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SECTION 4-1
1. Name the two types of BJTs according to their structure.
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## CHECKUP

Answers can be found at www. pearsonhighered.com/floyd.
2. The BJT is a three-terminal device. Name the three terminals.
3. What separates the three regions in a BJT?

## 4-2 Basic BJT Operation

In order for a BJT to operate properly as an amplifier, the two $p n$ junctions must be correctly biased with external dc voltages. In this section, we mainly use the npn transistor for illustration. The operation of the $p n p$ is the same as for the $n p n$ except that the roles of the electrons and holes, the bias voltage polarities, and the current directions are all reversed.

After completing this section, you should be able to

- Discuss basic BJT operation
- Describe forward-reverse bias
- Show how to bias pnp and npn BJTs with dc sources
- Explain the internal operation of a BJT
- Discuss the hole and electron movement
- Discuss transistor currents
- Calculate any of the transistor currents if the other two are known


## Biasing

Figure 4-3 shows a bias arrangement for both npn and pnp BJTs for operation as an amplifier. Notice that in both cases the base-emitter (BE) junction is forward-biased and the base-collector (BC) junction is reverse-biased. This condition is called forward-reverse bias.


## Operation

To understand how a transistor operates, let's examine what happens inside the npn structure. The heavily doped $n$-type emitter region has a very high density of conduction-band (free) electrons, as indicated in Figure 4-4. These free electrons easily diffuse through the forwardbased BE junction into the lightly doped and very thin $p$-type base region, as indicated by the wide arrow. The base has a low density of holes, which are the majority carriers, as represented by the white circles. A small percentage of the total number of free electrons injected into the base region recombine with holes and move as valence electrons through the base region and into the emitter region as hole current, indicated by the red arrows.

$\triangle$ FIGURE 4-4
BJT operation showing electron flow.

When the electrons that have recombined with holes as valence electrons leave the crystalline structure of the base, they become free electrons in the metallic base lead and produce the external base current. Most of the free electrons that have entered the base do not recombine with holes because the base is very thin. As the free electrons move toward the reverse-biased BC junction, they are swept across into the collector region by the attraction of the positive collector supply voltage. The free electrons move through the collector region, into the external circuit, and then return into the emitter region along with the base current, as indicated. The emitter current is slightly greater than the collector current because of the small base current that splits off from the total current injected into the base region from the emitter.

## Transistor Currents

The directions of the currents in an $n p n$ transistor and its schematic symbol are as shown in Figure 4-5(a); those for a pnp transistor are shown in Figure 4-5(b). Notice that the arrow on the emitter inside the transistor symbols points in the direction of conventional current. These diagrams show that the emitter current $\left(I_{\mathrm{E}}\right)$ is the sum of the collector current $\left(I_{\mathrm{C}}\right)$ and the base current $\left(I_{\mathrm{B}}\right)$, expressed as follows:

$$
I_{\mathrm{E}}=I_{\mathrm{C}}+I_{\mathrm{B}}
$$

As mentioned before, $I_{\mathrm{B}}$ is very small compared to $I_{\mathrm{E}}$ or $I_{\mathrm{C}}$. The capital-letter subscripts indicate dc values.


Transistor currents.

SECTION 4-2 CHECKUP

1. What are the bias conditions of the base-emitter and base-collector junctions for a transistor to operate as an amplifier?
2. Which is the largest of the three transistor currents?
3. Is the base current smaller or larger than the emitter current?
4. Is the base region much thinner or much wider than the collector and emitter regions?
5. If the collector current is 1 mA and the base current is $10 \mu \mathrm{~A}$, what is the emitter current?

## 4-3 BJT Characteristics and Parameters

Two important parameters, $\beta_{\mathrm{DC}}$ (dc current gain) and $\alpha_{\mathrm{DC}}$ are introduced and used to analyze a BJT circuit. Also, transistor characteristic curves are covered, and you will learn how a BJT's operation can be determined from these curves. Finally, maximum ratings of a BJT are discussed.

After completing this section, you should be able to

- Discuss basic BJT parameters and characteristics and analyze transistor circuits
- Define dc beta $\left(\beta_{\mathrm{DC}}\right)$ and dc alpha $\left(\alpha_{\mathrm{DC}}\right)$
- Calculate $\left(\beta_{\mathrm{DC}}\right)$ and $\left(\alpha_{\mathrm{DC}}\right)$ based on transistor current
- Describe a basic dc model of a BJT
- Analyze BJT circuits
- Identify transistor currents and voltages - Calculate each transistor current
- Calculate each transistor voltage
- Interpret collector characteristic curves
- Discuss the linear region - Explain saturation and cutoff in relation to the curves
- Describe the cutoff condition in a BJT circuit
- Describe the saturation condition in a BJT circuit
- Discuss the dc load line and apply it to circuit analysis
- Discuss how $\beta_{\mathrm{DC}}$ changes with temperature
- Explain and apply maximum transistor ratings
- Derate a transistor for power dissipation
- Interpret a BJT datasheet


## FIGURE 4-6

Transistor dc bias circuits.

When a transistor is connected to dc bias voltages, as shown in Figure 4-6 for both npn and $p n p$ types, $V_{\mathrm{BB}}$ forward-biases the base-emitter junction, and $V_{\mathrm{CC}}$ reverse-biases the base-collector junction. Although in this chapter we are using separate battery symbols to represent the bias voltages, in practice the voltages are often derived from a single dc power supply. For example, $V_{\mathrm{CC}}$ is normally taken directly from the power supply output and $V_{\mathrm{BB}}$ (which is smaller) can be produced with a voltage divider. Bias circuits are examined thoroughly in Chapter 5.

(a) $n p n$

(b) $p n p$

## DC Beta ( $\boldsymbol{\beta}_{\mathrm{DC}}$ ) and DC Alpha ( $\alpha_{\mathrm{DC}}$ )

The dc current gain of a transistor is the ratio of the dc collector current $\left(I_{\mathrm{C}}\right)$ to the dc base current $\left(I_{\mathrm{B}}\right)$ and is designated dc beta ( $\beta_{\mathrm{DC}}$ ).

$$
\beta_{\mathrm{DC}}=\frac{I_{\mathrm{C}}}{I_{\mathrm{B}}}
$$

Typical values of $\beta_{\mathrm{DC}}$ range from less than 20 to 200 or higher. $\beta_{\mathrm{DC}}$ is usually designated as an equivalent hybrid ( $h$ ) parameter, $h_{\mathrm{FE}}$, on transistor datasheets. $h$-parameters are covered in Chapter 6. All you need to know now is that

$$
h_{\mathrm{FE}}=\beta_{\mathrm{DC}}
$$

The ratio of the dc collector current $\left(I_{\mathrm{C}}\right)$ to the dc emitter current $\left(I_{\mathrm{E}}\right)$ is the dc alpha $\left(\alpha_{\mathrm{DC}}\right)$. The alpha is a less-used parameter than beta in transistor circuits.

$$
\alpha_{\mathrm{DC}}=\frac{I_{\mathrm{C}}}{I_{\mathrm{E}}}
$$

Typically, values of $\alpha_{D C}$ range from 0.95 to 0.99 or greater, but $\alpha_{D C}$ is always less than 1. The reason is that $I_{\mathrm{C}}$ is always slightly less than $I_{\mathrm{E}}$ by the amount of $I_{\mathrm{B}}$. For example, if $I_{\mathrm{E}}=100 \mathrm{~mA}$ and $I_{\mathrm{B}}=1 \mathrm{~mA}$, then $I_{\mathrm{C}}=99 \mathrm{~mA}$ and $\alpha_{\mathrm{DC}}=0.99$.

