocks may locally exhibit larger or more closely spaced joints. Surficial joints and cracks may be termed lineaments.

Relative permeability ratings for various rock materials are shown in table 4–9.

Differential weathering may be found in many types of igneous and metamorphic rocks and certain sedimentary rocks. Differential weathering of cherty



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limestones, for example, may result in highly permeable rock foundations. It is important that the rate of permeability and the depth and direction of water movement be determined as closely as possible to determine requirements for foundation treatment. Field investigation may require angular test borings, pressure testing, use of dyes or other tracer compounds, or other methods to properly determine permeability of rock.

(c) Consolidation

The bearing strength of rock is normally adequate to support dams and other structures designed by the NRCS. However, consolidation may be a problem in certain types of rock such as weakly cemented shales and siltstones, and rocks that have been altered to clay minerals. In each instance, samples of questionable materials must be obtained for laboratory analysis, following the same procedures used for soil materials. Caverns or mines may present a problem of bearing or stability, depending on the size and location of openings. Their locations must be mapped and evaluated for site feasibility, design, and construction.

(d) Rock texture

Texture is defined as the geometrical aspects of the component particles of a rock, including size, shape, and spatial arrangement. Texture is also applied to unconsolidated materials as an alternate description of particle gradation. Texture is important for field identification purposes and for predicting behavior of rock under load. Although specific geologic terms such as "phaneritic" and "aphanitic" imply specific descriptions of igneous rock, simpler terms such as "coarse-grained" and "fine-grained" are more useful. Descriptions of mineral constituents, degree and type of cementation, conditions of weathering, fracture system, and other properties influence engineering properties. These descriptors offer more engineering value than merely the type of rock. Standard symbols are available in the Federal Geographic Data Committee Digital Cartographic Standard for Geologic Map Symbolization (FGDC 2006) (http://ngmdb.usgs.gov/ fgdc gds/geolsymstd/download.php).

(e) Shearing resistance

Problems related to shear may result from poorly cemented shales and siltstones or highly weathered rock of low shear strength. Materials that dip in an adverse direction and are subject to saturation or unloading of toe supports by excavation are of particular concern. This includes strata dipping downstream in foundations or strata dipping toward the centerline (parallel to the slope of the abutment) of proposed auxiliary spillway excavations. Rock strata of low shear strength must be thoroughly delineated and evaluated for design and construction.

(f) Rock structure

The structure of rocks includes holes, cavities, joints, bedding planes, fractures, cleavage, schistosity, lenses, and similar features. Rock structure is an important factor affecting the amount and direction of groundwater flow, as well as actual sliding or slipping of any embankment under investigation.

The term "structure," as applied to the engineering geology of a site, refers to all of the geologic structures either at the site or in a location that could affect the site. These features include faults, folds, joints, rock cleavage, and discontinuities and unconformities. Structure has an important influence on the geologic conditions of a site and the ultimate stability and safety of an engineered structure. Problems of leakage, sliding of embankments, uplift pressure in foundations, and differential settlement are often traced back to inadequate delineation and consideration of the geologic structure at the site.

(g) Attitude

Attitude is the orientation of strata, faults, fractures, and other features relative to a horizontal plane. Attitude is usually expressed in terms of measured dip and strike. In more complex geologic structures, such as plunging anticlines, special conditions may require more elaborate descriptions including pitch and plunge, as well as dip and strike.

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(h) Discontinuities

The term "discontinuity" applies to any distinct break or interruption in the integrity of a rock mass. Discontinuities are classified as either stratigraphic or structural, according to their mode of formation.

(1) Stratigraphic discontinuities

Stratigraphic discontinuities can be either depositional or erosional. They represent a significant interruption of the orderly sequence of deposition, most frequently marked by a considerable time interval of erosion or nondeposition. The bedding planes above and below the disconformity are usually parallel. These features can be found in all stratified sedimentary rocks, most volcanic flows, and some low-grade metamorphic rocks. Zones of weathering or alteration may also be considered discontinuities.

(2) Structural discontinuities

Structural discontinuities develop after the initial formation of the rock mass as a result of external processes acting on it. These features are produced by the mechanical deformation or displacement of rock by natural stresses within the Earth's crust. They include fractures of all types, planes or zones of weakness, faults, and shear zones, most of which have little to no tensile strength. The deformation of rock falls into three broad categories: elastic, plastic, and fracture deformation.

Elastic deformation is deformation from which the rock mass instantaneously recovers its original shape on removal of the external forces acting on it. The passage of earthquake waves or tidal stresses may cause elastic deformation. Since no permanent structural discontinuities are produced by elastic deformation, this chapter addresses discontinuities associated only with plastic and fracture deformation.

Plastic deformation exceeds the strain limit for elastic deformation and results in a permanent change in shape of the rock mass. Folds, foliations (such as schistosity and gneissosity), and other linear and planar structures result. The orientation of such features is related to flowage and grain rotation accompanying compression and shearing forces, which ultimately lead to metamorphism. Fracture deformation results in rupture of the rock mass. Rupture produces discontinuities such as faults, joints, and cleavage. Fractures focus the influence of weathering processes along the fracture surfaces that further weaken the rock mass over time. Caves and solution features are examples of chemical weathering that has progressed along joint systems in karst terrain (see section 631.0405(b)).

Table 4–11

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631.0403 Rock mass properties: stratigraphic discontinuities

Using all available outcrop and subsurface data, prepare geologic maps, cross sections, fence diagrams, or sketches, as appropriate, illustrating all significant stratigraphic discontinuities. Table 4–10 shows types of discontinuities. Discontinuities are to be recorded on the Discontinuity Survey Data Sheets (app. C). Map and identify each discontinuity. If the beds are parallel, record as a stratigraphic discontinuity. If the beds are discordant, the discontinuity should be recorded as an unconformity.

When describing a lithosome, use the descriptors in table 4–11 as a guide.

Descriptors for shape of lithosome

| Discontinuity category | | Code | |
|------------------------|------------------------|------|--|
| tratigraphic | | | |
| Lithosome: | Blanket | 1 | |
| | Tongue | 2 | |
| Shoestring | | 3 | |
| Lens | | 4 | |
| Slump feature | | 5 | |
| Unconformity | | 6 | |
| Structural | | | |
| Plastic deforma | tion: Folded rock | 7 | |
| | Foliation: schistosity | 8 | |
| | gneissosity | 9 | |
| | Banded rock | 10 | |
| Fracture deform | nation: Random | 11 | |
| Systematic joint | t set | 12 | |
| Bedding plane p | parting | | |
| | uniformly bedded | 13 | |
| | cross-bedded | 14 | |
| | rhythmic bedding | 15 | |
| | interfingered | 16 | |
| | graded bedding | 17 | |
| | current bedding | 18 | |
| Sheeting joint | | 19 | |
| | Slaty cleavage | 20 | |
| | Fault | 21 | |
| | Other (put in notes) | 22 | |

| Feature | Description |
|------------------|---|
| Blanket | A sheet-like, tabular body with one dimen- sion considerably thinner or shorter than the other two dimensions. Syn.: seam. |
| Tongue | A prism or tongue-shape body with the shortest dimension thinning in one direc- tion. Syn.: pinch-out; wedge. |
| Shoestring | One dimension is considerably larger than the other two; the term "columnar" is ap- propriate if the long dimension is vertical. Syn.: stringer. |
| Lens | A body with tapering edges. |
| Slump feature | A post-depositional slump, fold, or buckle produced by downslope movement of somewhat more competent layers which maintain their continuity and are not pulled apart or disrupted. Common in the thin- bedded, sand/shale sequences. |

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(a) Sedimentary rocks

Because stratified sedimentary rock is so common throughout the United States, the identification of stratigraphic discontinuities in detailed engineering geological mapping is essential for a thorough geologic investigation, particularly for auxiliary spillways designed by the NRCS. The aspect and appearance of sedimentary rock facies provide clues about the origin of the rock unit. The conditions of origin include the energy environment of deposition, the provenance and availability of sediments, as well as the physical, chemical, climatological, and other environmental characteristics that prevailed during deposition and lithification. These factors collectively determine the size, shape, continuity, and vertical and lateral extent of the rock unit or lithosome.

Depositional environments for sedimentary rocks have been classified by Pettijohn (1975) as alluvial, shore zone, marine, inland basin, and glacial. Each depositional environment uniquely determines the development of stratigraphic discontinuities and bed correlations with the rock unit.

(b) Igneous rocks

Igneous dikes and sills can be considered a type of lithosome with engineering significance. These igneous bodies interrupt the continuity of the country (host) rock, resulting in the juxtaposition of materials that may have widely different engineering properties. This can affect the strength, erodibility, and excavatability of a rock mass. Dikes and sills can erode differentially, especially as portions of flow in an auxiliary spillway are directed initially in the direction of the strike of the sill/dike. Then, as the base level lowers, continued flow and its associated erosion will cause the headcut to proceed in the direction of dip.

(c) Lithosomes

A lithosome is a rock unit of essentially uniform or uniformly heterogeneous lithologic character, having intertonguing relationships in all directions with adjacent masses of different lithologic character. Features that characterize a lithosome include the size, shape, and lateral extent of a rock unit that formed under uniform physicochemical conditions. In addition to sedimentary lithosomes, discontinuities may be related to contact metamorphism. High temperature magma may penetrate sedimentary rocks (or zones of weakness in other rock types), extrude onto the Earth's surface, or form an intrusive body at depth. Heat can metamorphose the mineralogical and textural makeup of the adjacent host rock, creating a "baked" contact zone composed of hornfels. Hornfels is a dense, hardened, flinty, fine-grained material, sometimes with one or more minerals prominent as larger crystals. The width of the contact zone varies according to the size of the intrusion—from a featheredge around thin basaltic dikes and sills, to several kilometers in the case of large, granitic igneous plutons.

(d) Unconformities

An unconformity is the surface separating two rock units that are not in stratigraphic sequence, representing a substantial break in geologic time. In general, the younger strata do not "conform" to the strike and dip of the underlying, older rocks, implying geologic uplift and erosion. The soil-rock interface is an example of a common unconformity. The engineering geologist is primarily concerned where earth materials of widely different engineering properties are juxtaposed.

Detailed mapping of the location, size, shape, continuity, orientation, and lateral extent of lithosomes and unconformities is essential for prediction of the locations of potential knickpoints, overfalls, and scour holes. This is particularly important in exit channels that discharge onto steep hillslopes. The designer needs to know the location and erodibility characteristics of identified stratigraphic discontinuities.

Engineering significance of stratigraphic discontinuities

Engineering significance of juxtaposition of geologic materials with widely different mechanical behavior and erodibility can result in abrupt lateral or vertical changes in composition, texture, or hardness associated with discontinuities or variations in sedimentary facies. For example, interfingered thin seams and lenses of inherently weak materials, such as bentonite or other expansive clay shales, calcite, gypsum, or organic shales in sedimentary rock masses, can significantly increase the hydraulic erodibility of the rock mass.

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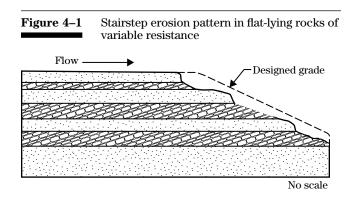
Detailed mapping should include the location of the discontinuity by stationing and elevation. The orientation of the discontinuity should be measured and recorded as well, as both an azimuth from true north and also as an azimuth relative to direction of spillway flow.

Many spillway exit channels are designed with the outlets discharging onto significantly steeper, natural hillslopes where turbulence can form a headcut, usually in the form of a waterfall or scour hole. The headcut formation represents a transition from a condition of surface attack to an overfall condition. In flat-lying, alternating sequences of dissimilar rock types, such as sandstones and shales in beds of roughly equal thicknesses, erosion produces a "stairstep" pattern that results in a comparatively gradual dissipation of flow energy down the hillslope (fig. 4–1).

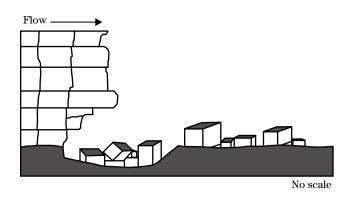
Overfall conditions can develop when resistant units are significantly thicker than the less resistant units they overlie. Less resistant units in the plunge area are subject to the full, undissipated attack of the energy in the spillway flow. As the underlying units are scoured out, the upper units become undermined and collapse, usually in large, discrete blocks (fig. 4–2). Structural discontinuities (e.g., joints) in the upper unit control the size and shape of the eroded blocks. The process proceeds upstream, resulting in headward migration of the overfall until either the resistant unit collapses and is eroded away or the flow in the spillway stops.

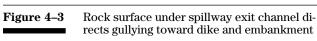
A common unconformity found in excavations for auxiliary spillways, particularly in the exit channels, is the soil/rock interface. Ordinarily, the surface of the rock is approximately parallel with the slope of the valley wall and, therefore, slopes toward the dam. Exceptions include sites located in areas of superimposed drainage patterns where the slope of the rock surface (i.e., the configuration of the buried topography) bears no relationship to the surface topography. Gullies typically begin either in the lower reaches of the constructed outlet channel or downstream below the constructed channel.

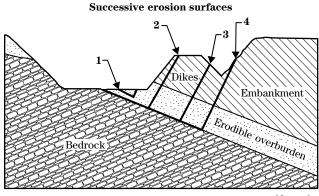
Once initiated, gullies migrate upstream toward the control section. Gullies form in the overburden materials that cover the underlying bedrock. These materials may be residuum, colluvium, talus, alluvium, or constructed fill. Such materials are generally more erodible than the embankment, which is composed of compacted materials. Once a downward-eroding gully encounters rock surface, the gullying process is forced to progress down the slope of the rock surface, which is toward the retaining dike or the dam. The concentrated flow in the gully then impinges on and attacks the dike or dam (fig. 4–3).











No scale

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631.0404 Rock mass properties: structural discontinuities

(a) Discontinuities related to plastic deformation

Apply standard geological mapping techniques to determine strike and dip of folded structures (e.g., bedding) and strike and plunge of linear aspects (e.g., fold axes). Use standard mapping symbols for strike and dip, fold axes, and related structures on the geologic evaluation map or sketch of the site (for standard symbols, see FGDC 2006 and AGI Data Sheets 2009).

(1) Folded structures

A fold is a curve or bend of a planar structure such as rock strata, bedding planes, foliation, or cleavage. It is usually the product of plastic deformation. Although any layered, banded, or foliated rock may display folds, they are most conspicuous in stratified sedimentary or volcanic rocks or their metamorphic equivalents. Folds may range in size from a few millimeters to hundreds of kilometers in wave length (the distance between adjacent crests of folds).

Regional folding may extend over large areas, resulting in an apparently uniform strike and dip at a particular site. Smaller local folds, however, are usually of more concern than those of a regional character. Minor folds that create channels for substantial water movement may escape detection in a geologic investigation of a structure site. Where such folds are suspected and anomalies are found in test holes, additional borings may be required to determine the location and size of the folds for design considerations. Descriptions of folds should indicate their size, location, type (anticline, syncline, drag), and the attitude of the limbs and axial plane.

(2) Foliation

Foliation is the planar arrangement of textural or structural features It is commonly associated with the planar or platy structure that results from flattening of the constituent grains of a metamorphic rock. A foliated rock tends to break along approximately parallel surfaces. Schistosity and gneissosity are the two main types of foliation.

Schistosity—A type of foliation or cleavage formed by dynamic metamorphism resulting in a parallel, planar arrangement of mineral grains of the platy, prismatic, or ellipsoidal types, such as mica and hornblende. Rocks of this type cleave readily. Schistosity is a function of compositional differences in the strata that developed in layers parallel to the foliation.

Gneissosity—A type of foliation formed by dynamic metamorphism that is regional in nature, resulting in coarse-textured lineations or distinct banding composed of alternating layers, bands, or streaks of siliceous and mafic minerals.

Banded rocks—Banded rocks consist of assemblages of parallel, tabular layers of rocks differing in composition, texture, or mineralogy associated with igneous and metamorphic activity; banding is analogous to bedding in sedimentary rocks. Banding may be inherited from bedding in source sediments or from layering in igneous rocks.

The orientation of foliation can have an effect on spillway flow that is analogous to the effect of corrugations and tight folds. Portions of spillway flow can be diverted in the direction of the strike of the foliation.

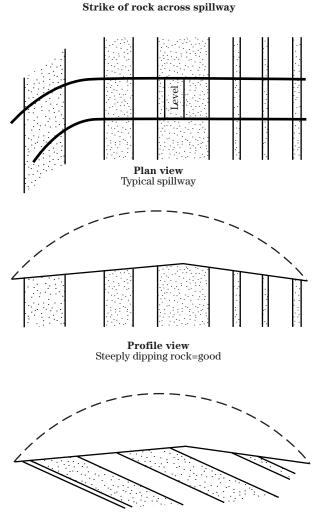
Engineering significance of structural discontinuities

Folded stratified rocks in auxiliary spillways where beds dip at an angle greater than 2 degrees (3.5%) require specific engineering designs. Resistant beds that form the surface (or near surface) of rock spillways can redirect spillway flow in the direction of the dip. Figure 4–4 illustrates some of the effects of strike and dip in rock spillways.

Corrugations and tight folds with wavelengths of approximately half the spillway width or less can also have engineering significance. Where the crest of a tight fold consists of an elevated prominent ridge of resistant rock, portions of the spillway flow can be diverted in the direction of the strike of the fold axis.

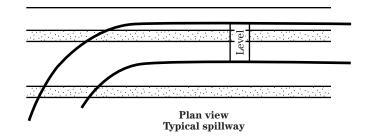
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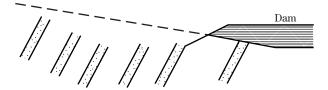
Figure 4–4 Effects of strike and dip in spillways



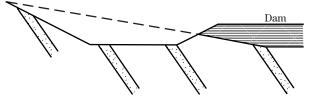
Profile view Gently dipping rock If rock dipping upstream=good If rock dipping downstream steeper than channel gradient=poor

Strike of rock across spillway

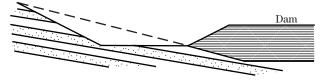




Spillway cross section Rock dipping away from dam=good



Spillway cross section Rock dipping toward dam=fair



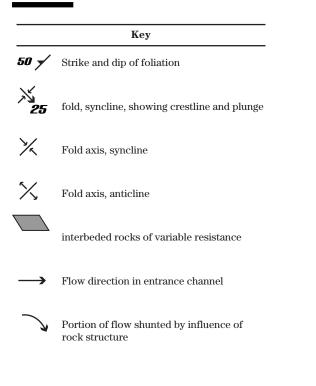
Spillway cross section Rock gently dipping toward dam=poor

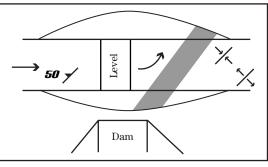
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The most favorable orientation of foliation (applies as well to the strike of fold axes of corrugations/tight folds) is within an arc ranging from 15 to 75 degrees in the quadrant pointing away from the dam. The least favorable orientation is within an arc ranging from 105 to 165 degrees in the quadrant pointing toward the dam (fig. 4–5).

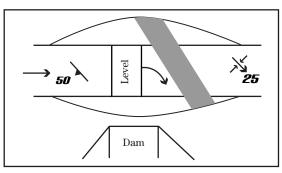
The following generalizations usually apply in folded rock terrain:

Figure 4–5 Effects of rock structure on spillway flow



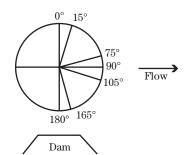


A. Plan—favorite oblique rock structures shunt flow away from dam



B. Plan—unfavorite oblique rock structures shunt flow away toward dam

C. Plan view of dam with spillway



- A rock unit dipping away from the dam is more favorable than a rock unit dipping toward the dam. Where the dip is consistent across the valley, consideration should be given to locating the spillway on the abutment that is underlain by rock dipping away from the dam.
- Relative favorability of the orientation of rock structure with respect to flow direction and location of dam.

| $15^{\circ}-75^{\circ}$ | best |
|----------------------------|------|
| 0° – 15° | good |
| $75^{\circ}-90^{\circ}$ | good |
| $90^{\circ}-105^{\circ}$ | fair |
| $165^\circ180^\circ$ | fair |
| $105^{\circ}-165^{\circ}$ | poor |

- A rock unit dipping in the upstream direction is more favorable than in the downstream direction.
- A rock unit that dips in the downstream direction, but less than the slope of the exit channel, tends to be more favorable than downstream dips that are greater than or equal to the channel gradient.

Rock structures include trends of axes of tight folds or corrugations, trends of foliation, and strikes of interbedded rocks of variable resistance.

(b) Discontinuities related to fracture deformation

A fracture (also called a crack, fissure, rupture, or parting) is any mechanical break in a rock mass. Fractures occur in all rock types in virtually all structural domains (Davis 1984). The characteristics of fractures strongly affect the engineering performance of rock.

Rock fractures can occur randomly or systematically and with or without relative displacement across the faces. A joint is a planar or near-planar surface of fracture or parting without visible displacement due to mechanical failure induced by stress in a rock mass. A fault is a fracture with visible relative displacement of opposite faces due to mechanical failure induced by stress.

General engineering significance of attributes of fractures

Hydraulic erodibility of rock is a function of complex interactions between rock material, rock mass properties and the hydraulic conditions of flow. Fracture-type discontinuities greatly influence rock mass erodibility. Although several important attributes of fractures have been identified and their engineering significance described individually in this chapter, it is clear that to predict engineering performance of excavated rock spillways, these attributes must be considered in an interdependent and interactive context. Table 4–12 summarizes the range in influence of attributes of fractures/joints on the erodibility of a rock mass.

| Table 4–12 | Summary of the influences of fracture attri- |
|------------|--|
| | butes on erodibility of a rock mass |

| Joint/fracture at- tribute | Most favorable | | Least favorable |
|-------------------------------|---|-------------------|---|
| Orientation | Parallel to flow or away from dam | \leftrightarrow | Perpendicu- lar to flow or toward dam |
| Joint pacing | Extremely wide | \leftrightarrow | Fissured |
| Bedding plane partings | Massive or unstratified | \leftrightarrow | Fissile |
| Aperture width | Extremely nar- row | \leftrightarrow | Wide |
| Infilling | Filled | \leftrightarrow | Open |
| | Plastic | \leftrightarrow | Nonplastic |
| | Inactive clay | \leftrightarrow | Swelling clay or sheet silicates, talc, graphite, or gypsum |
| Joint face | Unaltered | \leftrightarrow | Altered |
| Persistence | Very low | \leftrightarrow | Very high |
| Joint end type | Terminates in rock | \leftrightarrow | Terminates against another joint |

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(1) Random fractures

A random or nonsystematic fracture is a unique break in the rock with no obvious relationship to any other nearby fracture. A random fracture can originate as a fault or a joint. Random fractures are usually rough and highly irregular and have nonplanar surfaces with no apparent displacement. Patterns in apparently random fracturing in complex structural domains can often be differentiated by the application of stereographic projection techniques and by the analysis of joint orientation diagrams (App. C, Joint Orientation Diagrams).

(2) Systematic joints

Joints are defined as breaks in the rocks of the Earth's crust along which no movement has occurred. Joints may be from the induration process, or may be the product of tectonic activity. Joints usually occur in systematic patterns. They may allow movement of groundwater through otherwise impermeable material, which may create problems in design, construction, or functioning of the structure. The number and orientation of joint systems and their spacing also influences the ease of rock excavation. Description of joints should include their attitude, spacing, estimated depth of jointing, type of joints (strike, dip, or oblique) and kind of joint system.