EXAMPLE 4-1
Determine the dc current gain $\beta_{\mathrm{DC}}$ and the emitter current $I_{\mathrm{E}}$ for a transistor where $I_{\mathrm{B}}=50 \mu \mathrm{~A}$ and $I_{\mathrm{C}}=3.65 \mathrm{~mA}$.

$$
\begin{aligned}
\beta_{\mathrm{DC}} & =\frac{I_{\mathrm{C}}}{I_{\mathrm{B}}}=\frac{3.65 \mathrm{~mA}}{50 \mu \mathrm{~A}}=\mathbf{7 3} \\
I_{\mathrm{E}} & =I_{\mathrm{C}}+I_{\mathrm{B}}=3.65 \mathrm{~mA}+50 \mu \mathrm{~A}=\mathbf{3 . 7 0} \mathbf{~ m A}
\end{aligned}
$$

Related Problem*

## Transistor DC Model

You can view the unsaturated BJT as a device with a current input and a dependent current source in the output circuit, as shown in Figure 4-7 for an npn. The input circuit is a forward-biased diode through which there is base current. The output circuit is a dependent current source (diamond-shaped element) with a value that is dependent on the base current, $I_{\mathrm{B}}$, and equal to $\beta_{\mathrm{DC}} I_{\mathrm{B}}$. Recall that independent current source symbols have a circular shape.

\&FIGURE 4-7
Ideal dc model of an $n p n$ transistor.

## BJT Circuit Analysis

Consider the basic transistor bias circuit configuration in Figure 4-8. Three transistor dc currents and three dc voltages can be identified.
$I_{\mathrm{B}}$ : dc base current
$I_{\mathrm{E}}$ : dc emitter current
$I_{\mathrm{C}}$ : dc collector current
$V_{\mathrm{BE}}$ : dc voltage at base with respect to emitter
$V_{\mathrm{CB}}$ : dc voltage at collector with respect to base
$V_{\text {CE }}$ : dc voltage at collector with respect to emitter


$$
\triangle \text { FIGURE 4-8 }
$$

Transistor currents and voltages.

The base-bias voltage source, $V_{\mathrm{BB}}$, forward-biases the base-emitter junction, and the collector-bias voltage source, $V_{\mathrm{CC}}$, reverse-biases the base-collector junction. When the base-emitter junction is forward-biased, it is like a forward-biased diode and has a nominal forward voltage drop of

$$
V_{\mathrm{BE}} \cong 0.7 \mathrm{~V}
$$

Although in an actual transistor $V_{\mathrm{BE}}$ can be as high as 0.9 V and is dependent on current, we will use 0.7 V throughout this text in order to simplify the analysis of the basic concepts. Keep in mind that the characteristic of the base-emitter junction is the same as a normal diode curve like the one in Figure 2-12.

Since the emitter is at ground ( 0 V ), by Kirchhoff's voltage law, the voltage across $R_{\mathrm{B}}$ is

$$
V_{R_{\mathrm{B}}}=V_{\mathrm{BB}}-V_{\mathrm{BE}}
$$

Also, by Ohm's law,

$$
V_{R_{\mathrm{B}}}=I_{\mathrm{B}} R_{\mathrm{B}}
$$

Substituting for $V_{R_{\mathrm{B}}}$ yields

$$
I_{\mathrm{B}} R_{\mathrm{B}}=V_{\mathrm{BB}}-V_{\mathrm{BE}}
$$

Solving for $I_{\mathrm{B}}$,

Equation 4-4

Equation 4-5

Equation 4-6
-

$$
I_{\mathrm{B}}=\frac{V_{\mathrm{BB}}-V_{\mathrm{BE}}}{R_{\mathrm{B}}}
$$

The voltage at the collector with respect to the grounded emitter is

$$
V_{\mathrm{CE}}=V_{\mathrm{CC}}-V_{R_{\mathrm{C}}}
$$

Since the drop across $R_{\mathrm{C}}$ is

$$
V_{R_{\mathrm{C}}}=I_{\mathrm{C}} R_{\mathrm{C}}
$$

the voltage at the collector with respect to the emitter can be written as

$$
V_{\mathbf{C E}}=V_{\mathbf{C C}}-I_{\mathbf{C}} R_{\mathbf{C}}
$$

where $I_{\mathrm{C}}=\beta_{\mathrm{DC}} I_{\mathrm{B}}$.
The voltage across the reverse-biased collector-base junction is

$$
V_{\mathrm{CB}}=V_{\mathrm{CE}}-V_{\mathrm{BE}}
$$

## EXAMPLE 4-2

Determine $I_{\mathrm{B}}, I_{\mathrm{C}}, I_{\mathrm{E}}, V_{\mathrm{BE}}, V_{\mathrm{CE}}$, and $V_{\mathrm{CB}}$ in the circuit of Figure 4-9. The transistor has a $\beta_{\mathrm{DC}}=150$.

## FIGURE 4-9



Solution From Equation $4-3, V_{\mathrm{BE}} \cong \mathbf{0 . 7} \mathbf{V}$. Calculate the base, collector, and emitter currents as follows:

$$
\begin{aligned}
I_{\mathrm{B}} & =\frac{V_{\mathrm{BB}}-V_{\mathrm{BE}}}{R_{\mathrm{B}}}=\frac{5 \mathrm{~V}-0.7 \mathrm{~V}}{10 \mathrm{k} \Omega}=\mathbf{4 3 0} \boldsymbol{\mu} \mathbf{A} \\
I_{\mathrm{C}} & =\beta_{\mathrm{DC}} I_{\mathrm{B}}=(150)(430 \mu \mathrm{~A})=\mathbf{6 4 . 5} \mathbf{~ m A} \\
I_{\mathrm{E}} & =I_{\mathrm{C}}+I_{\mathrm{B}}=64.5 \mathrm{~mA}+430 \mu \mathrm{~A}=\mathbf{6 4 . 9} \mathbf{~ m A}
\end{aligned}
$$

Solve for $V_{\mathrm{CE}}$ and $V_{\mathrm{CB}}$.

$$
\begin{aligned}
& V_{\mathrm{CE}}=V_{\mathrm{CC}}-I_{\mathrm{C}} R_{\mathrm{C}}=10 \mathrm{~V}-(64.5 \mathrm{~mA})(100 \Omega)=10 \mathrm{~V}-6.45 \mathrm{~V}=\mathbf{3 . 5 5} \mathrm{V} \\
& V_{\mathrm{CB}}=V_{\mathrm{CE}}-V_{\mathrm{BE}}=3.55 \mathrm{~V}-0.7 \mathrm{~V}=\mathbf{2 . 8 5} \mathrm{V}
\end{aligned}
$$

Since the collector is at a higher voltage than the base, the collector-base junction is reverse-biased.

Related Problem Determine $I_{\mathrm{B}}, I_{\mathrm{C}}, I_{\mathrm{E}}, V_{\mathrm{CE}}$, and $V_{\mathrm{CB}}$ in Figure 4-9 for the following values: $R_{\mathrm{B}}=22 \mathrm{k} \Omega$, $R_{\mathrm{C}}=220 \Omega, V_{\mathrm{BB}}=6 \mathrm{~V}, V_{\mathrm{CC}}=9 \mathrm{~V}$, and $\beta_{\mathrm{DC}}=90$.

Open the Multisim file E04-02 in the Examples folder on the companion website. Measure each current and voltage and compare with the calculated values.

## Collector Characteristic Curves

Using a circuit like that shown in Figure 4-10(a), a set of collector characteristic curves can be generated that show how the collector current, $I_{\mathrm{C}}$, varies with the collector-toemitter voltage, $V_{\mathrm{CE}}$, for specified values of base current, $I_{\mathrm{B}}$. Notice in the circuit diagram that both $V_{\mathrm{BB}}$ and $V_{\mathrm{CC}}$ are variable sources of voltage.

Assume that $V_{\mathrm{BB}}$ is set to produce a certain value of $I_{\mathrm{B}}$ and $V_{\mathrm{CC}}$ is zero. For this condition, both the base-emitter junction and the base-collector junction are forward-biased because the base is at approximately 0.7 V while the emitter and the collector are at 0 V . The base current is through the base-emitter junction because of the low impedance path to

(a) Circuit

(b) $I_{\mathrm{C}}$ versus $V_{\mathrm{CE}}$ curve for one value of $I_{\mathrm{B}}$

## FIGURE 4-10

Collector characteristic curves.
ground and, therefore, $I_{\mathrm{C}}$ is zero. When both junctions are forward-biased, the transistor is in the saturation region of its operation. Saturation is the state of a BJT in which the collector current has reached a maximum and is independent of the base current.

As $V_{\mathrm{CC}}$ is increased, $V_{\mathrm{CE}}$ increases as the collector current increases. This is indicated by the portion of the characteristic curve between points $A$ and $B$ in Figure 4-10(b). $I_{\mathrm{C}}$ increases as $V_{\mathrm{CC}}$ is increased because $V_{\mathrm{CE}}$ remains less than 0.7 V due to the forward-biased base-collector junction.

Ideally, when $V_{\mathrm{CE}}$ exceeds 0.7 V , the base-collector junction becomes reverse-biased and the transistor goes into the active, or linear, region of its operation. Once the basecollector junction is reverse-biased, $I_{\mathrm{C}}$ levels off and remains essentially constant for a given value of $I_{\mathrm{B}}$ as $V_{\mathrm{CE}}$ continues to increase. Actually, $I_{\mathrm{C}}$ increases very slightly as $V_{\mathrm{CE}}$ increases due to widening of the base-collector depletion region. This results in fewer holes for recombination in the base region which effectively causes a slight increase in $\beta_{\mathrm{DC}}$. This is shown by the portion of the characteristic curve between points $B$ and $C$ in Figure $4-10(b)$. For this portion of the characteristic curve, the value of $I_{\mathrm{C}}$ is determined only by the relationship expressed as $I_{\mathrm{C}}=\beta_{\mathrm{DC}} I_{\mathrm{B}}$.

When $V_{\mathrm{CE}}$ reaches a sufficiently high voltage, the reverse-biased base-collector junction goes into breakdown; and the collector current increases rapidly as indicated by the part of the curve to the right of point $C$ in Figure 4-10(b). A transistor should never be operated in this breakdown region.

A family of collector characteristic curves is produced when $I_{\mathrm{C}}$ versus $V_{\mathrm{CE}}$ is plotted for several values of $I_{\mathrm{B}}$, as illustrated in Figure 4-10(c). When $I_{\mathrm{B}}=0$, the transistor is in the cutoff region although there is a very small collector leakage current as indicated. Cutoff is the nonconducting state of a transistor. The amount of collector leakage current for $I_{\mathrm{B}}=0$ is exaggerated on the graph for illustration.

EXAMPLE 4-3
Sketch an ideal family of collector curves for the circuit in Figure 4-11 for $I_{\mathrm{B}}=5 \mu \mathrm{~A}$ to $25 \mu \mathrm{~A}$ in $5 \mu \mathrm{~A}$ increments. Assume $\beta_{\mathrm{DC}}=100$ and that $V_{\mathrm{CE}}$ does not exceed breakdown.


Solution Using the relationship $I_{\mathrm{C}}=\beta_{\mathrm{DC}} I_{\mathrm{B}}$, values of $I_{\mathrm{C}}$ are calculated and tabulated in Table 4-1. The resulting curves are plotted in Figure 4-12.

| TABLE 4-1 | $I_{\mathrm{B}}$ | $I_{\mathrm{C}}$ |
| :--- | :--- | :---: | :---: |
|  | $5 \mu \mathrm{~A}$ | 0.5 mA |
|  | $10 \mu \mathrm{~A}$ | 1.0 mA |
|  | $15 \mu \mathrm{~A}$ | 1.5 mA |
|  | $20 \mu \mathrm{~A}$ | 2.0 mA |
|  | $25 \mu \mathrm{~A}$ | 2.5 mA |



FIGURE 4-12

Related Problem Where would the curve for $I_{\mathrm{B}}=0$ appear on the graph in Figure 4-12, neglecting collector leakage current?

## Cutoff

As previously mentioned, when $I_{\mathrm{B}}=0$, the transistor is in the cutoff region of its operation. This is shown in Figure 4-13 with the base lead open, resulting in a base current of zero. Under this condition, there is a very small amount of collector leakage current, $I_{\text {CEO }}$, due mainly to thermally produced carriers. Because $I_{\text {CEO }}$ is extremely small, it will usually be neglected in circuit analysis so that $V_{\mathrm{CE}}=V_{\mathrm{CC}}$. In cutoff, neither the base-emitter nor the base-collector junctions are forward-biased. The subscript CEO represents collector-to-emitter with the base open.


4 FIGURE 4-13
Cutoff: Collector leakage current ( $I_{\text {CEO }}$ ) is extremely small and is usually neglected. Base-emitter and base-collector junctions are reverse-biased.