Systematic joints are fractures that are generally evenly spaced and oriented in consistent patterns. Dips of systematic joints are typically high-angle to vertical. They cross other joints, with planar or broadly curved surfaces.

Partial exposures of joint faces are revealed by erosion, natural spalling, or excavation of the rock mass. A joint set is a group of more or less parallel joints, comprised of two or more intersecting joint sets.

(3) Bedding plane partings

Bedding plane partings are planar joints or fissures that split the rock along bedding planes. Bedding plane partings reflect changes in depositional conditions that differentiate successive layers in stratified sedimentary rock.

(4) Sheeting joints

Sheeting joints (also called stress relief joints) form by expansion or dilation accompanying release of load (pressure) during erosion or removal of overburden. Sheeting joints tend to form roughly parallel to the surface topography and tend to become more widely spaced, flatter, and more regular with depth. They rarely occur more than a few hundred meters deep. In horizontal sedimentary strata, sheeting joints often induce additional dilation on preexisting bedding plane partings. In massive igneous rocks, such as granite, sheeting joints can be spectacularly well developed by exfoliation; they tend to increase the erodibility of a rock mass and can be used advantageously in rock excavation.

(5) Slaty cleavage

Slaty cleavage is closely spaced, planar, parallel jointing developed in slates, phyllites, or tightly folded, homogeneous sedimentary rocks by low-grade metamorphism and deformation. The engineering significance of slaty cleavage is similar to that of fissility.

(6) Faults

A fault can occur as a single break or as a fault zone. A fault zone consists of numerous subparallel and interconnecting, closely spaced fault surfaces. The length of faults and shear zones and the amount of relative displacement can range from a few millimeters to hundreds of kilometers.

Fracture types and density descriptors are shown in tables 4-13 and 4-14.

A fault is defined as a break in the Earth's crust along which movement has taken place. Displacement may be a few inches or many miles. Faults may be detected by discontinuity of strata and by surface features. Aerial photographs often provide evidence of the presence of faults. Active faults may present serious hazards at a structural site. Inactive faults may also present special problems in design, construction, or functioning of the proposed structure. Faults encountered at sites should be described in detail, including type, such as normal or reverse, attitude of the fault plane, and the direction and amount of displacement. Of critical importance to the design of the structure will be the activity of the fault.

Faulting may bring together materials with different engineering properties and also modify groundwater conditions. Rock shattering, alteration of minerals, and fault gouge may also occur, presenting challenges for design of the structure.

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Table 4–13Fracture type

| | Fracture type |
|---|-------------------------------------|
| 1 | Random fracture |
| 2 | Systematic joint (high-angle) |
| 3 | Bedding plane parting |
| | (a) uniformly bedded |
| | (b) cross-bedded |
| | (c) rhythmically bedded |
| | (d) interfingered |
| | (e) graded bedding |
| | (f) current bedding (ripples, etc.) |
| 4 | Sheeting joint |
| 5 | Slaty cleavage, or fissile bedding |
| 6 | Fault |

dimensional expression of the joint surface is clear, express its orientation in terms of strike and dip. If the outcrop is so smooth and flat that only the trace of the joint is discernible, measure only the trend.

Identify precisely the measurement locations and elevations on a geologic evaluation map using standard symbols for strike and dip or trend. For presentation of orientation data for analysis, see Appendix C, Joint Orientation Diagrams.

| Table 4–14 | Fracture density description chart | | |
|-------------------------|------------------------------------|------------------|--|
| | Fracture density | | |
| Fracturing | Size range of pieces | Remarks | |
| Crushed | < 1 ft | Contains clay | |
| Intensely fractured | 1/16-in-0.1 ft | Contains no clay | |
| Closely fractured | 0.1-0.5 | | |
| Moderately fractured | 0.5–1.0 ft | | |
| Little fractured | 1.0–3.0 ft | | |

(c) Attributes of fractures

> 3.0

Characteristics of fractured rock include orientation, joint spacing, apperture width of joint face surfaces, type of infilling material, linear persistence, and type of joint ends.

(1) Orientation

Massive

Orientation is the establishment of the correct relationship in direction, usually with reference to points of the compass. Use a geological compass to measure the orientation of joints and fractures. If the three-

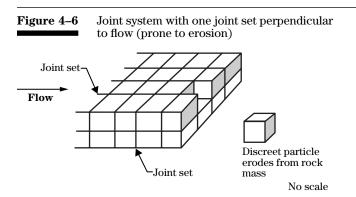
General engineering significance of orientation of rock joints and fractures

The orientation of joints and fractures within a rock mass relative to the direction of spillway flow strongly influences the strength anisotropy of the mass. If the direction of spillway flow is oriented perpendicular ($+/\sim$ 15°) to a persistent systematic joint set, the erosive attack will be acting against the weakest aspect of the rock mass. This relative orientation is the least desirable for the rock mass in resisting erosion. Once hydraulic erosion is initiated, headcutting tends to proceed in a consistent manner as discrete rock particles are eroded from the rock mass, typically in sizes defined by the spacing of the joint sets (fig. 4–6). The erodibility of a rock mass increases as joint spacing decreases.

Conversely, for spillways oriented parallel $(+/-15^{\circ})$ with a single persistent systematic joint set, the erosive attack will be acting against the most erosion-resistant aspect of the rock mass; this relative orientation is the most favorable for the rock mass in resisting erosion, provided that there are no persistent systematic joint sets oriented perpendicular to flow (fig. 4–7).

For two sets of persistent systematic joints, it is advantageous for the spillway to be oriented so that both sets are oblique to the direction of flow; i.e., neither set is within $+/-15^{\circ}$ of the direction of flow. This orientation improves discrete particle interlock and provides a more stable position for the center of mass of any given particle (fig. 4–8). Figure 4–7

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(2) Joint spacing

Joint spacing is the average spacing of joints within a joint set expressed in meters (or millimeters). The spacing and orientation of joints and bedding plane partings determine the size and shape of discrete rock particles.

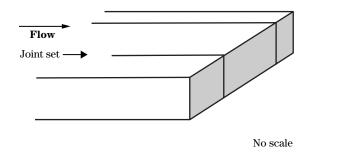
Use the fixed line survey method (app. B) to determine joint spacing. For systematic joints, place a 10-meter tape perpendicular to the trend of each joint set, count the number of joints that intersect the survey line, and divide the number counted by 10 to determine the average joint spacing. For random fractures, measure in three mutually perpendicular directions, if possible. If the vertical component is not available because of outcrop constraints, use data from drilling logs or rock core samples, if available, to estimate the spacing.

Descriptive terms should be consistent with the usage in table 4–15. Record the spacing of joints in each set and use table 4–15 as a guide for defining the spacing category.

Determine the mean diameter (D_{50}) of discrete rock particles by taking the cube root of the product of the average joint spacing of the three most prominent intersecting joint sets. For example, a rock mass with two intersecting vertical joint sets, one with an average spacing of 1.00 meter and the other 2.00 meters, and with bedding plane partings 0.10 meter, produces discrete rock particles with a mean diameter of 0.6

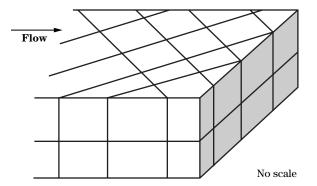
Table 4–15 Joint set spacing categories

| Spacing descriptors | | Spacing | Category |
|--------------------------|-------------------|---------------|----------|
| Bedding plane | Joint sets | (meters) | |
| Massive/ unstratified | Extremely wide | > 6.000 | 1 |
| Very thick-bedded | Very wide | 2.000-6.000 | 2 |
| Thick-bedded | Wide | 0.600 - 2.000 | 3 |
| Medium bedded | Mod. wide | 0.200-0.600 | 4 |
| Thin-bedded | Mod. close | 0.060-0.200 | 5 |
| Very thin-bedded | Close | 0.020-0.060 | 6 |
| Laminated | Very close | 0.006-0.020 | 7 |
| Thinly laminated | Shattered | 0.002-0.006 | 8 |
| Fissile | Fissured | < 0.002 | 9 |



One joint set parallel to flow (resists erosion)

| Figure 4–8 | Joint system with both sets oblique to flow |
|------------|---|
| | (resists erosion) |



meter. A mean diameter greater than or equal to 0.20 meter is used in the definition of rock in excavated earth spillways.

Engineering significance of size and shape of discrete rock particles

The size and shape of discrete rock particles are initially determined by the joint spacing of intersecting joint sets and bedding plane partings. The size of discrete rock particles strongly affects the erodibility of a rock mass. As the spacing of bedding plane partings and joints decreases, the erodibility and excavatability of a rock mass tend to increase.

Fissility is a primary foliation feature that is common in some fine-grained sedimentary rocks, particularly shales. Most shales are fissile or laminated. Fissility distinguishes shale from claystone or siltstone. In many shales, the most prominent fissility is parallel to the bedding, but in others, it is not. Fissility is responsible for the unravelling of shales under hydraulic attack and is a qualifier of material strength as it predisposes rock to mechanical weathering processes (wetting and drying, freeze-thaw, etc.) that can cause the rock to slake and disintegrate between flow events.

(3) Aperture width of joint face surfaces

Aperture refers to the opening between opposing faces of a joint, fracture, or fault.

In most instances, the width of an aperture is not constant along the trace of any given fracture or joint; therefore, a range category is recommended in table 4–16. Determine the aperture width category of each selected joint by measuring the aperture width at a sufficient number of places along the trace of the joint. If the width of an aperture of a particular joint varies through more than one range, state the length of the trace for which the aperture width category applies. For example, a 20-meter-long joint has a narrow aperture width (6-20 mm) for 13 meters and widens to moderately narrow (20-60 mm) for 7 meters. Clarify the variability by describing the joint in separately labeled segments on the Discontinuity Data Sheets, and show the location of the joint on the geologic evaluation map.

Table 4–16 Aperture category

| Aperture width category | Width range (mm) | Code |
|--------------------------------|---------------------|------|
| Wide | > 200 | 1 |
| Moderately wide | 60-200 | 2 |
| Moderately narrow | 20-60 | 3 |
| Narrow | 6–20 | 4 |
| Very narrow | 2-6 | 5 |
| Extremely narrow (hairline) | > 0–2 | 6 |

Engineering significance of joint aperture width

The aperture width of a joint affects the movement of water into the opening. The wider the aperture, the greater the potential for movement of the particle by uplift forces and pore pressure.

(4) Infilling

Infilling is the material occupying the aperture between joint faces; it is often referred to as gouge, breccia, or mylonite (for faults). The materials deposited in an opening can include airborne or washed materials, such as silt, clay, and other organic and mineral matter; or may include partially or completely remineralized vein deposits.

Soil materials in open fractures should be described according to standard soil logging terminology and classified by ASTM D2488 in the field or D2487 in the lab (Unified Soil Classification System (USCS)). Chemically precipitated or remineralized material in fractures should be identified by composition (quartz, carbonate, gypsum, etc.). The thickness of the infilling is usually the same as aperture width.

For each evaluated joint, record the general nature of the infilling according to the scheme in table 4–17. Report in the notes any range in variability.

Record the classification of the material according to the USCS, ASTM D2488.

The strength of the infilling can be estimated using Table 4–3, Correlation of Earth Material Hardness Categories with Laboratory Uniaxial Compressive Strength.

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Table 4–17 Joint infilling

| Nature of joint infilling | Code |
|---|------|
| Clean, open joint; no infilling present | 1 |
| Nonplastic silt (PI > 10), sand, or gravel; with or without crushed rock | 2 |
| Inactive clay or clay matrix; with or without crushed rock | 3 |
| Swelling clay or clay matrix; with or without crushed rock | 4 |
| Chlorite; talc; mica; serpentine; other sheet sili- cate; graphite; gypsum. Specify type in notes. | 5 |

Engineering significance of joint characteristics

The resistance to sliding of adjacent joint blocks affects excavatability, slope stability, and hydraulic erosion. Resistance to sliding can be either increased or decreased depending on:

- the aperture width
- continuity, texture, plasticity, consistency, permeability, and unconfined compressive strength of the infilling
- the character of the joint walls (Kirsten 1988)

Coatings or infolding of chlorite, talc, graphite, or other low-strength materials need to be identified because they increase the erodibility of the rock mass, especially when wet. Infillings that are dispersive or micaceous can squeeze or erode under fluid flow, contributing to increased erodibility and instability of the rock mass. Montmorillonitic clays can swell or cause swelling pressures. Fluid flow can readily remove cohesionless silts and sands, allowing for the entry and passage of moving water, which can cause uplift and sliding pressures on the discrete rock particles.