## Saturation

When the base-emitter junction becomes forward-biased and the base current is increased, the collector current also increases $\left(I_{\mathrm{C}}=\beta_{\mathrm{DC}} I_{\mathrm{B}}\right)$ and $V_{\mathrm{CE}}$ decreases as a result of more drop across the collector resistor ( $V_{\mathrm{CE}}=V_{\mathrm{CC}}-I_{\mathrm{C}} R_{\mathrm{C}}$ ). This is illustrated in Figure $4-14$. When $V_{\mathrm{CE}}$ reaches its saturation value, $V_{\mathrm{CE}(\mathrm{sat})}$, the base-collector junction becomes forward-biased and $I_{\mathrm{C}}$ can increase no further even with a continued increase in $I_{\mathrm{B}}$. At the point of saturation, the relation $I_{\mathrm{C}}=\beta_{\mathrm{DC}} I_{\mathrm{B}}$ is no longer valid. $V_{\mathrm{CE}(\mathrm{sat})}$ for a transistor occurs somewhere below the knee of the collector curves, and it is usually only a few tenths of a volt.

- FIGURE 4-15

DC load line on a family of collector characteristic curves illustrating the cutoff and saturation conditions.

## - FIGURE 4-14

Saturation: $A s I_{B}$ increases due to increasing $V_{\mathrm{BB}}, I_{\mathrm{C}}$ also increases and $V_{\mathrm{CE}}$ decreases due to the increased voltage drop across $R_{\mathrm{C}}$. When the transistor reaches saturation, $I_{C}$ can increase no further regardless of further increase in $I_{\mathrm{B}}$. Base-emitter and base-collector junctions are forward-biased.


## DC Load Line

Cutoff and saturation can be illustrated in relation to the collector characteristic curves by the use of a load line. Figure $4-15$ shows a dc load line drawn on a family of curves connecting the cutoff point and the saturation point. The bottom of the load line is at ideal cutoff where $I_{\mathrm{C}}=0$ and $V_{\mathrm{CE}}=V_{\mathrm{CC}}$. The top of the load line is at saturation where $I_{\mathrm{C}}=I_{\mathrm{C}(\text { sat })}$ and $V_{\mathrm{CE}}=V_{\mathrm{CE}(\mathrm{sat})}$. In between cutoff and saturation along the load line is the active region of the transistor's operation. Load line operation is discussed more in Chapter 5.


Determine whether or not the transistor in Figure 4-16 is in saturation. Assume
$V_{\mathrm{CE}(\mathrm{sat})}=0.2 \mathrm{~V}$.


Solution First, determine $I_{\mathrm{C}(\text { sat })}$.

$$
I_{\mathrm{C}(\mathrm{sat})}=\frac{V_{\mathrm{CC}}-V_{\mathrm{CE}(\mathrm{sat})}}{R_{\mathrm{C}}}=\frac{10 \mathrm{~V}-0.2 \mathrm{~V}}{1.0 \mathrm{k} \Omega}=\frac{9.8 \mathrm{~V}}{1.0 \mathrm{k} \Omega}=9.8 \mathrm{~mA}
$$

Now, see if $I_{\mathrm{B}}$ is large enough to produce $I_{\mathrm{C}(\text { sat })}$.

$$
\begin{aligned}
I_{\mathrm{B}} & =\frac{V_{\mathrm{BB}}-V_{\mathrm{BE}}}{R_{\mathrm{B}}}=\frac{3 \mathrm{~V}-0.7 \mathrm{~V}}{10 \mathrm{k} \Omega}=\frac{2.3 \mathrm{~V}}{10 \mathrm{k} \Omega}=0.23 \mathrm{~mA} \\
I_{\mathrm{C}} & =\beta_{\mathrm{DC}} I_{\mathrm{B}}=(50)(0.23 \mathrm{~mA})=11.5 \mathrm{~mA}
\end{aligned}
$$

This shows that with the specified $\beta_{\mathrm{DC}}$, this base current is capable of producing an $I_{\mathrm{C}}$ greater than $I_{\mathrm{C}(\mathrm{sat})}$. Therefore, the transistor is saturated, and the collector current value of 11.5 mA is never reached. If you further increase $I_{\mathrm{B}}$, the collector current remains at its saturation value of 9.8 mA .

Related Problem Determine whether or not the transistor in Figure 4-16 is saturated for the following values: $\beta_{\mathrm{DC}}=125, V_{\mathrm{BB}}=1.5 \mathrm{~V}, R_{\mathrm{B}}=6.8 \mathrm{k} \Omega, R_{\mathrm{C}}=180 \Omega$, and $V_{\mathrm{CC}}=12 \mathrm{~V}$.


Open the Multisim file E04-04 in the Examples folder on the companion website. Determine if the transistor is in saturation and explain how you did this.

## More About $\boldsymbol{\beta}_{\text {DC }}$

The $\beta_{\mathrm{DC}}$ or $h_{\mathrm{FE}}$ is an important BJT parameter that we need to examine further. $\beta_{\mathrm{DC}}$ is not truly constant but varies with both collector current and with temperature. Keeping the junction temperature constant and increasing $I_{\mathrm{C}}$ causes $\beta_{\mathrm{DC}}$ to increase to a maximum. A further increase in $I_{\mathrm{C}}$ beyond this maximum point causes $\beta_{\mathrm{DC}}$ to decrease. If $I_{\mathrm{C}}$ is held constant and the temperature is varied, $\beta_{\mathrm{DC}}$ changes directly with the temperature. If the temperature goes up, $\beta_{\mathrm{DC}}$ goes up and vice versa. Figure $4-17$ shows the variation of $\beta_{\mathrm{DC}}$ with $I_{\mathrm{C}}$ and junction temperature $\left(T_{\mathrm{J}}\right)$ for a typical BJT.


AFIGURE 4-17
Variation of $\boldsymbol{\beta}_{\mathrm{DC}}$ with $I_{\mathrm{C}}$ for several temperatures.
A transistor datasheet usually specifies $\beta_{\mathrm{DC}}\left(h_{\mathrm{FE}}\right)$ at specific $I_{\mathrm{C}}$ values. Even at fixed values of $I_{\mathrm{C}}$ and temperature, $\beta_{\mathrm{DC}}$ varies from one device to another for a given type of transistor due to inconsistencies in the manufacturing process that are unavoidable. The $\beta_{\mathrm{DC}}$ specified at a certain value of $I_{\mathrm{C}}$ is usually the minimum value, $\beta_{\mathrm{DC}(\min )}$, although the maximum and typical values are also sometimes specified.

## Maximum Transistor Ratings

A BJT, like any other electronic device, has limitations on its operation. These limitations are stated in the form of maximum ratings and are normally specified on the manufacturer's datasheet. Typically, maximum ratings are given for collector-to-base voltage, collector-to-emitter voltage, emitter-to-base voltage, collector current, and power dissipation.

The product of $V_{\mathrm{CE}}$ and $I_{\mathrm{C}}$ must not exceed the maximum power dissipation. Both $V_{\mathrm{CE}}$ and $I_{\mathrm{C}}$ cannot be maximum at the same time. If $V_{\mathrm{CE}}$ is maximum, $I_{\mathrm{C}}$ can be calculated as

$$
I_{\mathrm{C}}=\frac{P_{\mathrm{D}(\max )}}{V_{\mathrm{CE}}}
$$

If $I_{\mathrm{C}}$ is maximum, $V_{\mathrm{CE}}$ can be calculated by rearranging the previous equation as follows:

$$
V_{\mathrm{CE}}=\frac{P_{\mathrm{D}(\max )}}{I_{\mathrm{C}}}
$$

For any given transistor, a maximum power dissipation curve can be plotted on the collector characteristic curves, as shown in Figure 4-18(a). These values are tabulated in Figure 4-18(b). Assume $P_{\mathrm{D}(\max )}$ is $500 \mathrm{~mW}, V_{\mathrm{CE}(\max )}$ is 20 V , and $I_{\mathrm{C}(\max )}$ is 50 mA . The curve shows that this particular transistor cannot be operated in the shaded portion of the graph. $I_{\mathrm{C}(\max )}$ is the limiting rating between points $A$ and $B, P_{\mathrm{D}(\max )}$ is the limiting rating between points $B$ and $C$, and $V_{\mathrm{CE}(\max )}$ is the limiting rating between points $C$ and $D$.

(a)

| $P_{\mathrm{D}(\max )}$ | $V_{\mathrm{CE}}$ | $I_{\mathrm{C}}$ |
| :--- | ---: | ---: |
| 500 mW | 5 V | 100 mA |
| 500 mW | 10 V | 50 mA |
| 500 mW | 15 V | 33 mA |
| 500 mW | 20 V | 25 mA |

(b)

AFIGURE 4-18
Maximum power dissipation curve and tabulated values.

## EXAMPLE 4-5

A certain transistor is to be operated with $V_{\mathrm{CE}}=6 \mathrm{~V}$. If its maximum power rating is 250 mW , what is the most collector current that it can handle?

$$
I_{\mathrm{C}}=\frac{P_{\mathrm{D}(\max )}}{V_{\mathrm{CE}}}=\frac{250 \mathrm{~mW}}{6 \mathrm{~V}}=41.7 \mathrm{~mA}
$$

This is the maximum current for this particular value of $V_{\mathrm{CE}}$. The transistor can handle more collector current if $V_{\mathrm{CE}}$ is reduced, as long as $P_{\mathrm{D}(\max )}$ and $I_{\mathrm{C}(\max )}$ are not exceeded.

If $P_{\mathrm{D}(\max )}=1 \mathrm{~W}$, how much voltage is allowed from collector to emitter if the transis- tor is operating with $I_{\mathrm{C}}=100 \mathrm{~mA}$ ?

## EXAMPLE 4-6

The transistor in Figure 4-19 has the following maximum ratings: $P_{\mathrm{D}(\max )}=800 \mathrm{~mW}$, $V_{\mathrm{CE}(\max )}=15 \mathrm{~V}$, and $I_{\mathrm{C}(\max )}=100 \mathrm{~mA}$. Determine the maximum value to which $V_{\mathrm{CC}}$ can be adjusted without exceeding a rating. Which rating would be exceeded first?

## FIGURE 4-19



Solution First, find $I_{\mathrm{B}}$ so that you can determine $I_{\mathrm{C}}$.

$$
\begin{aligned}
& I_{\mathrm{B}}=\frac{V_{\mathrm{BB}}-V_{\mathrm{BE}}}{R_{\mathrm{B}}}=\frac{5 \mathrm{~V}-0.7 \mathrm{~V}}{22 \mathrm{k} \Omega}=195 \mu \mathrm{~A} \\
& I_{\mathrm{C}}=\beta_{\mathrm{DC}} I_{\mathrm{B}}=(100)(195 \mu \mathrm{~A})=19.5 \mathrm{~mA}
\end{aligned}
$$

$I_{\mathrm{C}}$ is much less than $I_{\mathrm{C}(\max )}$ and ideally will not change with $V_{\mathrm{CC}}$. It is determined only by $I_{\mathrm{B}}$ and $\beta_{\mathrm{DC}}$.

The voltage drop across $R_{\mathrm{C}}$ is

$$
V_{R_{\mathrm{C}}}=I_{\mathrm{C}} R_{\mathrm{C}}=(19.5 \mathrm{~mA})(1.0 \mathrm{k} \Omega)=19.5 \mathrm{~V}
$$

Now you can determine the value of $V_{\mathrm{CC}}$ when $V_{\mathrm{CE}}=V_{\mathrm{CE}(\max )}=15 \mathrm{~V}$.

$$
V_{R_{\mathrm{C}}}=V_{\mathrm{CC}}-V_{\mathrm{CE}}
$$

So,

$$
V_{\mathrm{CC}(\max )}=V_{\mathrm{CE}(\max )}+\left(V_{R_{\mathrm{C}}}=15 \mathrm{~V}+19.5 \mathrm{~V}=\mathbf{3 4 . 5} \mathrm{V}\right.
$$

$V_{\mathrm{CC}}$ can be increased to 34.5 V , under the existing conditions, before $V_{\mathrm{CE}(\max )}$ is exceeded. However, at this point it is not known whether or not $P_{\mathrm{D}(\max )}$ has been exceeded.

$$
P_{\mathrm{D}}=V_{\mathrm{CE}(\max )} I_{\mathrm{C}}=(15 \mathrm{~V})(19.5 \mathrm{~mA})=293 \mathrm{~mW}
$$

Since $P_{\mathrm{D}(\max )}$ is 800 mW , it is not exceeded when $V_{\mathrm{CC}}=34.5 \mathrm{~V}$. So, $V_{\mathrm{CE}(\max )}=15 \mathrm{~V}$ is the limiting rating in this case. If the base current is removed causing the transistor to turn off, $\boldsymbol{V}_{\mathbf{C E}(\max )}$ will be exceeded first because the entire supply voltage, $V_{\mathrm{CC}}$, will be dropped across the transistor.

Related Problem
The transistor in Figure 4-19 has the following maximum ratings: $P_{\mathrm{D}(\max )}=500 \mathrm{~mW}$, $V_{\mathrm{CE}(\max )}=25 \mathrm{~V}$, and $I_{\mathrm{C}(\max )}=200 \mathrm{~mA}$. Determine the maximum value to which $V_{\mathrm{CC}}$ can be adjusted without exceeding a rating. Which rating would be exceeded first?

## Derating $\boldsymbol{P}_{\mathbf{D}(\text { max })}$

$P_{\mathrm{D}(\max )}$ is usually specified at $25^{\circ} \mathrm{C}$. For higher temperatures, $P_{\mathrm{D}(\max )}$ is less. Datasheets often give derating factors for determining $P_{\mathrm{D}(\max )}$ at any temperature above $25^{\circ} \mathrm{C}$. For example, a derating factor of $2 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ indicates that the maximum power dissipation is reduced 2 mW for each degree Celsius increase in temperature.