(5) Linear persistence

Linear persistence is the extent to which an individual fracture can be traced within a plane.

Persistence is one of the most important factors in rock performance evaluation. However, it is usually difficult to measure adequately because joints often extend beyond the outcrop area. Persistence can be quantified by measuring the discontinuity trace lengths on the surface of exposures.

The joints of some sets are often more continuous than those of other sets. Minor sets tend to terminate against primary sets or may terminate in solid rock (fig. 4–9).

Measure, in meters, the lengths of all selected joint traces in the direction of strike and in the direction of dip, if discernable. Note whether it is a strike, dip, or apparent trace.

Using table 4–18 as a guide, record the persistence category of each identified joint.

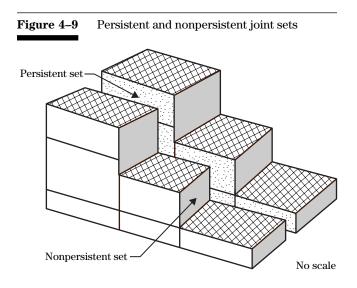


Table 4–18Joint persistence categories

| Joint trace persistence category | Trace length range (meters) | Code |
|-------------------------------------|--------------------------------|------|
| Very low | < 1 | 1 |
| Low | 13 | 2 |
| Medium | 3 10 | 3 |
| High | 10 20 | 4 |
| Very high | > 20 | 5 |

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Engineering significance of linear persistence of joints

Linear persistence strongly affects the hydraulic erodibility of a rock mass. A rock mass interrupted by highly persistent joints is potentially more erodible than a rock mass with less persistent joints. The higher the persistence category of systematic joint sets in a rock mass upstream of the crest of a slope or overfall, the greater the tendency for the development of tension cracks during flow. The persistence factor determines the height and width of a step, which would occur between adjacent joints for a tension (failure) surface to develop and for the process to repeat itself.

(6) Joint ends

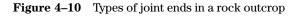
Joint ends refer to the nature of the terminations of a joint. Joints can terminate in solid rock, or they can terminate against another joint (like the letter "T"). Intersecting or through-going joints (like the letter "X"), are not considered to terminate at the intersection.

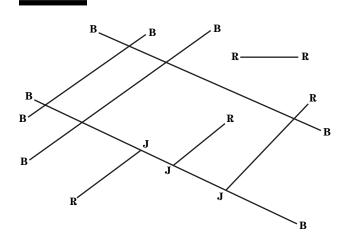
Record the type of joint termination for both ends of each joint according to the scheme in table 4–19. Figure 4–10 provides illustrated examples. Note that all length measurements in type B are considered to be minimum values since the ends are not observable.

In addition to weakening a rock mass by fracture, faults can juxtapose rock masses of widely differing engineering characteristics, which may lead to the formation of knickpoints and differential erosion of earth materials during spillway flow. Additionally, the trace of a fault can be enlarged by hydraulic erosion, directing portions of the flow along the trace. An orientation toward the dam or retaining dike is, therefore, unfavorable.

How the spillway channel is laid out relative to rock features can greatly affect its performance. Small changes in layout can either take advantage of favorable rock characteristics or avoid adverse features, resulting in significant improvement in spillway performance. Table 4–19Types of joint ends

| Joint type | Description |
|------------|--|
| R | Joint end terminates in solid rock |
| J | Joint end terminates against another joint |
| В | Joint end extends beyond outcrop area |





Engineering significance of joint ends

The type of joint end strongly influences the erodibility of a rock mass. Joints that terminate in solid rock have the least potential for forming a discrete rock particle. Joints that terminate against other joints greatly increase the erodibility of the rock mass, particularly if a persistent systematic joint set is oriented perpendicular to flow $(+/-15^{\circ})$.

Systematic joints and random fractures within a rock mass reduce its integrity and stability, and increase its excavatability and erodibility.

Additionally, by increasing the surface area on the rock mass, jointing increases the susceptibility to physical and chemical weathering, which will further weaken the rock mass over time.

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631.0405 Properties related to both rock materials and rock mass

Physical properties that are related to both the rock material and the rock mass include seismic velocity, weathering, and secondary cavities. Each of these characteristics can affect the hydraulic erodibility and excavation characteristics of rock.

(a) Seismic velocity

Seismic velocity is the velocity of propagation of pressure waves through a rock mass. Seismic velocity is a function of many rock material properties, including density, porosity, mineral composition, and the degree of cementation and consolidation; and rock mass properties, including degree of fracturing and degree of weathering. Different seismic velocities are also obtained for wet and dry joint apertures in rock masses which are otherwise identical.

Engineering significance of seismic velocity

Generally, the lower the seismic velocity of a rock mass, the greater the erodibility and excavatability of the rock mass. Most earth materials with seismic velocities less than 1,000 milliliters per second are prone to particle-by-particle erosion (Caterpillar Tractor Company 1983; Kirsten 1982); an obvious exception is highly plastic, nondispersive clay. The "Little Bear Residuum" in the Lower Mississippi River Valley is an example of an extremely erosionresistant residual soil associated with limestone parent material.

Seismic refraction surveys are routinely conducted during preliminary site investigations to provide a rapid assessment of depth to rock, configuration of the rock surface, and an indication of the relative integrity of foundation materials. The results of a seismic survey must be considered provisional until supplemented with "ground truth" provided by conventional drilling and excavation techniques in subsequent detailed investigations. The seismic velocity of an earth material is determined by a seismic survey using standard refraction techniques conducted by personnel with appropriate training and experience.

(b) Weathering

Weathering is the physical disintegration or chemical decomposition of earth materials resulting in changes in the color, texture, composition, density, or form, with little or no transport of the loosened or altered material. In this section, the scope of weathering is limited to the condition of the joint face rock material. The effects of weathering tend to diminish with depth and are best assessed on a macroscopic scale in the field.

The rate and type of rock weathering depend on climate, topography, vegetation, time, and the physical and chemical composition of the rock.

Physical weathering is the disintegration of rock into essentially unaltered pieces by the following processes:

- differential expansion by pressure release when rock is exposed at the surface or confining forces are reduced
- growth of crystals, such as ice or salt in cracks and pores
- differential expansion and contraction during cyclic heating and cooling
- the prying action of roots

Chemical weathering is the decomposition of the chemical structure of the mineral grains that make up a rock. All chemical weathering reactions use water as either a reactant or the carrier of reactant products. The chief chemical weathering processes are hydration, hydrolysis, oxidation, carbonation, and solution.

Use descriptors in table 4–20 to classify the weathering condition of the joint face rock material of identified joints.

| Table 4–20 | Descriptors for weathering condition of joint face rock material (after ISRM 1978) | |
|---------------|---|--|
| Descriptor | Weathering condition of joint face rock material | |
| Fresh | No sign of weathering of joint face rock material | |
| Discolored | Joint face rock material is iron-stained or discolored, but otherwise unweath- ered | |
| Disintegrated | Joint face rock material is physically disintegrated to a soil condition with original fabric still intact. Material is friable and mineral grains are not decomposed | |
| Decomposed | Joint face rock material is chemically altered to a soil condition with original fabric still intact; some or all of min- eral grains are decomposed | |

Engineering significance of weathering rock

Physical weathering results in the widening of existing discontinuities, the creation of new discontinuities by rock fracture, the opening of grain boundaries, and the fracture or cleavage of individual mineral grains.

Chemical weathering results in staining of rock surfaces in its early stages. Long-term chemical weathering results in the formation of clay minerals and chemical changes in the original minerals. In soluble rocks, it results in the widening of joints and the development of caves, sinkholes, and other karst features.

Weathering of rock material lowers the integrity of the rock and reduces its resistance to erosion and excavation. Where rock materials are known to weather rapidly (e.g., some shales in the Appalachian States or the Plains States), soil liners have been applied to the rock surface to inhibit weathering processes.

(c) Secondary cavities

Secondary cavities are open holes and voids, such as pits, vugs, and vesicles, that form as a result of chemical or mechanical processes acting on the rock mass after its formation. These types of secondary cavities are exclusive of fractures, jointing, and other open, planar, secondary features.

Identify the type of secondary cavities, if present, using the descriptors in table 4–21 as a guide.

Table 4–21 Descriptors for secondary cavities

| Secondary cavities | Description |
|------------------------|--|
| Pitted (1–10 mm) | Small openings, 1–10 mm |
| Vuggy (11–100 mm) | Openings often lined with crystals |
| Cavitied (> 100 mm) | Openings > 100 mm |
| Honeycombed | Only thin walls separate pits or vugs |
| Vesicular | Small openings in volcanic rocks of variable shape formed by entrapped gas bubbles during solidification |

Engineering significance of secondary cavities

Secondary cavities reduce the integrity of the rock mass by increasing porosity and by decreasing strength and unit weight. By increasing the surface area of the rock mass, secondary cavities increase its susceptibility to physical and chemical weathering, which further weakens the rock mass over time.

(d) Geohydrologic properties

Geohydrologic properties are attributes of a rock unit that affect the mode of occurrence, location, distribution, and flow characteristics of subsurface water within the unit. Geohydrologic properties include material and mass properties, but also account for the interaction and behavior of subsurface water within the rock mass. Field tests are typically used to evaluate geohydrologic properties of the rock mass, including secondary porosity, hydraulic conductivity, transmissivity, and other hydraulic parameters. Laboratory tests are used to evaluate geohydrologic properties of the rock material, such as primary porosity and permeability. Typical classification elements include:

- primary porosity (use data collected for rock material properties)
- secondary porosity (use data collected for rock mass properties)
- hydraulic conductivity (pump tests, published information)
- transmissivity (pump tests, published information)
- storativity/specific yield (pump tests, published information)
- soluble rock (occurrence of limestone, gypsum, or dolomite; see data collected for rock material properties)
- water table/potentiometric surface (measured in field, published data, date of measurement)
- aquifer type (unconfined, confined, leaky artesian, perched)
- electrical conductivity or resistivity (geophysical survey)

631.0406 Rock material field classification system

(a) Scope

The NRCS uses the RMFC system to classify rock and assess rock performance for engineering applications of rock. Classification alone does not preclude or replace laboratory testing for specific engineering design purposes.

(b) Outcrop confidence level

Outcrop confidence is the relative measure of the predictability or homogeneity of the structural domain and the lithology of the rock unit from one exposure to another or to the proposed site of investigation. The three levels of outcrop confidence are defined as:

- *Level 1: High*—Rock units are massive and homogeneous, vertically and laterally extensive. Site geology has a history of low tectonic activity.
- *Level II: Intermediate*—Rock characteristics are generally predictable, but have expected lateral and vertical variability. Structural features produced by tectonic activity tend to be systematic in orientation and spacing.
- *Level III: Low*—Rock conditions are extremely variable because of complex depositional or structural history, mass movement, or buried topography. Significant and frequent lateral and vertical changes in rock units can be expected.

Once a rock unit has been established, it can be defined by classification elements and analyzed for performance in relation to selected performance objectives.

(c) Classification elements

Classification elements are objective physical properties of a rock unit that define its engineering characteristics. Engineering classification of a rock unit considers the material properties of the rock itself, the structural characteristics of the in situ rock mass, Engineering Classification of Rock Materials Part 631 National Engineering Handbook

and the flow of water contained in the rock or within the system of discontinuities. The RMFC system uses three major types of classification elements: rock material properties, rock mass properties, and geohydrologic properties.