EXAMPLE 4-7

Solution The change (reduction) in $P_{\mathrm{D}(\max )}$ is

$$
\Delta P_{\mathrm{D}(\max )}=\left(5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}\right)\left(70^{\circ} \mathrm{C}-25^{\circ} \mathrm{C}\right)=\left(5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}\right)\left(45^{\circ} \mathrm{C}\right)=225 \mathrm{~mW}
$$

Therefore, the $P_{\mathrm{D}(\max )}$ at $70^{\circ} \mathrm{C}$ is

$$
1 \mathrm{~W}-225 \mathrm{~mW}=775 \mathrm{~mW}
$$

Related Problem A transistor has a $P_{\mathrm{D}(\max )}=5 \mathrm{~W}$ at $25^{\circ} \mathrm{C}$. The derating factor is $10 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$. What is the $P_{\mathrm{D}(\max )}$ at $70^{\circ} \mathrm{C}$ ?

## BJT Datasheet

A partial datasheet for the 2N3904 npn transistor is shown in Figure 4-20. Notice that the maximum collector-emitter voltage ( $V_{\mathrm{CEO}}$ ) is 40 V . The CEO subscript indicates that the voltage is measured from collector $(\mathrm{C})$ to emitter $(\mathrm{E})$ with the base open $(\mathrm{O})$. In the text, we use $V_{\mathrm{CE}(\max )}$ for this parameter. Also notice that the maximum collector current is 200 mA .

The $\beta_{\mathrm{DC}}\left(h_{\mathrm{FE}}\right)$ is specified for several values of $I_{\mathrm{C}}$. As you can see, $h_{\mathrm{FE}}$ varies with $I_{\mathrm{C}}$ as we previously discussed.

The collector-emitter saturation voltage, $V_{\mathrm{CE}(\mathrm{sat})}$ is 0.2 V maximum for $I_{\mathrm{C}(\text { sat })}=10 \mathrm{~mA}$ and increases with the current.

## EXAMPLE 4-8

A 2N3904 transistor is used in the circuit of Figure 4-19 (Example 4-6). Determine the maximum value to which $V_{\mathrm{CC}}$ can be adjusted without exceeding a rating. Which rating would be exceeded first? Refer to the datasheet in Figure 4-20.

Solution From the datasheet,

$$
\begin{aligned}
P_{\mathrm{D}(\max )} & =P_{\mathrm{D}}=625 \mathrm{~mW} \\
V_{\mathrm{CE}(\max )} & =V_{\mathrm{CEO}}=40 \mathrm{~V} \\
I_{\mathrm{C}(\max )} & =I_{\mathrm{C}}=200 \mathrm{~mA}
\end{aligned}
$$

Assume $\beta_{\mathrm{DC}}=100$. This is a reasonably valid assumption based on the datasheet $h_{\mathrm{FE}}=$ 100 minimum for specified conditions ( $\beta_{\mathrm{DC}}$ and $h_{\mathrm{FE}}$ are the same parameter). As you have learned, the $\beta_{\mathrm{DC}}$ has considerable variations for a given transistor, depending on circuit conditions. Under this assumption, $I_{\mathrm{C}}=19.5 \mathrm{~mA}$ and $V_{R_{\mathrm{C}}}=19.5 \mathrm{~V}$ from Example 4-6.

Since $I_{\mathrm{C}}$ is much less than $I_{\mathrm{C}(\max )}$ and, ideally, will not change with $V_{\mathrm{CC}}$, the maximum value to which $V_{\mathrm{CC}}$ can be increased before $V_{\mathrm{CE}(\max )}$ is exceeded is

$$
V_{\mathrm{CC}(\max )}=V_{\mathrm{CE}(\max )}+V_{R_{\mathrm{C}}}=40 \mathrm{~V}+19.5 \mathrm{~V}=59.5 \mathrm{~V}
$$

However, at the maximum value of $V_{\mathrm{CE}}$, the power dissipation is

$$
P_{\mathrm{D}}=V_{\mathrm{CE}(\max )} I_{\mathrm{C}}=(40 \mathrm{~V})(19.5 \mathrm{~mA})=780 \mathrm{~mW}
$$

Power dissipation exceeds the maximum of 625 mW specified on the datasheet.
Related Problem Use the datasheet in Figure 4-20 to find the maximum $P_{\mathrm{D}}$ at $50^{\circ} \mathrm{C}$.
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## NPN General Purpose Amplifier

This device is designed as a general purpose amplifier and switch The useful dynamic range extends to 100 mA as a switch and to 100 MHz as an amplifier.

| Symbol | Parameter | Value | Units |
| :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {cEo }}$ | Collector-Emitter Voltage | 40 | V |
| $\mathrm{V}_{\text {cbo }}$ | Collector-Base Voltage | 60 | V |
| $\mathrm{V}_{\text {EbO }}$ | Emitter-Base Voltage | 6.0 | V |
| $\mathrm{I}_{\mathrm{c}}$ | Collector Current - Continuous | 200 | mA |
| $\mathrm{T}_{\mathrm{J}, \mathrm{T}} \mathrm{stg}$ | Operating and Storage Junction Temperature Range | -55 to +150 | ${ }^{\circ} \mathrm{C}$ |

## notes

NOTES:

1) These ratings are based on a maximum junction temperature of 150 degrees $C$.
2) These are steady state limits. The factory should be consulted on applications involving pulsed or low duty cycle operation
Thermal Characteristics $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise noted

| Symbol | Characteristic | Max |  |  | Units |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  |  | 2N3904 | ${ }^{*}$ MMBT3904 | ${ }^{* *}$ PZT3904 |  |
| $\mathrm{P}_{\mathrm{D}}$ | Total Device Dissipation | 625 | 350 | 1,000 | mW |
|  | Derate above $25^{\circ} \mathrm{C}$ | 5.0 | 2.8 | 8.0 | $\mathrm{~mW} /{ }^{\circ} \mathrm{C}$ |
| $\mathrm{R}_{\text {日JC }}$ | Thermal Resistance, Junction to Case | 83.3 |  |  | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{R}_{\text {日JA }}$ | Thermal Resistance, Junction to Ambient | 200 | 357 | 125 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