(d) Rock material classification process

The classification process consists of identifying the rock units at the site of investigation, describing them in terms of appropriate classification elements, and conducting the performance assessment. The performance assessment includes selecting the performance objectives for the proposed engineering uses of the rock and classifying the rock material within each selected objective.

- Identification of rock units
- Description of rock units by classification elements
 - rock material properties
 - rock mass properties
 - geohydrologic properties
- Selection of performance objectives
 - hydraulic erodibility in earth spillways
 - excavation characteristics
 - construction quality
 - fluid transmission
 - rock mass stability
- Classification by objective
 - determine class of rock or each selected performance objective

Step 1 Identify rock units—Rock unit identification includes determining the location and extent of each mappable unit in the outcrop or in the stratigraphic section at and near the site. When done in conjunction with a review of available data, maps, and literature, this fieldwork should provide the outcrop confidence level. If a formally recognized geologic formation is expected to perform as a homogeneous mass for engineering purposes, it may be considered a rock unit and identified by its formal stratigraphic name, such as Vishnu schist. All other mappable rock units should be assigned alphanumeric designations,

such as rock unit L–6. Each unit should be located on a geologic map by stationing, depth, and elevation. The outcrop confidence level should be determined and recorded in the notes.

Step 2 Describe rock units by classification elements—Each rock unit is characterized in terms of specific classification elements that affect performance of the rock for its intended use. The investigator may include any additional elements considered necessary for further clarification and refinement.

Rock material properties—Determined by examining and classifying hand specimens, core sections, drill cuttings, outcroppings, and disturbed samples using conventional geologic terminology.

Rock mass properties—Determined by geologic mapping, fixed line survey, geophysical survey, remote imagery interpretation, core sample analysis, and geomorphic analysis.

Geohydrologic properties—Determined by pressure testing; review of logs/data from water wells, observation wells, drill holes, and piezometers; review of published and unpublished maps and reports; interpretation of rock material and rock mass properties; and dye tests.

Step 3 Select performance objectives—This step involves the selection of performance objectives (engineering uses) of the rock for which an assessment of engineering performance is needed. Tables 4–22 through 4–27 provide the criteria for applicable classification elements that define each class for the five performance objectives considered in this system.

Step 4 Classification by objective—Determining the class of the rock material for all identified performance objectives is the final step in the procedure. Each of the five performance objectives has three classes of rock material (tables 4–22 through 4–27). A class defines the expected capabilities and limitations of the rock for each engineering use. End member classes I and III for each performance objective are intentionally defined restrictively. Therefore, rock material that classifies as class II is usually an indication that additional evaluation may be needed. Rock units assigned to the same class within a given performance objective can be expected to perform similarly.

(e) Evaluation of earth materials for excavation by a ripping index

NRCS Construction Specification 21, Excavation, provides criteria for defining rock excavation and common excavation for pay purposes. One of the criteria defining rock excavation is the need to use either heavy ripping equipment (rated above 250 flywheel horsepower) or blasting for excavation. This section describes the ripping index method for predicting the excavatability of any earth material. The index allows estimation of the minimum energy or effort required for excavation, on a scale ranging from hand tools to drilling and blasting.

A relationship may exist between rippability and hydraulic erodibility of rock, although no definitive study has been published to date. Caterpillar Tractor Company (1983) correlates the seismic velocities of some broad categories of earth materials with ripping performance of tractors.

An earth material classification system developed by Kirsten (1988) was field proven by ripping trials to reasonably and accurately predict the excavation characteristics of a broad range of earth materials. Kirsten's ripping index, k_n , allows earth material to be classified on a continuous basis from soft soil through hard rock.

Moore, Temple, and Kirsten (1994) developed the concept of a headcut erodibility index based on the analogy between bulldozer drawbar power required for ripping earth material and the hydraulic power associated with turbulent hydraulic energy dissipation at a headcut in a concentrated flow channel. Both indexes comprise the same parameters for rock material and rock mass. The classification system for the headcut erodibility index, k_h , (Temple and Moore 1997) is presented in NEH628.52.

(1) Hydraulic erodibility in earth spillways

For hydraulic erodibility in earth spillways, use table 4–22, which covers evaluation of erodibility of rock subject to intermittent flowing water.

For performance objectives for spillways in rock, refer to NEH628.52 and its appendices. Classification criteria included in this chapter are consistent with or are taken from NEH628.52.

(2) Excavation characteristics of rock

Cost of rock excavation may be greatly influenced by the nature of rock and secondary alteration. The geologist must describe the properties, quality, and quantity of rock proposed for excavation in terms translatable into workability by construction equipment, so that the amounts of rock excavation can be determined.

Table 4–22Hydraulic erodibility in earth spillways

| Classification elements | Class I | Class II | Class III |
|--|--|---|--|
| | Highly erosion resistant | Erosion resistant | Moderately erosion resistant |
| | Rock material experiences headcut erosion rates < 0.3 m/h (1 ft/h) at a unit dis- charge of 9.2 m ³ /s/m (100 ft ³ /s/ft) and 9 m (30 ft) of energy head. Must fulfill the following condition: | Rock material experi- ences headcut ero- sion rates from 0.3 to 3.0 m/h (1 to 10 ft/h) at a unit discharge of 9.2 m ³ /s/m (100 ft ³ /s/ ft) and 9 m (30 ft) of energy head. Must fulfill the fol- lowing condition: | Rock material experiences headcut erosion rates > 3.0 m/h (10 ft/h) at a unit discharge of 9.2 m ³ /s/m (100 ft ³ /s/ft) and 9 m (30 ft) of energy head. Must fulfill the following condi- tion: |
| Headcut erodibility index, k _h (NEH628.52), which comprises: material strength, block size, dis- continuity shear strength, relative ground structure | k _h > 100 | 10 <k<sub>h<100</k<sub> | 1 <k<sub>h<10</k<sub> |

Engineering Classification of Rock Materials Part 631 National Engineering Handbook

For further details on classification of rock for excavation, see NEH642, NRCS Standard Specifications, Construction, and Construction Materials.

For excavation characteristics, use table 4–23, which covers evaluation of excavation characteristics of rock.

(3) Construction quality of rock

For construction quality, use table 4–24, which shows rock quality classification for riprap, aggregate, embankment fill, and road armor for construction applications.

(4) Permeability of rock

For water transmission, table 4–25 shows the potential for water transmission through primary and secondary porosity in rock units underlying reservoirs, canals, and structural foundations; for excavation dewatering; for drainage for slope stability and for point and nonpoint source pollution; for groundwater yield for water supply development (water wells, springs, aquifers, basins) for groundwater recharge or disposal; and for saltwater intrusion.

(5) Rock mass stability

Table 4–26 shows rock mass stability of natural or constructed slopes for gravity or seismic activity.

(6) Ripping index method for estimating excavation characteristics of rock materials

Excavation characteristics of rock material are a function of the material's ripping index. The ripping index is determined by following the same procedures used in determining the headcut erodibility index (NEH628.52).

Table 4–27 correlates parameters for excavatability of rock materials. The table begins with the earth material that may be classified as the transition zone between "rock" and "soil." In the first column, rock material is delineated by hardness. The second column provides the minimum tools required for excavation. The excavation class (rock or common), as defined in NRCS Construction Specification 21, Excavation, is provided in parentheses. Determining the ripping index or seismic velocity allows prediction of the minimum size machine needed (expressed in flywheel horsepower) to excavate the material. The final column indicates the class of rock for excavation characteristics in the RMFC system.

Table 4–23 Excavation characteristics of rock

| Classification elements | Class I | Class II | Class III |
|---|--|--|--|
| | Very hard ripping to blast- ing | Hard ripping | Easy ripping |
| | Rock material requires drill- ing and explosives or impact procedures for excavation may classifyl as rock exca- vation (NRCS Construction Spec. 21). Must fulfill all conditions below: | Rock material requires rip- ping techniques for excava- tion may classify as rock excavation (NRCS Construc- tion Spec. 21). Must fulfill all conditions below: | Rock material can be excavated as common material by earth- moving or ripping equipment may classify as common excava- tion (NRCS Construction Spec. 21). Must fulfill all conditions below: |
| Headcut erodibility index, k _h (NEH628.52) | $kh \ge 100$ | $10 < k_h < 100$ | $k_h \leq 10$ |
| Seismic velocity, approxi- mate (ASTM D5777 and Caterpillar Handbook of Ripping, 1997) | > 2,450 m/s (> 8,000 ft/s) | 2,150–2,450 m/s (7,000–8,000 ft/s) | < 2,150 m/s (< 7,000 ft/s) |
| Minimum equipment size (flywheel power) required to excavate rock. All machines assumed to be heavy-duty, track-type back- hoes or tractors equipped with a single tine, rear- mounted ripper. | $\begin{array}{l} 260 \ kW \ (350hp), \\ for \ k_h < 1,000 \\ 375 \ kW \ (500hp), \\ for \ k_h < 10,000 \\ Blasting, \\ for \ k_h > 10,000 \end{array}$ | 185 kW (250 hp) | 110 kW (150 hp) |

1/ The classification is a general guide and does not prescribe the actual contract payment method to be used, nor supersedes NRCS contract documents. The classification is for engineering design purposes only.

Table 4–24 Construction quality of rock

| Classification elements | Class I | Class II | Class III |
|--------------------------------|---|---|--|
| | High grade | Medium grade | Low grade |
| | Rock material is suitable for high-stress aggregate, filter and drain material, riprap, and other construction applications requir- ing high durability. Must fulfill all conditions below: | Rock material is potentially suitable for construction applications. May require additional evaluation if at least one condition below is fulfilled: | Rock material is unsuitable for aggregate, filter and drain material, or riprap. Reacts essentially as a soil material in embankments. Must fulfill at least one condition below: |
| Strength (table 4–3) | > 50 MPa (> 7,250 lb/in ²) | 12.5–50 MPa (1,800–7,250 lb/in ²) | < 12.5 MPa (< 1,800 lb/in ²) |
| Hardness (table 4–3) | Hard to extremely hard rock | Moderately hard rock | Moderately soft to very soft rock |
| Unit weight (table 4–4) | >2.24 g/cm ³ (> 140 lb/ft ³) | 2.08–2.24 g/cm ³ (130–140 lb/ft ³) | 2.08 g/cm ³ (<130 lb/ft ³) |

Table 4–25Permeability of rock

| Classification elements | Class I | Class II | Class III |
|--|---|--|--|
| | Slowly permeable | Moderately permeable | Highly permeable |
| | Rock material has low capabil- ity to transmit water. Must fulfill all conditions below . | Rock material has potential to transmit water, generally through primary porosity. May require additional evaluation if at least one condition below is ful- filled. | Rock material has high capability to transmit water, generally through secondary porosity. Must fulfill at least one condition below. |
| Soluble rock | No soluble rock occurs in the rock mass. | Soluble rock, if present, oc- curs as a minor or second- ary constituent in the rock mass. | Soluble rock, such as limetone, gypsum, dolo- mite, marble, or halite, is the predominant rock type. |
| Primary porosity | Very low primary porosity; pores not interconnected or free draining | Pores visible under 10x hand lens; slowly free draining | Pores visible to naked eye; rapidly free draining |
| Number of joint sets (include bed- ding plane partings) | 1 joint set and random fractures; or rock mass intact and massive | ≤ 2 joint sets and random fractures | \geq 3 interconnecting joint sets |
| Joint aperture category | Extremely narrow, hairline (<2 mm) | Very narrow to narrow (2–6 mm) | Narrow to wide $(\geq 6 \text{ mm})$ |
| Infilling (including gouge) | Joints tight or filled with co- hesive, plastic clay or swelling fines matrix | Joints open or filled with nonplastic, nonswelling fines matrix | Joints open or filled with sand or gravel with < 15% cohesionless, nonplastic fines matrix |
| Major voids, solutional (caverns, sinkholes, enlarged joints), depo- sitional (lava tubes or interbed- ded gravels and lava beds) or structural/tectonic (faults, stress relief joints) | No major voids occur in rock mass | | Any types of major voids occur in rock mass |
| Hydraulic conductivity (dams and other structures) | $< 10^{-6}$ m/s (< 0.3 ft/d) | | $> 10^{-5}$ m/s (> 3 ft/d) |
| Transmissivity (irrigation wells) | $< 10^{-3} m^2/s (< 10^3 ft^2/d)$ | | $> 1 \text{ m}^2/\text{s} (> 10^5/\text{ft}^2/\text{d})$ |
| Transmissivity (domestic/ stock wells) | $< 10^{6} \text{ m}^{2/\text{s}} (< 1 \text{ ft}^{2/\text{d}})$ | | >10 ⁻⁴ m ² /s (>10 ² ft ² /d) |