*Device mounted on FR-4 PCB $1.6^{\prime \prime} \times 1.6^{\prime \prime} \times 0.06$."
${ }^{* *}$ Device mounted on FR - $4 \mathrm{PCB} 36 \mathrm{~mm} \times 18 \mathrm{~mm} \times 1.5 \mathrm{~mm}$; mounting pad for the collector lead min. $6 \mathrm{~cm}^{2}$

| Symbol | Parameter | Test Conditions | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| OFF CHARACTERISTICS |  |  |  |  |  |
| $\mathrm{V}_{\text {(BR) }}$ CEO | Collector-Emitter Breakdown Voltage | $\mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=0$ | 40 |  | V |
| $\mathrm{V}_{\text {(BR) }{ }^{\text {cbo }}}$ | Collector-Base Breakdown Voltage | $\mathrm{I}_{\mathrm{C}}=10 \mu \mathrm{~A}, \mathrm{I}_{\mathrm{E}}=0$ | 60 |  | V |
| $\mathrm{V}_{\text {(BR) } \mathrm{EBO}}$ | Emitter-Base Breakdown Voltage | $\mathrm{I}_{\mathrm{E}}=10 \mu \mathrm{~A}, \mathrm{I}_{\mathrm{C}}=0$ | 6.0 |  | V |
| $I_{\text {BL }}$ | Base Cutoff Ourrent | $\mathrm{V}_{\text {CE }}=30 \mathrm{~V}, \mathrm{~V}_{\text {EB }}=3 \mathrm{~V}$ |  | 50 | nA |
| Icex | Collector Cutoff Current | $\mathrm{V}_{\text {CE }}=30 \mathrm{~V}, \mathrm{~V}_{\text {EB }}=3 \mathrm{~V}$ |  | 50 | nA |
| ON CHARACTERISTICS* |  |  |  |  |  |
| $\mathrm{h}_{\text {FE }}$ | DC Current Gain | $\begin{aligned} & \mathrm{I}_{\mathrm{C}}=0.1 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=1.0 \mathrm{~V} \\ & \mathrm{C}_{\mathrm{C}}=1.0 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=1.0 \mathrm{~V} \\ & \mathrm{I}_{\mathrm{C}}=10 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=1.0 \mathrm{~V} \\ & \mathrm{I}_{\mathrm{C}}=50 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=1.0 \mathrm{~V} \\ & \mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=1.0 \end{aligned}$ | 40 70 100 60 30 | 300 |  |
| $\mathrm{V}_{\text {CE(sat) }}$ | Collector-Emitter Saturation Voltage | $\begin{aligned} & I_{\mathrm{C}}=10 \mathrm{~mA}, I_{\mathrm{B}}=1.0 \mathrm{~mA} \\ & I_{\mathrm{C}}=50 \mathrm{~mA}, I_{\mathrm{B}}=5.0 \mathrm{~mA} \end{aligned}$ |  | $\begin{aligned} & 0.2 \\ & 0.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ |
| $\mathrm{V}_{\text {BE(sat) }}$ | Base-Emitter Saturation Voltage | $\begin{aligned} & \mathrm{I}_{\mathrm{C}}=10 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=1.0 \mathrm{~mA} \\ & \mathrm{I}_{\mathrm{C}}=50 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=5.0 \mathrm{~mA} \\ & \hline \end{aligned}$ | 0.65 | $\begin{aligned} & \hline 0.85 \\ & 0.95 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{V} \\ & \mathrm{~V} \\ & \hline \end{aligned}$ |
| SMALL SIGNAL CHARACTERISTICS |  |  |  |  |  |
| $\mathrm{f}_{\mathrm{T}}$ | Current Gain - Bandwidth Product | $\begin{aligned} & I_{\mathrm{C}}=10 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=20 \mathrm{~V}, \\ & \mathrm{f}=100 \mathrm{MHz} \end{aligned}$ | 300 |  | MHz |
| Cobo | Output Capacitance | $\begin{aligned} & \mathrm{V}_{\mathrm{CB}}=5.0 \mathrm{~V}, \mathrm{I}_{\mathrm{E}}=0, \\ & \mathrm{f}=1.0 \mathrm{MHz} \end{aligned}$ |  | 4.0 | pF |
| $\mathrm{C}_{\text {ibo }}$ | Input Capacitance | $\begin{aligned} & V_{\text {EB }}=0.5 \mathrm{~V}, I_{C}=0, \\ & f=1.0 \mathrm{MHz} \end{aligned}$ |  | 8.0 | pF |
| NF | Noise Figure | $\begin{aligned} & \mathrm{I}_{\mathrm{C}}=100 \mu \mathrm{~A}, \mathrm{~V}_{\mathrm{CE}}=5.0 \mathrm{~V}, \\ & \mathrm{R}_{\mathrm{S}}=1.0 \mathrm{k} \Omega, \mathrm{f}=10 \mathrm{~Hz} \text { to } 15.7 \mathrm{kHz} \end{aligned}$ |  | 5.0 | dB |
| SWITCHING CHARACTERISTICS |  |  |  |  |  |
| $\mathrm{t}_{\mathrm{d}}$ | Delay Time | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=3.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{BE}}=0.5 \mathrm{~V}, \\ & \mathrm{I}_{\mathrm{C}}=10 \mathrm{~mA}, I_{\mathrm{B} 1}=1.0 \mathrm{~mA} \end{aligned}$ |  | 35 | ns |
| $\mathrm{t}_{\mathrm{r}}$ | Rise Time |  |  | 35 | ns |
| $\mathrm{t}_{\text {s }}$ | Storage Time | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=3.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=10 \mathrm{~mA} \\ & \mathrm{I}_{\mathrm{B} 1}=\mathrm{I}_{\mathrm{B} 2}=1.0 \mathrm{~mA} \end{aligned}$ |  | 200 | ns |
| ${ }^{\text {t }}$ | Fall Time |  |  | 50 | ns |
| ${ }^{\text {Peulse Test: Pulse Wiath } \leq 300 \mu \mathrm{~s} \text {, Duty Cycle } 52.0 \%}$ |  |  |  |  |  |

FIGURE 4-20
Partial datasheet. For a complete 2N3904 datasheet, go to http://www.fairchildsemi.com/ds/ 2N\%2F2N3904.pdf. Copyright Fairchild Semiconductor Corporation. Used by permission.

SECTION 4-3 CHECKUP

1. Define $\beta_{\mathrm{DC}}$ and $\alpha_{\mathrm{DC}}$. What is $h_{\mathrm{FE}}$ ?
2. If the dc current gain of a transistor is 100 , determine $\beta_{\mathrm{DC}}$ and $\alpha_{\mathrm{DC}}$.
3. What two variables are plotted on a collector characteristic curve?
4. What bias conditions must exist for a transistor to operate as an amplifier?
5. Does $\beta_{\mathrm{DC}}$ increase or decrease with temperature?
6. For a given type of transistor, can $\beta_{\mathrm{DC}}$ be considered to be a constant?

## 4-4 The BJT as an Amplifier

Amplification is the process of linearly increasing the amplitude of an electrical signal and is one of the major properties of a transistor. As you learned, a BJT exhibits current gain (called $\beta$ ). When a BJT is biased in the active (or linear) region, as previously described, the BE junction has a low resistance due to forward bias and the BC junction has a high resistance due to reverse bias.