Table 4–26 Rock mass stability

| Classification elements | Class I | Class II | Class III |
|--|--|---|---|
| | Stable | Potentially unstable | Unstable |
| | Rock material has very low potential for instability. Must fulfill all conditions below: | Rock material has potential for instability. May require additional evaluation if at least one condition below is fulfilled: | Rock material has significant potential for instability. Must fulfill at least one condi- tion below: |
| Strength (table 4–3) | > 50 MPa (> 7,250 lb/in ²) | 12.5–50 MPa (1,800–7,250 lb/in²) | < 12.5 MPa (< 1,800 lb/in ²) |
| Hardness (table 4–3) | Hard to extremely hard rock | Moderately hard rock | Moderately soft to very soft rock |
| RQD (ASTM D6032) | >75 | 25-75 | <25 |
| Number of joint sets in rock mass (include bedding plane partings) | 1 joint set and random frac- tures, or rock mass intact and massive; no adverse compo- nent of dip | ≤ 2 joint sets plus random fractures; no set contains adverse component of dip | ≥ 3 interconnecting joint sets; and > 1 set contains adverse component of dip |
| Joint water condition | Unconfined | Unconfined | Confined |

Table 4–27 Correlation of indicators of rock excavatability

| Earth material hardness (table 4–3) | Excavation description (excavation class) | Ripping index ^{1/} (kn) | Seismic velocity ^{2/} (ft/s) | Equipment ^{3/} needed for ex- cavation (hp) | RMFC system class (table 4–4) |
|---|--|--|---|--|-------------------------------------|
| Stiff cohesive soil or dense co- hesionless soil through very soft rock or hard, rock-like material | Power tools (common ^{4/}) | 0.10-1.0 | 2,000–5,000 | ≥ 100 | — |
| Soft through moderately soft rock | Easy ripping (common ^{4/}) | 1.0–10 | 5,000–7,000 | ≥ 150 | III |
| Moderately hard through hard rock | Hard ripping (rock $^{5/}$) | 10-100 | 7,000-8,000 | ≥ 250 | II |
| Very hard rock | Very hard ripping (rock ^{5/}) | 100–1,000 | 8,000–9,000 | ≥ 350 | Ι |
| Extremely hard rock | Extremely hard ripping to blasting (rock ^{5/}) | 1,000-10,000 | 9,000–10,000 | ≥ 500 | Ι |
| | Drilling and blasting (rock ^{5/}) | > 10,000 | > 10,000 | _ | Ι |

Because ripping index, kn, (Kirsten, 1988) is equal to headcut erodibility index, kh (NEH628.52), use k_h.
 Seismic velocity values are approximate, taken from ASTM D5777 and Caterpillar Handbook of Ripping (1997).

3/ Flywheel horsepower, machines assumed to be heavy-duty, track-type backhoe or tractor equipped with a single tooth, rear-mounted ripper.

4/ Meets criteria for common excavation in NRCS Construction Specification 21, Excavation.

5/ Meets criteria for rock excavation in NRCS Construction Specification 21, Excavation.

Note: The classification is a general guide and does not prescribe the actual contract payment method to be used, nor supersedes NRCS contract documents. The classification is for engineering design purposes only.

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Glossary

| Bedrock | A general term for in-place (in situ), usually solid rock that is exposed at the surface of the Earth or overlain by unconsolidated material. Colloquial syn.: ledge. See Rock mass. |
|------------------------|--|
| Bedding plane | A bedding plane is a planar or near planar interface that reflects a change in depositional conditions indicated by a parting, color difference, or both, and defines successive layers of stratified rock. |
| Cleavage | The property or tendency of a rock to split along secondary, aligned frac- tures or closely spaced, planar structures produced by deformation or metamorphism. |
| Clastic | Pertaining to a rock or sediment composed principally of broken fragments that are derived from preexisting rocks or minerals and that have been trans- ported some distance from their places of origin. See Pyroclastic. |
| Corrugations | Small-scale, tight folds; wrinkles; or furrows. |
| Density | The mass of a unit volume of substance at a specified temperature, ex- pressed in SI units of kilograms per cubic meter, but often is reported in grams per cubic centimeter. Syn.: unit weight, weight per unit volume. |
| Discontinuity | Any distinct break or interruption in the integrity of a rock mass. See Strati- graphic discontinuity; Structural discontinuity. |
| Discrete rock particle | An intact, sound fragment of rock material whose shape and size is defined by the discontinuities that form its margins. The mean diameter of a rock particle is defined as the cube root of the product of its three dimensions (length, width, and thickness). Syn.: rock block, intact block. |
| Durability | The resistance of discrete rock particles to breaking down over time due to weathering processes, hard wear, and abrasion. Syn.: weatherability. |
| Earth material | The entire spectrum of soil and rock materials. See table 4–2 for the ranges in strength and hardness of earth materials. |
| Earth spillway | An open channel spillway in earth materials without vegetation. |
| Fault | A fracture or fracture zone along which there has been relative displacement of opposite faces, due to mechanical failure by stress in a rock mass. |
| Fissility | The tendency of a rock to split or part into thin layers or plates. Bedding fissility is a primary feature inherited from the time of deposition; it is the result of compaction with concomitant recrystallization, and to some degree, is due to the parallel arrangement of platy or elongated, fine-grained mineral particles. |
| Fold axis | The intersection (which is a line) of the axial surface of a fold with any bed. The axial surface is the plane or surface that divides the fold as symmetri- cally as possible. |
| Fracture | A general term for any physical break in a rock mass without regard to the nature of the origin of the break. Syn.: crack, fissure, rupture, parting. |

| Chapter 4 | Engineering Classification of Rock Materials | Part 631 National Engineering Handbook |
|----------------------------------|---|--|
| Freeboard hydrograph | The hydrograph used to establish the of dam or structure; also used to eval spillway system. | |
| Geologic evaluation map (GEM) | A plan view diagram or drawing repre- entation and location of selected geol and symbols at a chosen scale and pr | 0 11 1 0 |
| Groundmass | [ign] The glassy or fine-grained crysta tals of a porphyritic igneous rock. | lline material between the larger crys- |
| Intact rock | Rock containing no discontinuities. S | yn.: rock material. |
| Joint | A planar or near-planar surface of fra placement, due to induced mechanica | |
| Joint set | A group of more or less parallel joints | 5. |
| Joint system | Two or more joint sets that intersect. | |
| Knickpoint | | specially a point of abrupt change or in- a stream or of its valley, resulting from resistant bed. |
| Lithosome | | rock of uniform character that has in- nt masses of different lithology. There igraphic nomenclature. |
| Master joint | A persistent joint plane of greater tha major joint, regional joint. | n average extent. Syn.: main joint, |
| Pyroclastic | Pertaining to clastic rock material for expulsion from a volcanic vent; it is n canic." See elastics. | rmed by volcanic explosion or aerial ot synonymous with the adjective "vol- |
| Rock mass | Rock as it occurs in situ, including its ering profile. Syn.: bedrock, rock out | system of discontinuities, and weath- crop. Colloquial: ledge. |
| Rock mass properties | in the field. Normally, rock mass prop | t be evaluated on a macroscopic scale berties, such as joints and faults, are too entirety and are difficult to impossible |
| Rock material | An intact, natural body or aggregate of discontinuities, such as joints. Syn: in | |
| Rock material properties | can be evaluated in hand specimen (a therefore, can be subject to meaningf | hand specimens, core sections, drill |

| Rock unit | An identifiable body of rock that is consistent in mineral, structural, and hydraulic characteristics. A rock unit can be considered essentially homoge- neous for engineering performance analysis and for descriptive and mapping purposes. A rock unit can be delineated by measurable or otherwise describ- able physical properties or features. The term is similar to lithosome in that the body of rock has consistent, mappable characteristics, but differs in that the body need not have been formed under uniform physicochemical condi- tions. |
|-------------------------------|---|
| Sheeting joint | A joint that forms by expansion (also called dilation, scaling, and exfolia- tion) accompanying release of load (pressure) during geologic erosion. Syn.: pressure release joint, stress relief joint, sheeting. |
| Sketch map | A map drawn freehand from observation or uncontrolled surveys showing only approximate space, scale, and orientation relationships of the main features of an area. |
| Slaty cleavage | Closely spaced, planar, parallel jointing of fine-grained, platy minerals de- veloped in slates and phyllites by low-grade metamorphism; or in tightly folded, homogeneous sedimentary rocks by deformation. Slaty cleavage is perpendicular to the direction of greatest shortening of the rocks in which it is formed. |
| Standard practice | A definitive procedure for performing one or more specific operations or functions that does not produce a test result. |
| Stratigraphic discontinuities | Features that originate contemporaneously with the formation of a rock mass. Syn.: primary discontinuities, first order discontinuities, syngenetic discontinuities. |
| Structural discontinuities | Features that develop after the initial formation of the rock as a result of external processes acting on the rock mass. Syn.: secondary discontinuities, second order discontinuities, epigenetic discontinuities. |
| Structural domain | A geologic locality having rock masses with similar major lithologic and structural features. Syn.: structural region. |
| Tight folds | Fold with an interlimb angle between 0° and 30° . |
| Trace | The intersection of a geological surface with another surface, e.g., the trace of a fault on the ground. The trace is a line. Syn.: trend, strike. |
| Unconformity | The surface separating two rock units that are not in stratigraphic sequence representing a substantial break in geologic time. Often, but not always, the younger stratum does not "conform" to the dip and strike of the underlying, older rocks; it usually implies geologic uplift and erosion. |
| Vein | An epigenetic mineral filling or deposit in the aperture of a fracture, in a rock mass, in tabular or sheet-like form. Quartz and calcite are the most common vein minerals. |

Appendix B

Rock Surveys

The fixed line survey

A fixed line survey is an inventory of all structural discontinuities that intersect a linear traverse of specified length and orientation. In structural domains where joint set patterns are obvious, the fixed line survey can be used to make rapid determinations of joint set spacings, which, in turn, are used to determine mean diameter and shape of discrete rock particles.

In complex structural domains where joints and fracture patterns are difficult to discern, the fixed line survey can be applied to differentiate subtle joint patterns and to inventory a representative sample of the joints for assessment of joint attributes.

If the survey line is parallel with the trend of a dominant joint set, the method is subject to potential undersampling and data bias.

Procedure

The rock outcrop in the area of interest must be well exposed, clean, and accessible for measurement and study. Cleaning can be accomplished using power equipment, hand tools, or pressurized air or water.

To determine the average spacing of a persistent systematic, high-angle joint set, orient a measuring tape perpendicular to the trend of the joint set. The length of the survey line depends on the spacing of the joints and the amount of outcrop available for measurement. As a rule of thumb, 10 meters or 10 joints, whichever is greater, is the recommended length of the survey line. Widely spaced joints require a longer line to obtain a meaningful average. In some instances, outcrop limitations necessitate shorter lines. Determine the spacing for each persistent joint set. To measure the number of bedding plane partings or sheeting joints on steep outcrops, place a weighted tape or telescoping range pole against the face. Where the vertical component is not exposed, estimate the spacings using test hole logs or core samples in the spillway near the survey line.