After completing this section, you should be able to

- Discuss how a BJT is used as a voltage amplifier
- List the dc and ac quantities in an amplifier
- Describe how the dc and ac quantities are identified
- Describe voltage amplification
- Draw the schematic for a basic BJT amplifier - Define current gain and
voltage gain - Calculate voltage gain - Calculate amplifier output voltage


## DC and AC Quantities

Before discussing the concept of transistor amplification, the designations that we will use for the circuit quantities of current, voltage, and resistance must be explained because amplifier circuits have both dc and ac quantities.

In this text, italic capital letters are used for both dc and ac currents $(I)$ and voltages $(V)$. This rule applies to rms, average, peak, and peak-to-peak ac values. AC current and voltage values are always rms unless stated otherwise. Although some texts use lowercase $i$ and $v$ for ac current and voltage, we reserve the use of lowercase $i$ and $v$ only for instantaneous values. In this text, the distinction between a dc current or voltage and an ac current or voltage is in the subscript.

DC quantities always carry an uppercase roman (nonitalic) subscript. For example, $I_{\mathrm{B}}$, $I_{\mathrm{C}}$, and $I_{\mathrm{E}}$ are the dc transistor currents. $V_{\mathrm{BE}}, V_{\mathrm{CB}}$, and $V_{\mathrm{CE}}$ are the dc voltages from one transistor terminal to another. Single subscripted voltages such as $V_{\mathrm{B}}, V_{\mathrm{C}}$, and $V_{\mathrm{E}}$ are dc voltages from the transistor terminals to ground.

AC and all time-varying quantities always carry a lowercase italic subscript. For example, $I_{b}, I_{c}$, and $I_{e}$ are the ac transistor currents. $V_{b e}, V_{c b}$, and $V_{c e}$ are the ac voltages from one transistor terminal to another. Single subscripted voltages such as $V_{b}, V_{c}$, and $V_{e}$ are ac voltages from the transistor terminals to ground.

The rule is different for internal transistor resistances. As you will see later, transistors have internal ac resistances that are designated by lowercase $r^{\prime}$ with an appropriate subscript. For example, the internal ac emitter resistance is designated as $r_{e}^{\prime}$.

Circuit resistances external to the transistor itself use the standard italic capital $R$ with a subscript that identifies the resistance as dc or ac (when applicable), just as for current and voltage. For example $R_{\mathrm{E}}$ is an external dc emitter resistance and $R_{e}$ is an external ac emitter resistance.

## Voltage Amplification

As you have learned, a transistor amplifies current because the collector current is equal to the base current multiplied by the current gain, $\beta$. The base current in a transistor is very small compared to the collector and emitter currents. Because of this, the collector current is approximately equal to the emitter current.

With this in mind, let's look at the circuit in Figure 4-21. An ac voltage, $V_{s}$, is superimposed on the dc bias voltage $V_{\mathrm{BB}}$ by capacitive coupling as shown. The dc bias voltage $V_{\mathrm{CC}}$ is connected to the collector through the collector resistor, $R_{\mathrm{C}}$.


The ac input voltage produces an ac base current, which results in a much larger ac collector current. The ac collector current produces an ac voltage across $R_{\mathrm{C}}$, thus producing an amplified, but inverted, reproduction of the ac input voltage in the active region of operation, as illustrated in Figure 4-21.

The forward-biased base-emitter junction presents a very low resistance to the ac signal. This internal ac emitter resistance is designated $r_{e}^{\prime}$ in Figure 4-21 and appears in series with $R_{\mathrm{B}}$. The ac base voltage is

$$
V_{b}=I_{e} r_{e}^{\prime}
$$

The ac collector voltage, $V_{c}$, equals the ac voltage drop across $R_{\mathrm{C}}$.

$$
V_{c}=I_{c} R_{\mathrm{C}}
$$

Since $I_{c} \cong I_{e}$, the ac collector voltage is

$$
V_{c} \cong I_{e} R_{\mathrm{C}}
$$

$V_{b}$ can be considered the transistor ac input voltage where $V_{b}=V_{s}-I_{b} R_{\mathrm{B}} . V_{c}$ can be considered the transistor ac output voltage. Since voltage gain is defined as the ratio of the output voltage to the input voltage, the ratio of $V_{c}$ to $V_{b}$ is the ac voltage gain, $A_{v}$, of the transistor.

$$
A_{v}=\frac{V_{c}}{V_{b}}
$$

Substituting $I_{e} R_{\mathrm{C}}$ for $V_{c}$ and $I_{e} r_{e}^{\prime}$ for $V_{b}$ yields

$$
A_{v}=\frac{V_{c}}{V_{b}} \cong \frac{I_{e} R_{\mathrm{C}}}{I_{e} r_{e}^{\prime}}
$$

The $I_{e}$ terms cancel; therefore,

$$
A_{v} \cong \frac{\boldsymbol{R}_{\mathrm{C}}}{r_{e}^{\prime}}
$$

Equation 4-7 shows that the transistor in Figure 4-21 provides amplification in the form of voltage gain, which is dependent on the values of $R_{\mathrm{C}}$ and $r_{e}^{\prime}$.

1 FIGURE 4-21
Basic transistor amplifier circuit with ac source voltage $V_{s}$ and dc bias voltage $V_{\mathrm{BB}}$ superimposed.

Equation 4-7

Since $R_{\mathrm{C}}$ is always considerably larger in value than $r_{e}^{\prime}$, the output voltage for this configuration is greater than the input voltage. Various types of amplifiers are covered in detail in later chapters.

## EXAMPLE 4-9

FIGURE 4-22

Solution The voltage gain is

$$
A_{v} \cong \frac{R_{\mathrm{C}}}{r_{e}^{\prime}}=\frac{1.0 \mathrm{k} \Omega}{50 \Omega}=\mathbf{2 0}
$$

Therefore, the ac output voltage is

$$
V_{\text {out }}=A_{V} V_{b}=(20)(100 \mathrm{mV})=\mathbf{2} \mathbf{V} \mathbf{~ r m s}
$$

Related Problem What value of $R_{\mathrm{C}}$ in Figure $4-22$ will it take to have a voltage gain of 50 ?

## SECTION 4-4 CHECKUP

1. What is amplification?
2. How is voltage gain defined?
3. Name two factors that determine the voltage gain of an amplifier.
4. What is the voltage gain of a transistor amplifier that has an output of 5 V rms and an input of 250 mV rms?
5. A transistor connected as in Figure 4-22 has an $r_{e}^{\prime}=20 \Omega$. If $R_{\mathrm{C}}$ is $1200 \Omega$, what is the voltage gain?

## 4-5 The BJT as a Switch

In the previous section, you saw how a BJT can be used as a linear amplifier. The second major application area is switching applications. When used as an electronic switch, a BJT is normally operated alternately in cutoff and saturation. Many digital circuits use the BJT as a switch.

After completing this section, you should be able to

- Discuss how a BJT is used as a switch
- Describe BJT switching operation
- Explain the conditions in cutoff
- Determine the cutoff voltage in terms of the dc supply voltage