For complex structural domains with abundant unique fractures, establish three mutually perpendicular axes for survey lines—one axis parallel with the spillway flow direction and another perpendicular to the flow. The third axis, the vertical component, is described in the previous paragraph. The discrete rock particle mean diameter is determined by taking the cube root of the product of the average joint set spacings in the three surveyed directions.

To improve the determination of the average joint set spacing in a given dimension, survey more than one line. For example, use three parallel survey lines 5 meters apart and average the results. The number of lines needed is a function of the size and geologic complexity of the site.

Documentation

Show the location of each line on a geologic evaluation map and record its orientation, elevation, and ground coordinates or stationing on the Discontinuity Data Sheets (app. F).

The attributes of all structural discontinuities that intersect the fixed lines are then measured according to procedures described in this chapter and recorded on the Discontinuity Data Sheets (app. F).

The fixed area survey

A fixed area survey is an inventory of all structural discontinuities of specified area and shape. The fixed area survey is a detailed assessment of structural discontinuities at a project site.

The specified area may include: the entire auxiliary spillway, selected reaches between the control section and the outlet of the exit channel, or offsite areas that are considered germane to the study objectives. The shape of the survey area is usually square or rectangular; however, in some instances, a circular or rhomboidal shape may be useful.

Procedure

The rock outcrop in the area of interest must be well exposed, clean, and accessible for measurement and study. Cleaning can be accomplished using power equipment, hand tools, or pressurized air or water.

For mapping large areas or areas with a high density of fractures, subdivide the study area into manageable subareas. For square or rectangular areas, the subareas can be quarters, ninths, sixteenths, twenty-fifths, etc., of the total area. These subareas must be labeled appropriately.

To avoid measuring the same joint or feature twice, it is helpful to trace out with chalk the full length of each joint after it is measured.

Documentation

The attributes of all structural discontinuities within the survey area are evaluated according to procedures described in this chapter and recorded on the Discontinuity Data Sheets (app. F). Show the location of each feature on the geologic evaluation map, sketch, or on the corresponding subarea map.

Appendix C

Joint Orientation Diagrams

Joint orientation diagrams are useful statistical tools in the analysis of orientation data of joints, faults, and unique fractures. Preferred orientations can often be determined from data collected in complex structural domains. Structural orientation data can be summarized in pole diagrams, pole-density diagrams, rose diagrams, and strike histograms.

The analysis of joint data consists of standard and well known procedures in geological mapping. The information presented below is an overview of joint orientation diagrams.

Three-dimensional plots

Pole diagrams are spherical projections (stereographic displays) of three-dimensional, strike, and dip data. Two types of stereographic diagrams are displayed in figures 4A–1 and 4A–2. The Wulff net is an equal-angle projection in which the angular relationships between features are accurately represented (Wulff 1902). The Schmidt net (Lambert projection) (Sander and Schmidegg 1926; Lambert 1772) is an equal-area projection in which the spatial distribution of data is accurately represented.

The Schmidt net is the preferred stereographic projection for joint analysis; the Wulff net is not recommended because it has a built-in bias that invalidates the statistical distribution of plotted points.

All joint pole data are plotted onto a Schmidt net to distinguish joint set patterns. Contouring the values of the density of the poles (the concentration or number of points per unit area) on the resulting scatter diagram provides a measure of the degree of preferred orientation of structures in complex rock masses.

Where three-dimensional control on the attitude of the joints cannot be attained, either due to the nature of the surfaces of the outcrop or due to the collection of joint orientations from aerial photos, the orientation data can be plotted on two-dimensional plots, such as rose diagrams or strike histograms. In preparing rose diagrams and strike histograms, the trend or strike data are first organized into intervals of 5 or 10 degrees, encompassing the orientation range from west through north to east. The number (or percentage) of readings within each interval is summed. Data can

then be plotted as either a rose diagram or a strike histogram.

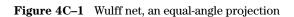
Rose diagrams

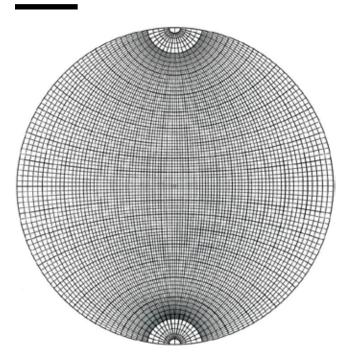
The number (or percentage) of joints that occur in each 5-degree (or 10°) interval is plotted in a family of concentric circles radiating outward from a common point. The data can also be plotted on the north side of a semicircle with similar graphic effect.

Strike histograms (frequency diagrams)

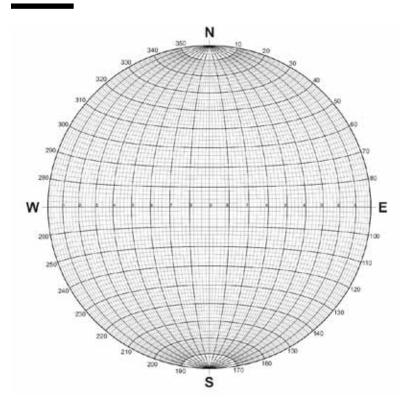
The intervals are plotted along the y-axis, and the number (or percentage) of joints occurring within each 5-degree (or 10°) interval is plotted on the x-axis of an x-y plot.

The advantage of two-dimensional plots is that dominant or preferred joint set orientations can be readily recognized at the high-frequency peaks. The disadvantage is that a given peak can mask two sets of joints of distinctly different inclination and/or dip direction.





 $Figure \ 4C-2 \quad {\rm Schmidt \ net \ (Lambert \ projection), \ an \ equal-area \ projection}$



Appendix D

(See also NEH628.52, Appendix C, Data Sheets for Headcut Erodibility Index) (Use one set of sheets for each material) Set _____ of ____

| General Information | | | |
|--|---------------------|-------------------|----------------|
| Watershed name: | | Site number: | State: |
| Investigator: | Title: | | _ Date: |
| Type of investigation: Intensity of investi | igation: | | |
| Reconnaissance | Subjective survey | Detail | ed/design |
| Preliminary | Objective survey | | |
| As-built/construction | Photograph numbers: | | |
| Spillway performance | | | |
| Earth Material (Soil/Rock) Unit Identific | ation | | |
| Formal rock type name or alphanumeric desig | gnation: | Rock code fre | om table 4D–5: |
| Soil group name (ASTM D2488): | | Unified classific | cation symbol: |
| Location (show on geol. map/sketch): Station | Offset (lt) | Offset (rt) | _ Elevation |
| Locality type (check one): Natural exposure_ | Channel side slo | ope Chann | el floor |

Earth Material Properties

| Table 4D–1 | Color (choose from up to three columns for |
|------------|--|
| | selected condition below) |

| Color | | | | |
|------------|------------|------------|---------|--|
| | | | Dry | |
| | | | Wet | |
| | | | Fresh | |
| | | | Altered | |
| | | | | |
| 1st | 2nd | 3rd | | |
| descriptor | descriptor | descriptor | | |
| light | yellowish | white | | |
| dark | buff | yellow | | |
| | orangish | buff | | |
| | brownish | orange | | |
| | pinkish | brown | | |
| | reddish | pink | | |
| | bluish | red | | |
| | purplish | blue | | |
| | orange | green | | |
| | olive | purple | | |
| | greenish | olive | | |
| | greyish | grey | | |
| | | black | | |

Other notes:

Table 4D-2Grain size (for sedimentary and pyroclasticrocks, check one below)

Sheet 1 of 3

| Descriptor | Grain size (mm/ sieve size) | |
|-------------|------------------------------------|--|
| Very coarse | > 75 mm/ 3 in. (cobble-size+) | |
| Coarse | 4.75–75 mm/ #4–3 in (gravel-size) | |
| Medium | 0.075–4.75 mm/ #200–#4 (sand-size) | |
| Fine | 0.005–0.075 mm (silt-size) | |
| Very fine | < 0.005 mm (clay-size) | |

 Table 4D–3
 Texture (for ign. and cryst. meta. rocks), check one below

| Descriptor | Description of texture | |
|-------------|--|--|
| Aphanitic | Components cannot be seen with naked eye | |
| Crystalline | Composed of interlocking crystals | |
| Glassy | Vitreous; without crystallization | |
| Pegmatitic | Very coarsely crystalline (> 10 mm diameter) | |
| Porphyritic | Large crystals set in fine-grained ground mass | |

Table 4D-4Secondary cavities

| Secondary cavities | Description | |
|---------------------|--|--|
| Pitted (1-10 mm) | Small openings, 1–10 mm | |
| Vuggy (11-100 mm) | Openings often lined with crystals | |
| Cavitied (> 100 mm) | Openings > 100 mm | |
| Honeycombed | Only thin walls separate pits or vugs | |
| Vesicular | Small openings in volcanic rocks of variable shape formed by entrapped gas bubbles during solidification | |

| Table 4D–5 | Rc | ock type class | Rock type classification (code numbers in parenthesis) | qumu | ers in I | parent | hesis) | | | | | | | |
|---------------------------|----------------|--|--|----------------|----------------------------|----------|---|--|--|--|------------------------|--|----------------------------|------------------|
| Genetic | | | Detrital sedimentary | | | | Chemical | Metamorphic | orphic | Pyroclastic | | lgen | lgeneous | |
| Usual structure | | | Bedded | | | | Bedded | Foliated | Massive | Bedded | | Mas | Massive | |
| Composition | | Grains of rock, quartz, feldspar | quartz, feldspar, | At le | At least 50% of | oť | Salts, | Quartz, feldspars, | Quartz, feldspars, | At least 50% of | Quartz, micas, c | Quartz, feldspars, micas, dark minerals | Feldspar; dark minerals | Dark minerals |
| | | | <u>o</u> | carb | grants are or carbonate | | silica, carbonaceous | micas, dark minerals | micas, dark minerals, carbonates | igneous rock | Acid | Intermediate | Basic | Ultrabasic |
| Very | | Gra | Grains are of rock fragments | nents | | | CLINKER (31) | TECTONIC BRECCIA (41) | RECCIA (41) | Rounded grains: | | | | |
| coarse- grained | sceons | Rounded grains: CONGOMERATE (11) | VTE (11) | | CALCIRUDITE | | SALINE ROCKS Halite (32) | MIGMATITE (42) METACON- GUERAT GNEISS (13) | METACON- GLOMERATE (51) | AGGLOMEHALE (61) Angular grains: | | PEGMATITE (71) | 1) | |
| | pny | Angular grains: BRECCIA (12) | | (1C) he | | | Anhydrite (33) Gypsum (34) | | MARBLE (52) GRANULITE (53) | VOLCĂNIC BRECCIA (62) | GRANITE (72) | GRAN | GABBRO (91) | PYROX- ENITE |
| Medium- grained (4) 60 | suceous | Grains are mainly mineral fragment SANDSTONE (13) | mineral fragments (13) | atritnarat | ferentiate | | CAL CAREOUS ROCKS | SCHIST (44) | QUARTZITE (54) | TUFF (63) | SYENITE (73) | (82) ANORTHOSITE (83) | DIABASE (92) | (01) PERIDO- |
| Fine- (200) mm | | GRAYWACKE | GRAYWACKE (Argillaceous ss) (15) | tihnu) | [2] | | | Amphibolite (45) | lite (45) | • | APLITE | MONZONITE | | (02) |
| 0.005 | r Lutaceous | MUDSTONE (16) SHAI F-fissila | SILTSTONE>50% fine-grained particles (18) | | CALCISILITTE | | LIMESTONE (35) | РНҮЦЛТЕ (46) | HORNFELS (55) | Fine-grained TUFF (64) | (74) RHYOLITE or | (84) Dacite (85) | BASALT (93) | DUNITE (03) |
| grained Predominan | Argillaceous o | mudstone (17) | CLAYSTONE>50% very fine grained particles (19) | DTSJRAM I I | | | DOLOMITE (36) | Mylonite (47) SLATE (48) | ie (47) | Very fine-grained TUFF (65) | (75) (75) | ANDESITE (86) | | BASAT (04) |
| |] | | | | | <u></u> | SILICEOUS ROCKS Chert (37) Flint (38) | Ultramylonite (49) | nite (49) | Welded TUFF (66) | ٥ ٩ | VOLCANIC GLASSES | SES | |
| amor- phous | | | | | | OĔ | CARBONACEOUS ROCKS | | | | OBSIDIAN (76) | OBSIDIAN PITCHSTONE TACHYLYTE | TACHYLYTE (87) | |
| | | | | | | <u> </u> | LIGNITE/COAL (39) | | | PUMICE (67) | | ì | ì | |

Sheet 2 of 3

Sheet 3 of 3

Table 4D-6 Hardness and unconfined compressive strength

| Hardness category | Typical range in unconfined com- pressive strength (MPa) | Strength value selected (MPa) | Field test on sample | Field test on outcrop |
|--|---|----------------------------------|--|--|
| Soil* | < 0.60 | | Use USCS classifications | |
| Very soft rock or hard, soil-like mate- rial | 0.60–1.25 | | Scratched with fingernail. Slight indentation by light blow of point of geologic pick. Requires power tools for excavation. Peels with pocket knife. | |
| Soft rock | 1.25–5.0 | | Permits denting by moderate pres- sure of the fingers. Handheld speci- men crumbles under firm blows with point of geologic pick. | Easily deformable with finger pressure. |
| Moderately soft rock | 5.0–12.5 | | Shallow indentations (1–3 mm) by firm blows with point of geologic pick. Peels with difficulty with pocket knife. Resists denting by the fingers, but can be abraded and pierced to a shallow depth by a pencil point. Crumbles by rubbing with fingers. | Crumbles by rubbing with fingers. |
| Moderately hard rock | 12.5–50 | | Cannot be scraped or peeled with pocket knife. Intact handheld specimen breaks with single blow of geologic hammer. Can be distinctly scratched with 20d common steel nail. Resists a pencil point, but can be scratched and cut with a knife blade. | Unfractured outcrop crumbles under light hammer blows. |
| Hard rock | 50–100 | | Handheld specimen requires more than one hammer blow to break it. Can be faintly scratched with 20d common steel nail. Resistant to abra- sion or cutting by a knife blade but can be easily dented or broken by light blows of a hammer. | Outcrop withstands a few firm blows before breaking. |
| Very hard rock | 100–250 | | Specimen breaks only by repeated, heavy blows with geologic hammer. Cannot be scratched with 20d com- mon steel nail. | Outcrop withstands a few heavy ringing ham- mer blows but will yield large fragments. |
| Extremely hard rock | > 250 | | Specimen can only be chipped, not broken by repeated, heavy blows of geologic hammer. | Outcrop resists heavy ringing hammer blows and yields, with diffi- culty, only dust and small fragments. |

Field assessment: _____ Uniaxial lab test: _____ O

____ Uniaxial lab test: _____ Other: _____ Rebound hammer (ASTM D5873): _____

* See NEH631.03 for consistency and density of soil materials. For very stiff soil, SPT N values = 15 to 30. For very soft rock or hard, soil-like material, SPT N values exceed 30 blows per foot.

Appendix E

Rock Mass Properties

Sheet 1 of 2

Line survey to determine average spacing of joint sets

- Plot location of surveyed lines on a geologic evaluation map or sketch.
- Notes: For systematic joint sets:

Lines 1 and 2 are for the two most persistent, high-angle, intersecting joints. Line 3 is for bedding plane partings or sheeting joints (the vertical axis).

- Notes: For apparently random fractures:
 - Line 1 is perpendicular to spillway flow direction.
 - Line 2 is parallel to spillway flow direction.
 - Line 3 is for bedding plane partings or sheeting joints (the vertical axis).

| Table 4E–1 | Line survey data |
|------------|------------------|
|------------|------------------|

| Survey line (axis) | a Plunge of line | b Trend (Azim) | c Line length (meters) | d No. of joints | e Average spacing d/c | f Spacing category |
|-----------------------|---------------------|-------------------|------------------------------|--------------------|-----------------------------|-----------------------|
| Line 1 (x) | | | | | | |
| Line 2 (y) | | | | | | |
| Line 3 (z) | | | | | | |

Spacing categories (for column f):

Table 4E–2 Joint set spacing categories

| Spacing des | criptors | Spacing | Category |
|------------------------|----------------|---------------|----------|
| Bedding plane partings | Joint sets | (meters) | |
| Massive/unstratified | Extremely wide | > 6.000 | 1 |
| Very thick-bedded | Very wide | 2.000-6.000 | 2 |
| Thick-bedded | Wide | 0.600 - 2.000 | 3 |
| Medium bedded | Mod. wide | 0.200-0.600 | 4 |
| Thin-bedded | Mod. close | 0.060 - 0.200 | 5 |
| Very thin-bedded | Close | 0.020-0.060 | 6 |
| Laminated | Very close | 0.006-0.020 | 7 |
| Thinly laminated | Shattered | 0.002 - 0.006 | 8 |
| Fissile | Fissured | < 0.002 | 9 |

Discrete rock particle mean diameter (use values in table 4E-1, column e):

 $\sqrt[3]{e_x e_y e_z} =$ meters

Other observations/notes on rock mass properties:

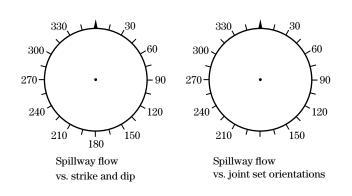
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Sketch map of auxiliary spillway in the space below.

Sheet 2 of 2

- On both circles, plot azimuths of spillway flow direction using an arrow.
- On left circle, plot strike and dip of rock. On right circle, plot trends and plunges of major joint sets.
- Indicate approximate location of dam (i.e., left side or right side).

Figure 4E–1 Plotted azimuth of spillway flow direction



Appendix F

Discontinuity Survey Data Sheets

Sheet 1 of 3

Notes:

- 1. Assign each discontinuity an ID number and show location on geologic evaluation map or sketch.
- 2. Use codes numbers from the following tables and enter data on the form at the bottom of this sheet and on Sheet 2 of 2.
- 3. Use code from table 4F–6, Rock Description Data Sheets for classifying compressive strength of infilling.
- 4. Classify infilling according to ASTM D2488 (UNRCS), record soil symbols on data sheet.

| Table 4F–1 | Discontinuity category | |
|---------------|------------------------|--------------------|
| Discontinuity | category | Code |
| Stratigraphic | | |
| Litho | some | |
| 110110 | Blanket | 1 |
| | Tongue | $\overline{2}$ |
| Shoe | string | $2 \\ 3 \\ 4 \\ 5$ |
| Lens | 0 | 4 |
| Slum | p feature | |
| | onformity | 6 |
| Structural | | |
| Plast | ic deformation | |
| | Folded rock | 7 |
| | Foliation | |
| | schistosity | 8 |
| | gneissosity | 9 |
| | Banded rock | 10 |
| Fract | ture deformation | |
| | om fracture | 11 |
| | matic joint set | 12 |
| Bedd | ing plane parting | |
| | Uniformly bedded | 13 |
| | Cross-bedded | 14 |
| | Rhythmic bedding | 15 |
| | Interfingered | 16 |
| | Graded bedding | 17 |
| (1) | Current bedding | 18 |
| | ting joint | 19 |
| | cleavage | 20 |
| Fault | | 21 |
| Othe | r (put in notes) | 22 |

Table 4F-2Joint end category

| Joint end category | End 1 | End 2 |
|---|-------|-------|
| Joint end extends beyond the exposure area | x b | x b |
| Joint end terminates in solid rock inside exposure area | t r | t r |
| Joint end terminates against another joint | tj | tj |

Table 4F-3Aperture category

| Aperture category | Width range (mm) | Code |
|-----------------------------|---------------------|------|
| Wide | > 200 | 1 |
| Moderately wide | 60-200 | 2 |
| Moderately narrow | 20-60 | 3 |
| Narrow | 6–20 | 4 |
| Very narrow | 2-6 | 5 |
| Extremely narrow (hairline) | > 0-2 | 6 |

Table 4F-4Nature of joint infilling

| Nature of joint infilling | Code |
|---|------|
| Clean, open joint; no infilling present | 1 |
| Nonplastic silt (PI > 10), sand, or gravel; with or without crushed rock | 2 |
| Inactive clay or clay matrix; with or without crushed rock | 3 |
| Swelling clay or clay matrix; with or without crushed rock | 4 |
| Chlorite; talc; mica; serpentine; other sheet sili- cate; graphite; gypsum. Specify type in notes. | 5 |

Table 4F–5 Joint persistence category

| -0 | John b | ersistence | calege |
|----|--------|------------|--------|
| | | | |

| Joint persistence category | Trace length (meters) | Code |
|----------------------------|--------------------------|------|
| Very low | < 1 | 1 |
| Low | 1–3 | 2 |
| Medium | 3–10 | 3 |
| High | 10-20 | 4 |
| Very high | > 20 | 5 |

 Table 4F-6
 Weathering condition of joints

| Descriptor | Weathering condition of joint face rock material | Code |
|---------------|--|------|
| Fresh | No sign of weathering. | 1 |
| Discolored | Iron-stained or discolored, but otherwise unweathered. | 2 |
| Disintegrated | Physically disintegrated to a soil condition with original fabric still intact. Material is friable and mineral grains are not decomposed. | 3 |
| Decomposed | Chemically altered to a soil condition with original fabric still intact. Some or all mineral grains are decomposed. | 4 |

 $\operatorname{Sheet} 2 \text{ of } 3$

Sheet 3 of 3

Table 4F-7 Work sheet for discontinuities

| | A | Measurement | | | В | | С | | Е | 5 | D2488 | F | |
|-------------------|---------------------|-----------------|-----|------------------|--------------------------|---------------------------|---------------|---------------|------------------------|---------------------------|-----------------------------|-------------------------------|-----------------------|
| Discon. ID no. | Discon. type no. | Trend (Azim) | Dip | Dip direction | Joint persist. (m) | Joint persist. code | End 1 code | End 2 code | Aper. width code | Nature infill. code | Strength infill. code | Infill. classif. (USCS) | Joint wea. code |
| 1 | I | | 1 | | I | I | | I | | | | I | |
| 2 | I | | 1 | | I | I | | I | | | | I | |
| 3 | I | | I | | I | I | | I | | | | I | |
| 4 | | | | | I | I | | | | | | I | |
| 5 | I | | I | | I | Ι | | I | | | | I | |
| 6 | I | | - 1 | | I | I | | 1 | | | | I | |
| 7 | I | | I | | I | I | | I | | | | I | |
| 8 | I | | I | | I | I | | 1 | | | | I | |
| 9 | I | | I | | I | I | | 1 | | | | I | |
| 10 | I | | I | | I | I | | | | | | I | |
| 11 | | | | | I | I | | | | | | I | |
| 12 | I | | I | | I | I | | 1 | | | | I | |
| 13 | I | | I | | I | I | | I | | | | I | |
| 14 | I | | I | | I | I | | 1 | | | | I | |
| 15 | I | | I | | I | I | | Ι | | | | I | |
| 16 | I | | I | | I | I | | Ι | | | | I | |
| 17 | I | | I | | I | I | | Ι | | | | I | |
| 18 | I | | I | | I | I | | Ι | | | | I | |
| 19 | I | | I | | I | I | | | | | | I | |
| 20 | I | | I | | I | I | | Ι | | | | I | |
| | | | I | 11 | I | I | | | | | | I | |
| | 1 | | I | | I | I | | | | | | I | |
| | I | | I | | I | I | | Ι | | | | I | |
| | I | | I | | I | I | | | | | | I | |
| | 1 | | I | | | I | | | | | | I | |
| | 1 | | I | | I | I | | | | | | I | |
| | | | I | | I | I | | | | | | I | |
| | I | | I | | I | I | | | | | | I | |
| | I | | I | | I | I | | I | | | | I | |

Other notes: